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PERTH ADDRESS: 43 PLANET STREET, CARLISLE, WESTERN AUSTRALIA, 6101 TELEPHONE: (09) 361 4437 (09) 361 4963 TELEX AA92372 CABLE: EXLOGG, PERTH

GEOLOGICAL - ENGINEERING WELL REPORT

ESSO AUSTRALIA LIMITED

FORTESCUE No. 2 BASIC NOVEMBER 1978

by

EXPLORATION LOGGING OF AUSTRALIA INC.

CONTENTS

		-							
I.	INTRODUCTION								
II.	WELL HISTORY								
III.	GEOPRESSURE ENGINEERING								
	A. Pore Pressure - Lithology - Drill Rate - Drilling Exponent - Ditch Gas - Temperature								
-	B. Fracture Pressure								
IV.	DRILLING ENGINEERING								
	A. Well Data								
	B. Bit Data								
	C. Hydraulic Data								
	D. Hole Condition								
	E. Hole Deviation								
۷.	HYDROCARBON EVALUATION								
VI.	CONCLUSIONS AND RECOMMENDATIONS								
	APPENDICES								
	A. Geopressure Engineering Methods								
	B. Instrumentation and Data Collection Methods								
	C. Manual Plots and Tables								
	(i) Drilling Data Pressure Log								
	(ii) Temperature Data Log								
	(iii) Pressure Analysis Log								
	D. Computer Prints and Plots								
	(i) Drilling Data Printout								
	(ii) Borehole Hydraulics Pressure Loss Data Printout								
	(iii) Drilling Data Plot: 1:1000								
	(a) ROP, Dxc, Torque, WOB, RPM								
	(b) ROP, Dxc, Torque, Flowline Temp, Pore Pressure, ECD								

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I. INTRODUCTION

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The Fortescue No. 2 exploration well was drilled in the Gippsland Basin in the Bass Strait at geographical coordinates 38⁰25' 56.96"S, 148⁰15' 59.13"E.

The well was spudded in 70 metres of water on 30th October, 1978 and drilled to a total depth of 2653 metres on 14th November, 1978. The objective was to evaluate the position of liquid boundaries and the hydrocarbon content in the Latrobe sandstones within the Latrobe Group.

The well was plugged and abandoned after wireline testing on 21st November, 1978.

Drilling was contracted to the Odeco semi-submersible rig "Ocean Digger". Exploration Logging of Australia, Inc. provided a full data acquisition and pressure detection service using the Gemdas Level VI system. (Geological Engineering and Data Acquisition System).

II. WELL HISTORY

a)				section, r 1978	101m	(seabed)	-	256m	(20"	casing	point),
	NB	ŧ	1	HTC	050	C3AJ	2	26"		132-256	m

Fortescue No. 2 was spudded on 30th October 1978 with an HTC OSC 3AJ 26" bit with 20, 20, 20 jets which drilled to 256 metres in $7\frac{1}{2}$ hours without a marine riser. At 256 metres the hole angle was $\frac{1}{2}^{0}$. 20" casing was set with the shoe at 234 metres with 650 sacks of Class N cement with 2600 bbls of gel, and tailed with 350 sacks of Class N cement with 2% C_aCl₂ and 43 bbls of fresh water.

b)				section, mber 197		879	m	(13	3/8	11	casing	poin	t),
	NB	ŧ	2	НТС	OSC3A	J		17	71 ₂ "		256-8	3 7 9 m	1

A $17\frac{1}{2}$ " HTC OSC 3AJ with 20, 20, 20 jets was used to drill out the shoe and continued drilling to 879 metres using spud mud as the circulation fluid. Initially the penetration rate averaged 180 metres per hour, but was slowed to a 40 metre per hour average due to a rapid increase in mud solids. Mud weights of 8.5ppg at 260 metres rapidly increased to 10.0 ppg at the flowline at 879 metres. The maximum formation gas over this interval was 74 units and the average background gas increased from 6 units to 40 units. At 879 metres the hole was circulated clean prior to running ISF/Sonic, FDC/GR/Cal logs. Hole deviation at 879 metres was 0° . 13.3/8" casing was run and cemented with the shoe at 861 metres. Before drilling out the B.O.P's were tested.

c)	12¼'	hole	section,	879 -	2420m,	3 - 8	November 1978
	NB	≠ 3	нтс	ХЗА		12¼"	879 - 1238 m
	NB	≠ 4	HTC	ХЗА		124"	1238 - 1615 m
	NB	≠ 5	HTC	ХЗА		124"	1615 - 2142 m
	NB	≠ 6	HTC	ХЗА		124"	2142 - 2420 m

An HTC X3A $12\frac{1}{4}$ " bit with 18, 18, 18 jets drilled out the cement and shoe using a lightly dispersed mud type of 9.2 ppg. At 894 metres a

- 2 -

pressure integrity test was performed; the hole was pressured to 13.5ppg EMW without any leak-off occurring. This bit drilled on to 1238 metres attaining an average rate of penetration of 19.4 metres and the background gas varied from 12 to 20 units. A survey at 1238 metres indicated a possible hole angle of $2.3/4^{\circ}$. Trip gas at this depth was 60 units.

Bit No. 4, another HTC X3A $12\frac{1}{4}$ " bit with 18, 18, 18 jets drilled to 1615 metres at an average rate of 12.2 metres per hour, using 160 RPM and 50,000 lbs weight. The maximum formation gas for this bit run was 16 units at 1135 metres and the average background gas was 6 units. Trip gas at 1615 metres was 12 units. A survey at 1615 indicated a hole angle of 0° .

Bit No. 5 was another HTC X3A $12\frac{1}{4}$ " bit with 18, 18, 20 jets. This bit drilled to 2142 metres at an average penetration rate of 19.9 metres per hour using 120 RPM and 40 - 60,000 lbs. weight. The average background gas was 7 units for this bit run; the maximum formation gas being 8 units. Trip gas at 2142 metres was 5 units, and a survey showed the hole angle to be $\frac{1}{2}^{0}$.

Upon resuming drilling with bit no. 6, an HTC X3A $12\frac{1}{4}$ " bit with 18, 18, 20 jets, the flowline became blocked with gumbo at 2146 metres. This took 2 hours to clear before drilling recommenced. At the start of the bit run the mud system was treated such that the lightly dispersed type was changed to a Polysal type. The average penetration rate for this bit was 16.6 metres per hour using 135 RPM and 20 - 60,000 lbs. weight. This bit was pulled at 2420 metres, the average background gas for the interval was 4 units, with a maximum of 8 units. Mud weight to 2345 metres averaged 9.1 to 9.4 ppg, but at 2345 metres the mud was weighted up to 9.3 ppg, and this weight was maintained to T.D.

The hole was circulated clean and the pipe was strapped out of the hole in preparation for the coring programme. The mud was changed to a polymer type at this stage, this mud being used to T.D. A survey at 2420 metres showed a hole angle of 2° .

- 3 -

d)	8 15	/32" ho	ole section,	2420 -	2464m -	coring,	9 - 1	l Novei	nber	1978
	CB		CHRIS	C22		15/32		2420 -		
	CB CB	•	CHRIS CHRIS	RRC22 RRC22		15/32 15/32		2436 - 2451 -		

Core barrel No. 1 was run in and bottom up was circulated prior to coring. Trip gas at 2420 metres was 12 units. Core No. 1 was cut from 2420 metres to 2436 metres at an average penetration rate of 0.8 metres per hour. The core bit used was a Christensen C22 8.15/32". Recovery was 97%. 50-80 RPM and 30,000 lbs. weight were used to cut the core.

Core No. 2 was cut with the same C22 bit, to 2451 metres. An average rate of penetration of 2.3 metres per hour was achieved with 50-85 RPM and 20,000 lbs. weight. Recovery was 79%.

Core No. 3 used the same bit again, from 2451 metres to 2464 metres. The average penetration rate was 3.3 metres per hour using 60-80 RPM and 15 - 20,000 lbs. weight. Recovery was 81%.

e) 12¼" hole section, 2420 - 2464m - 12 November 1978 NB ≠ 7 HTC XDG 12¼" 2420 - 2464 m

Bit No. 7, a 12¼" HTC XDG with 14, 15, 15 jets was used to ream the rat-hole from 2420 metres to 2464 metres. At 2464 metres the bit became stuck in the hole necessitating 100,000 lbs. overpull to free it. Upon pulling the bit it was found to have several broken teeth.

f) 8 15/32 " hole section, 2464 - 2480 m - coring, 12 - 13 November 1978

CB ≠ 4 CHRIS C20 8 15/32" 2464 - 2480 m

Core No. 4 was cut from 2464 metres to 2480 metres with a Christensen C20 8.15/32" bit. Using 80 RPM and 20,000 lbs. weight it drilled at an average rate of penetration of 3.8 metres per hour. Recovery was 87.5%. Background gas during coring operations varied from 1 unit to 4 units with no peaks. Trip gas at 2480 metres was 22 units.

g)	12¼"	hole	section,	2464 - 2653m ·	- 13 - 14	November 1978
	NB	≠ 8	HTC	XDG	12¼"	2464 - 2600 m
	NB	≠ 9	HTC	XDG	12¼"	2600 - 2653 m

Bit No. 8, an HTC XDG $12\frac{1}{4}$ " bit with 15, 15, 15 jets drilled to 2600 metres at an average rate of 13.1 metres per hour using 120 RPM and 50- 60,000 lbs. weight. The average background gas for this bit run was 2 units with a maximum of 4 units. Trip gas at 2600 metres was 18 units.

Bit No. 9, an HTX XDG 12¼" bit with 15, 15, 16 jets drilled to T.D. at 2653 metres at an average rate of 18.8 metres per hour using 120 RPM and 50,000 lbs. weight. The average background gas was 2 units with a maximum of 3 units. Bottoms-up was circulated prior to a wiper trip, after which returns were circulated again in preparation for Schlumberger logs. Trip gas from the wiper trip was 40 units. Logs run at T.D. were IES/Sonic, FDC/CNL, HDT, CIS, RFT, CST.

Fortescue No. 2 was plugged and abandoned on 21st November 1978.

III. <u>GEOPRESSURE ENGINEERING</u>

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A. PORE PRESSURE

Refer to Appendix C (iii) Pressure Analysis Log, for a graphical presentation of the pore pressure regimes present in Fortescue No. 2

Before a more detailed analysis of the various pressure evaluation parameters is undertaken it may be stated in general that the absence of hole problems in Fortescue No. 2 can be attributed to the absence of abnormal pressure regimes. An overbalanced condition was maintained throughout the well with the mud weights used. This may have hindered rather than enhanced the optimization of drill rates and hydrocarbon evaluation. A pressure gradient of 8.5 lb/gal E.M.W. was considered to be normal for the area.

LITHOLOGY -

Because of the absence of clean shales throughout the well, very little in the way of quantitative analysis could be performed. However, general compaction trends modified locally by lithological variations are readily observable in both the drill rate and drilling exponent plots.

DRILL RATE -

The top hole section of the well drilled at rates of up to 500 m/hr. These decreased with depth to 10 m/hr. Apart from minor fluctuations the decrease was uniform. Four cores were cut between 2420 and 2480 metres. Drill rates during coring varied from 1 m/hr in siltstone to a maximum of 7 m/hr in sandstone. The remainder of the well was drilled in sequence of interbedded sandstones, siltstones and coal which were erratic in behaviour as regards drill rate and drilling exponents.

The use of bumper subs in the drill string was an obstacle to the accurate determination of drill rates and subsequent drilling exponent analysis. Wherever possible these inaccuracies have been removed.

- 6 -

DRILLING EXPONENTS -

As a result of the absence of clean shales it was not possible to establish a normal trend line for corrected 'd' exponent which was suitable for quantitative use. However, with one exception normal compaction trends were readily apparent. A kick back in trend occurs at 1615 metres, however this was not considered to be an indication of abnormal pressure but a reflection of the transitional nature of the lithology in the interval.

GAS -

Background gas ranged from a low of $\frac{1}{2}$ unit to 50 units. The maximum gas reading recorded was 74 units at 717 metres. Below 879 metres average background gas showed a steady decrease to 2 units at TD. Oil was found in sands in cores \neq 2 and \neq 3.

It is considered that the magnitude of the gas readings were adversely affected by the high overbalance in the borehole.

No connection gases were recorded and trip gas values were consistent with influencing factors such as length of time spent out of the hole.

These were taken to be an indication that the pressure regime of the area was normal.

TEMPERATURE -

Continuous monitoring of the flowline temperature was carried out in an attempt to locate transition zones in the geothermal gradient due to changes in the thermal conductivity of the formations due to the presence of excess pore fluids. On all occasions when sudden decreases or increases in the flowline temperature occurred, either the addition of water or chemicals to the mud system was the apparent cause. B. FRACTURE PRESSURE

Refer to Appendix C (iii), Pressure Analysis Log, for a graphical presentation of the estimated fracture gradients for Fortescue No. 2.

Values for fracture pressure in Fortescue No. 2 were calculated using standard methods derived from Gulf Coast data. The three principal methods used were Mathews and Kelly, Eaton's and Anderson et al.

A pressure integrity test was performed at the 13.3/8" casing shoe, although the test did not continue to leak off. From this data, however, it was possible to calculate a value for Poisson's ratio, which was then used to prepare a fracture curve using Eaton's method. Due to the imcomplete fracture test data the calculated value for Poisson's ratio is somewhat higher than values normally obtained from actual leak off pressures.

The overburden gradient was calculated from bulk density values obtained from wireline data for the whole well. An overburden curve was thus established and the values used in determination of fracture pressures.

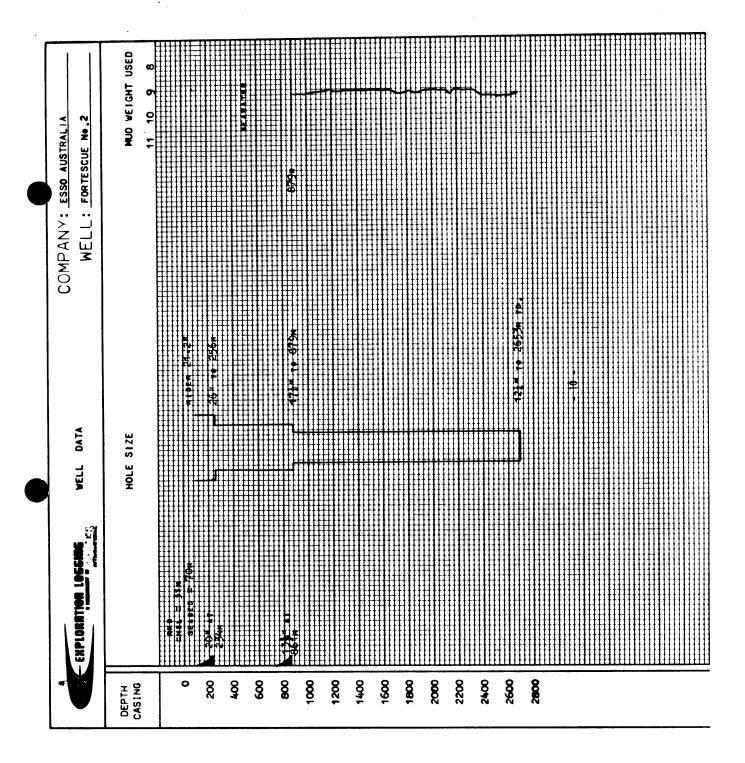
At no time during the drilling of Fortescue No. 2 was there any indication that mud hydrostatic could exceed the estimated fracture gradient.

IV. DRILLING ENGINEERING

Monitoring and analysis of the Drilling Engineering at the wellsite was centred on the Bit Analysis, Hydraulics, Hole Condition and Hole Deviation.

The pertinent data for each engineering aspect covered is presented in a tabular format, in this section.

More detailed analysis of all the engineering parameters relevant to the drilling of the well, such as weight on bit, rate of penetration, torque, mud characteristics, detailed hydraulics and flow regime analysis, are presented in Appendix D as hardcopy computer printouts and plots reduced to size for this Report or reference to the original listings in the Esso files.



CB 1 CB 2 CB 3 CB 4 NO. 7 Q œ δ თ ω N 8 15/32" CHRIS 8 15/32" CHRIS 8 15/32" CHRIS 8 15/32" CHRIS 124" 124" 124" 12%" 12%" 1214" 124" SIZE 175" 26" HTC HTC HTC HTC HTC HTC HTC HTC MAKE нтс RR C22 RR C22 TYPE OSC3AJ OSC3AJ XDG XDG C22 X 3A ХЗА X 3A ХЗА 1351 8888 8888 1351 8888 8888 1141 1141 1351 1141 1141 1111 1111 CODE 20,20,20 JET SIZES 15,15,16 15,15,15 18,18,20 18,18,18 18,18,18 14,15,15 18,18,20 20,20,20 ! ł 2600-2653M DRILLED 2464-2600M 2464-2480M 2420-2464M 2451-2464M 2436-2451M 2142-2420M 879-1238M 0-256M 2420-2436M 1615-2142M 1238-1615M 256-879M 20 3/4 3 11¥ 16 3/4 10 18 31 26½ HOURS ų L Š ω AVERAGE ROP (m/HR) 16.3 10.7 14.7 REAM 16.6 19.9 з. 8 0.8 з. З 2.3 12.2 19.4 38.3 21.5 195 178 567 FINAL COST/M 24 32 161 12 1 50-60 15-20 20-60 40-60 MOB APPM TORQUE CONDITION 20 28 33 50 5-10 ខ 50 88 60-80 50-85 50-80 120 **80** 120 140 135 **16**0 120 125 120 120 5.5 з.5 4.5 5.5 G 4 თ J ω · 2 3 1 5 3 3/16 324 SALVAGE SALVAGE 15% WORN 271 10% WORN 4 ω N -7 1/16 œ თ N N 1/16 1/8 ----0

BIT SUMMARY - COST ANALYSIS

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ECD (PPG)		9.26	9.30	9.29	9.48	9.46	
Impact For	rce (1b)	1814	520	1767	1752	1285	
Bit Hydrau	ilic HP	664	114	691	674	530	
Jet Pressu (PSI)	ire Drop	1094	387	1220	1209	1377	
Jet Veloci ft/sec	ty	363	217	387	381	409	- · ·
PV/YP	· .	7/15	8/13	7/14	14/16	17/22	
Mud Wt in PPG		1.6	9.1	9.1	9.3	9.3	
ES	Riser	60	29	56	55	38	
LOCITI	Casing	74	92	182	174	120	
ANNULAR VELOCITIES Ft/Min	Pipe	- 16	66	190	187	120	
ANNU	Collars	103	138	264	260	180	
Pump Press	ure (PSI)	2320	850	2660	2370	2710	
Mud Flow (SPM)	120	58	112	011	76	
Mud Flow (I	GPM)	1040	505	970	955	660	
Av Drill Ra	ate (m/hr)	580	22	26	35	20	
Nozzles (/32)		20 20 20	18 18 18	18 18 20	18 18 20	15 15 16	
lole Size ((in)	17%	12%	124	12%	124	
DEPTH INTERVAL (M)		265-878	878-1135	1135-2235	2235-2420	2420-2653	

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HYDRAULICS ANALYSIS

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D. HOLE CONDITION

The borehole condition was monitored during the drilling of the well by observing the differential lag time, the type, percentage, size and shape of the cavings, the hole deviation, the estimated differential pressure, the percentage of swelling clays, and the differential annular velocity adjacent to the drill collars. During trips hole drag and fillup were monitored and recorded.

There were two isolated borehole problems in the well, namely, blocked flowline and stuck pipe.

Carbides indicated that the well remained reasonably in gauge to 2142 metres with a maximum difference between carbide and theoretical lag of +120 strokes. At 2142 metres the flowline became blocked and took some two hours to clear. Subsequent carbides indicated the hole was out of gauge with a carbide to a theoretical lag difference of +613 strokes.

After reaming out the core rat hole at 2464 metres the drill string became stuck and took an overpull of 100,000 lbs.

With the exception of excessive cavings at 2142 metres sample quality was good with only approximately 5% cavings.

E. SURVEY DATA

Depth M.	Inclination Deg.
256	12
879	0
1238	2 3/4?
1615	0
2142	1
2420	2 ² 0

V. <u>HYDROCARBON EVALUATION</u>

INTRODUCTION -

Hydrocarbon evaluation at the wellsite was performed while drilling by use of standard mud logging techniques. These included "hot wire" gas detection which indicated the relative amount of combustible gas in the drill returns. Both total gas and petroleum vapours (all combustible gases less methane) were monitored and recorded.

Gas held in cuttings was assessed by pulverising 100 cc's of cuttings in a blendor with water and measuring the amount of gas liberated. A comparison of the cuttings' gas magnitude with that of the ditch gas was used to give a qualitative indication of formation permeability.

Ditch gas was analysed continuously and automatically by three chromatographs, standard catalytic, hydrogen flame ionization and thermoconductivity. The catalytic detector can become saturated at high gas levels and the flame ionization detector is used as a back-up in this event. The thermoconductivity chromatograph was used to detect inert gases nitrogen and helium and also for carbondioxide.

Samples of mud and pulverised cuttings gas were manually entered into the standard chromatograph directly from the blendor.

Oil evaluation was undertaken by observing the mud and unwashed cuttings for oil. Cuttings samples were observed under the ultraviolet light for all fluorescence and solvent cut.

RESULTS -

Gas readings were generally low throughout the drilling of Fortescue No. 2. In the surface hole section the background gas remained at around 2 units to 450 metres where it increased steadily to 10 units. Prior to setting surface casing ditch gas increased to 50-70 units. All chromatographic analysis showed only C_1 present in this section.

Following the setting of 13 3/8" casing the ditch gas dropped steadily to a background of less than 10 units, falling further to under 5 units as the payzone was approached. Small traces of C_2 were recorded from 1100 metres down.

Before encountering the Labrobe Formation the drilling was halted and the top of the payzone was continuously cored. Mud weight was increased prior to penetration of the paysands and these factors led to a further drop in ditch gas. Despite the evidence of oil in the cores ditch gas and chromatographic analysis showed no significant increase during the coring of the Latrobe Group sands.

When drilling recommenced after coring there was no increase in gas detected in the mud, although traces of C_3 were consistent after penetrating some coal stringers. Gas remained low until T.D. at 2653 metres.

Cuttings gas was negligible throughout the entire well. No connection gases were observed and maximum trip gas was 50 units at 2536 metres.

GAS RATIOS -

Since the gas readings taken while drilling were so low and the presence of only three members of the paraffin series detected, the most useful application of the gas ratio analysis is with the samples gained from the RFT tool which were analysed by chromatograph at the wellsite. A printout of these results is included (See A).

N.B. DELTA C = $%C_1 - (%C_3 + %C_4)$

TRIANGULAR GAS PLOT - (See B.)

A triangular gas plot analysis of the hydrocarbon measurements from the RFT tool was conducted to determine possible productivity and hydrocarbon phase of the formation fluids.

It has been found that the summation of $%C_2/100 + %C_3/100 + %C4/100$ called the hydrocarbon coefficient (HC) is directly proportional to the

size of the triangle plotted. The larger the HC then the wetter the gas is, or the heavier the oil is. The hydrocarbon phase is determined by the orientation of the triangle - i.e. if the apex is above the base Δ gas is indicated; the opposite ∇ indicates oil. Of the five sets of results plotted all triangles indicated oil phase and three plotted offscale indicating a heavier oil phase.

From empirical methods it has been found that an HC of < 0.003 indicates unproductive, 0.003 < HC < 0.175 indicates gas and HC > 0.175 indicates oil. In addition, if lines are drawn from each corner of the plotted triangle to the points A, B and C, then they intersect at a data point (+). If this point falls within the ellipse then the section is considered productive.

All the HC values from Fortescue No. 2 were above 0.175, which indicated oil but the intersection data points fell outside of the ellipse, though close, indicates doubtful productivity.

RECTANGULAR GAS RATIO PLOT (See C.) -

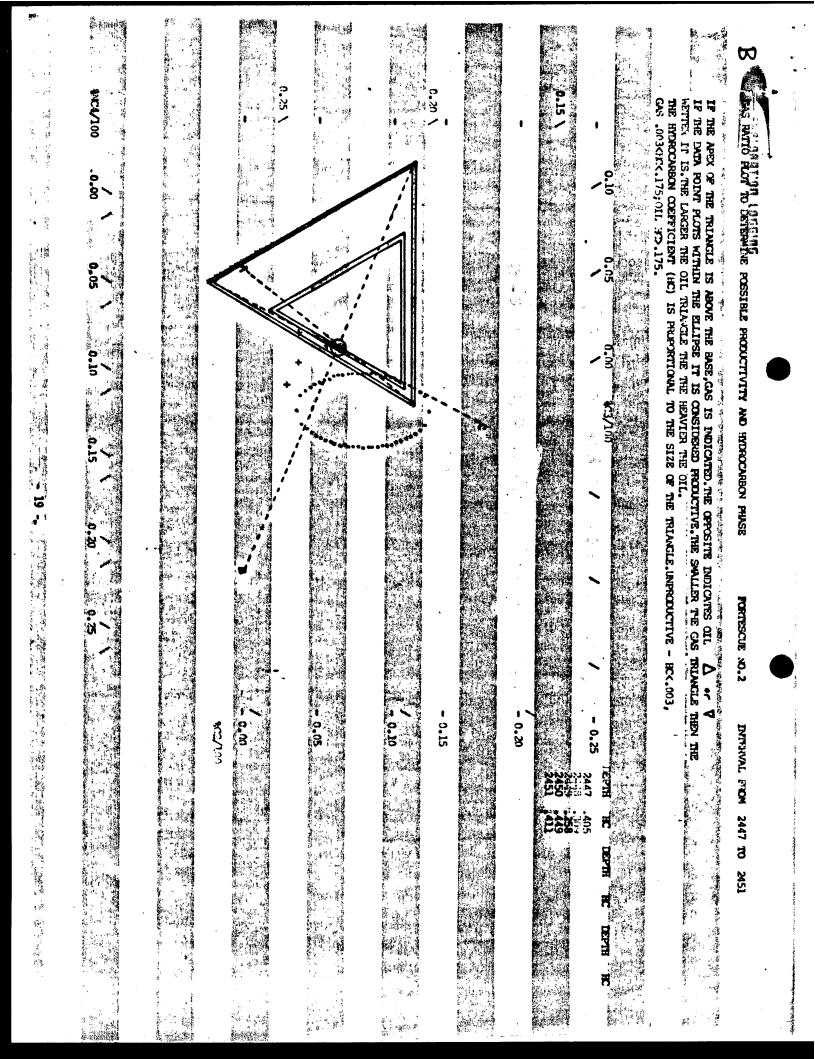
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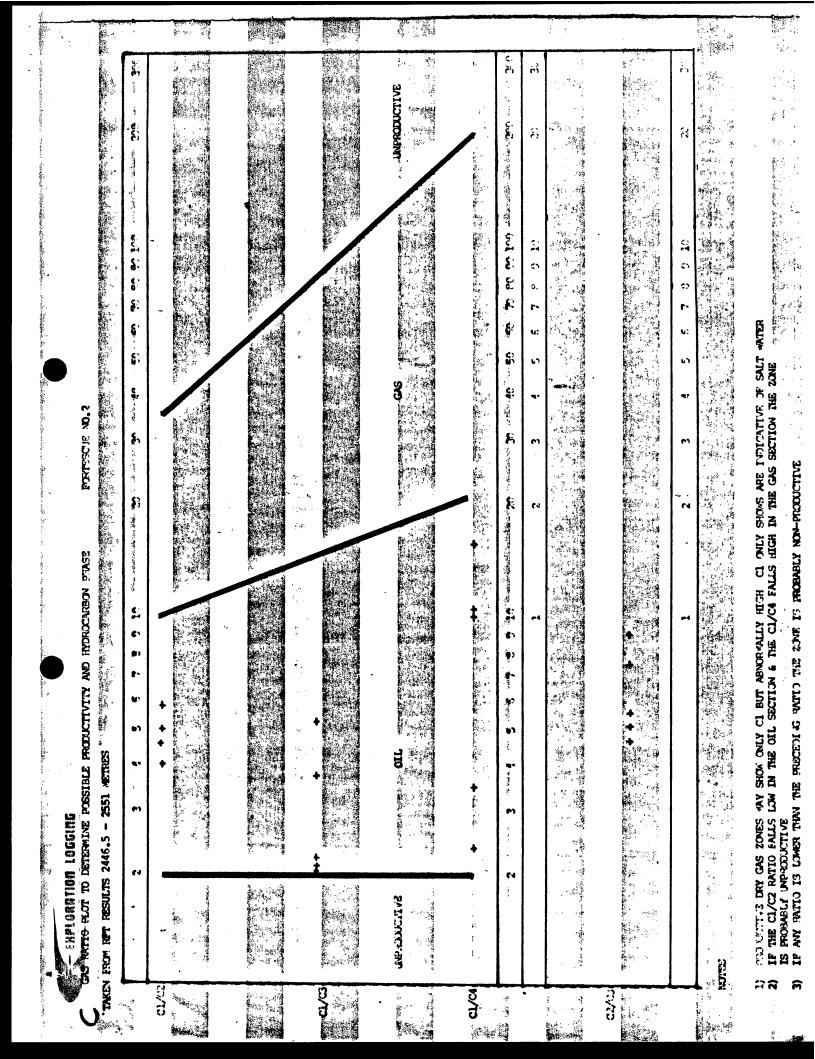
This gas ratio plot uses methane ratios to determine possible productivity and hydrocarbon phase. The limitations are as follows:-

- a) Productive dry gas zones may show only C₁ but abnormally high C₁ shows are usually indicative of salt water.
- b) If the $C_{T}C_{2}$ ratio falls low in the oil section and the $C_{T}C_{4}$ ratio falls high in the gas section the zone is probably non-productive.
- c) If any ratio (C+C₅excepted if oil mud is used) is lower than a preceding ratio the zone is probably nonproductive. For example, if the C+C₄ ratio is less than the C+C₃ ratio the zone is probably wet.
- d) The ratios may not be definitive for tight, low permeability zones.

All results plotted from Fortescue No. 2 indicate the oil phase. Lower C_3 ratios with respect to C_2 indicates non-productive zones in all cases. These gas ratio programs are still in the experimental stage, and with more data available the phase boundaries and productivity prediction fields may be modified. From the results shown for Fortescue No. 2, the plots correctly identify the phase since oil was recovered in the RFT tool. The indications of productivity were all negative or at least marginal, though production tests may prove otherwise.

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VI. CONCLUSIONS AND RECOMMENDATIONS

The successful drilling of Fortescue No. 2 in 16 days to 2653 metres was attributed in part to the normal pore pressure regimes and consequent lack of hole problems.

For future wells in the same area it is recommended that mud weights used in drilling competent formations are such that at any depth the mud hydrostatis pressure is kept at approximately 200 p.s.i. more than the estimated pore pressure at that depth. This is a practical over-balance margin which would allow pore pressure estimation and hydrocarbon evaluation to be more accurate and meaningful.

APPENDIX A

GEOPRESSURE AND ENGINEERING METHODS

Appendix A

Page

DATA ACQUISITION AND ANALYSIS METHODS

Α.	Pore	Pressure Prediction						
	I.	Befo	re Drilling					
		(1)	Seismic Information					
		(2)	Well Histories	iii				
	II.	Drill	ling Parameters	iii				
		(1)	Rate of Penetration					
		(2)	Drilling Exponent Corrected	iii				
		(3)	Temperature	v				
		(4)	Gas	vii				
		(5)	Shale Density	ix				
		(6)	Shale Factor	x				
		(7)	Hole Condition	xii				
в.	Pore	Press	sure Quantification	xiii				
с.	Overt	ourder	Pressure Determination	xxi				
D.	Fract	Fracture Pressure Determination xxi						

Appendix A

Data Acquisition and Methods of Analysis

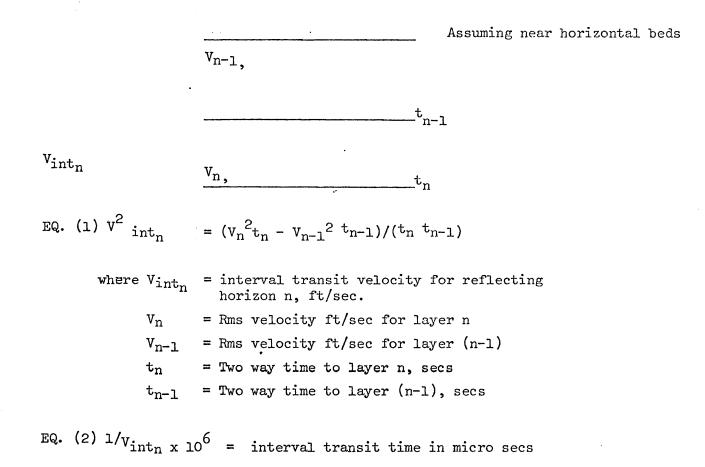
The methods used to obtain data, and the calculations employed to predict and quantify pore and fracture pressures are explained below.

A. Pore Pressure Prediction and Detection

- I. Before Drilling
- (1) Seismic Information

Field data from the reflection seismograph may be used to predict both the depth to abnormally pressured formations and the approximate pressure magnitude. The degree of accuracy depends upon the quality of the velocity spectrum. Where common depth point stacking is performed and scanned using RMS velocity increments of 50 feet/sec., areas of greatest semblance are enhanced. Therefore interval velocity calculations are more accurate and trends can be placed within closer limits.

From the velocity spectrum of RMS velocity versus two-way time, the interval transit time of the seismic energy (Eq. 2) (reciprocal of interval velocity $x \ 10^6$) can be derived using Dix's formula (Eq. 1). A near exponential decrease of interval transit time with depth is usually seen in normally compacted sediments. Departures from this curve are usually caused by abnormal pressures, formation changes and poor resolution in the velocity analysis. With Interval Transit Time plotted on the semilogrithmic X axis (abscissa) and depth on the linear axis (ordinate), a "sonic log" type plot is produced. Therefore the compaction trend can be readily compared with that derived from shale interval transit time from the sonic wireline logging tool. Decreases in the rate of decrease of interval time (i.e. increase interval velocity) with depth within shale section is usually indicative of undercompaction and geopressures. Screening of raw data during drilling of the well consists of selecting shale points and utilizing velocity survey data at casing points. This can help to reduce the log intervals over which data is averaged and so narrow down the range of possible normal trends. The greater the velocity data available in an area the more accurate the pore pressure predictions.



ii

(2) Well Histories

Data from other wells drilled in the vicinity are very useful prespud information. Information from seismic profiles, wireline logs (FDC, sonic and conductivity/resistivity), FIT and DST data, lithology and mud logs, and completion and pressure reports is of great asset in evaluating the pore pressure prospects in a new well.

II. Drilling Parameters

(1) Rate of Penetration

The rate of penetration is calculated from a kelly height versus time recorder.

With constant drilling conditions (i.e. bit size, weight on bit, rotary rpm, hydraulics and mud weight) in a uniform lithology, the rate of penetration will be determined by formation compaction characteristics. As the formations become more compacted with depth, the rate of penetration will decrease. The lithology used for determining the compaction rate is clean shale. On entering an overpressured shale there will be an increase in drill rate concomitant with the increase in porosity, and the decrease in differential pressure between mud weight and pore pressure.

It is not always possible to maintain constant parameters when drilling, and bit wear is usually an unknown factor.

To normalise the parameters and remove the effect of all non-lithological variations, the corrected drilling exponent was devised.

(2) Dxc (Drilling Exponent Corrected)

Various formulae have been proposed to allow control of the major drilling variables. The Jorden and Shirley formulation allows control of most of the drilling variables and has proved very successful in most areas.

iii

$$Dx = \frac{Log \frac{R}{60N}}{Log \frac{12W}{10^{6}D}}$$

where D = drilling exponent

R = rate of penetration (ft/hour)

N = rotary speed (rpm)

W = weight on bit (lbs)

 $D \cdot = bit diameter (in)$

The drilling exponent will increase with depth, compaction and differential pressure in a homogenous shale. On entering an overpressured zone, the compaction and differential pressure will decrease, which is reflected by a decrease in the D exponent.

Rehm and McClendon proposed the following correction to allow for mud weight.

Dxc	= Dx	$x \frac{Weq}{ECD}$	where	Dxc	=	corrected D
				$\mathtt{D} \mathtt{x}$	=	D exponent
				Weq	=	normal pore pressure gradient (Equivalent mud weight, ppg)
				ECD	=	effective circulating density

Any negative deviation of the Dxc from a normal trend (based on clean shale points) may be indicative of an increase in pore pressure.

(3) Mud Temperature

Heatflow is generated radially from the Earth's core and is usually constant in any given area across any given increment. This may be true for the average temperature gradient across normally pressured formations, but abnormally pressured formations have been shown to exhibit abnormally high geothermal gradients. The top of an overpressured zone will be marked by a sharp increase in geothermal gradient due to the higher than normal porosity of the formation which reduces thermal conductivity (insulates). The seal above zones of overpressure may exhibit a decrease in the geothermal gradient due to insulating effect of the geopressured zone below and/or due to the greater thermal conductivity of the abnormally compacted seal rock.

The temperature of the drilling fluid at the flowline will be proportional to the geotemperature, but many variables must be taken into account. These variables include the mixing, treatment and addition of new, cooler mud into the circulatory system, pump rate, lag time, ambient temperature, lithology, casing size and length of riser.

Two other methods are also used to obtain geotemperature data whilst drilling. The first is the circulate returns temperature. Returns are usually circulated prior to pulling each bit, and after significant drilling breaks. A plot of these circulated returns temperatures usually provides a better approximation of the geothermal gradient than that obtained from the flowline temperature over the bit run. As with the standard method, recent mud additions can have a serious effect upon the circulated returns temperature.

A further method of obtaining geotemperature data is a survey Temp-Plate. This is a small, heat sensitised strip which is attached to the survey tool. A record of downhole survey temperature can therefore be kept. It has been found that this latter method more closely reflects the true geothermal gradient, although recorded temperature values are lower than true values.

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Wireline log runs present an opportunity to calculate true bottom hole temperatures. By use of a Horner Plot, a method adapted from Horner's bottom hole pressure plots, reasonably accurate true bottom hole temperatures can be obtained. In most cases, the circulation time prior to running wireline logs is recorded. For each log run, time (in hours) since circulation stopped and the maximum bottom hole temperatures are recorded.

The recorded data may then be plotted on semilogrithmic paper, with temperature on the linear ordinate and the dimensionless time factor, Δt on the semilog abscissa (where t = circulation $t+\Delta t$

hours and Δt = time since circulation stopped, hours). A straight line joining the plotted points is extrapolated to the temperature axis and true bottom hole static temperature is read off. (See Figure 1).

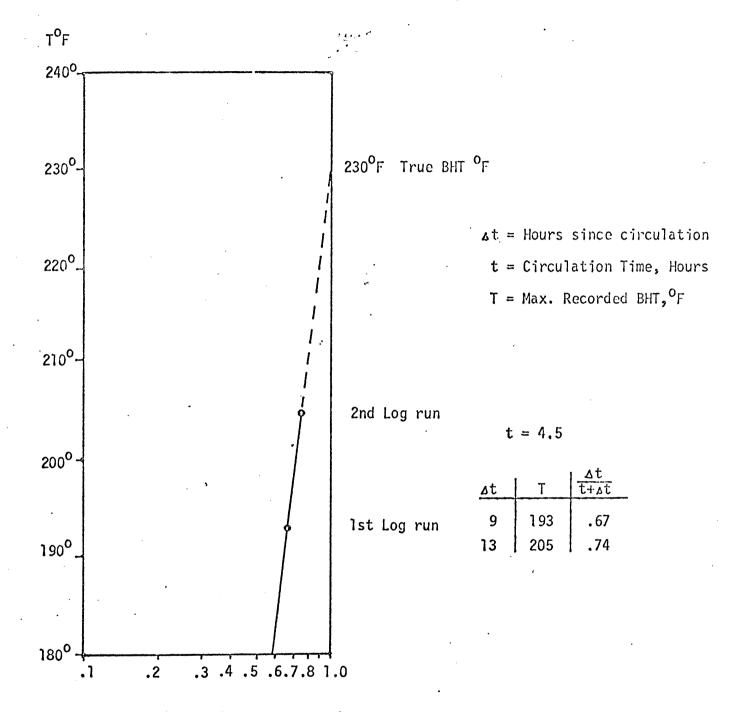
The method fails if circulation and the addition of new, cool mud into the system occurs between log runs.

(4) Gas

The amount of gas detected within the drilling mud at the flowline can be very useful indicator of differential pressure. Background gas values are very important. If the background gas increases with depth in a formation of constant lithology, permeability, and gas saturation with a fixed mud weight, then an increase in pore pressure may be indicated.

Gas magnitude is relative when gas is being used as a measure of differential pressure. Formation permeability and gas saturation must be considered in determining the amount of background gas to be expected while drilling. Low permeability formations are likely to yeild only small amounts of background gas even with high gas saturation. This is also the case for a formation with high permeability and low gas saturation. Refer to Figure 2.

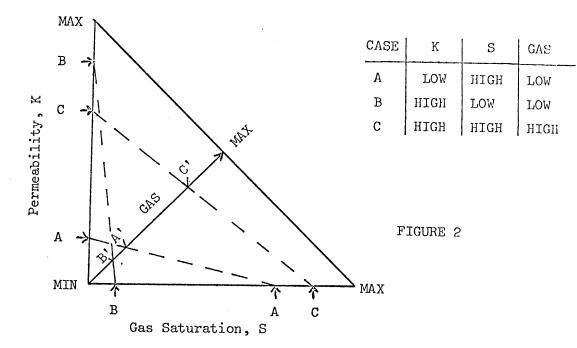
HORNER TEMPERATURE PLOT



<u>At</u> t+st

vii

GAS MAGNITUDE AS A FUNCTION OF SATURATION AND PERMEABILITY



In a low gas saturated formation a slight increase in background gas may be significant while in a high gas saturated formation high background gas may not be significant. Thus, low background gas in low gas saturated or low permeability formations can be expected, even when drilling underbalanced. Disregard of this factor can lead to sloughing, bridging, stuck pipe, or a well kick if gas alone is used for determining an underbalanced hole condition.

The background gas after a gas peak should be compared with the background gas prior to the peak. A higher background gas after a peak than that before the peak may suggest an underbalanced hole condition.

Pore pressures cannot be quantified by gas readings alone, but they can be quantified (provided the above mentioned permeability and saturation factors are taken into account) by a comparison of changes in gas readings with changes in mud weight in hydrocarbon bearing formations.

Produced gas (e.g. connection gas, swab gas and trip gas) are also important factors to consider in pore pressure analysis. Their presence indicates a near balanced hole condition for permeable hydrocarbon bearing formations or even a slightly underbalanced

viii

condition for low permeability hydrocarbon bearing formations.

Connection gas is due to the reduction in differential pressure caused in part by ceasing circulation and in part by swabbing, such that hydrocarbons (or other fluids) are produced (flow into the hole) from the formation.

Swab gas is that gas produced by a formation due to underbalance caused by the upward movement at the drill string. This may be accompanied by pump shutdown (e.g. during connections and trips) or not. There are two types of swabbing, one being the piston type (some part of the drill string acting as a plunger in the bore hole) and the other being the frictional type (friction between moving drill string and annular mud inducing a slight lifting force in annular mud column).

Trip gas is produced gas caused by pump shutdown, pulling the drill string, and lowering of the hydrostatic head (if the hole is not kept full) during a trip.

(5) Shale Density

Shale density in a homogeneous claystone/shale section which has a hydropressure gradient will increase with depth as compaction increases and porosity decreases. Values typically range from 1.7 to 2.7 gm/cc and show a steady rate of increase with depth. Anomalies from this normal compaction trend may be due to mineralogy, e.g., sideritic, dolomitic and calcareous shales exhibit higher than normal values. Sandy, silty shales and soft wet clay will produce further variations.

Geopressure is indicated by a constant or decrease in density with depth reflecting the increased porosity and fluid content. Cap rocks of higher than normal density may be present above this zone of abnormal pressure.

ix

(6) Shale Factor (Refer Figure 3)

During normal deposition of clays, the principle component is montmorillonite. This is a flocculated sheet silicate which has a large capacity to absorb and retain water between the individual molecular sheets and between the flocculate particles. After deposition, montmorillonite undergoes compaction through gravity loading which flushes the intraparticle water into the pore spaces. Providing that the hydraulic conductivity is sufficiently high to remove this water, compaction will continue. The outer layers of water bonded to the clay particles may next be removed as montmorillonite alters diagenetically with depth to mixed-layer clays and finally to illite. This alteration involves compaction of pore spaces, orientation of particles and reduction in inter-layer and intraparticle area, thereby reducing the total area available for chemical absorption. Notes that if the hydraulic conductivity is insufficient to remove the liberated water as it is flushed, then at depth the clays will be abnormally pressured and of a "younger" diagenetic age.

Illite or kaolinite may be deposited as the primary clays. As non-swelling clays they have very little intraparticle water. These clays dewater by loss of interparticle water through compaction. Again, if the hydraulic conductivity of the clays is lower than that required to efficiently flush the water, then these clays will be overpressured. Non-swelling clays, as stated above, are geometrically more compact than their swellable counterparts and therefore originally contain less sites for chemical absorption of free ions.

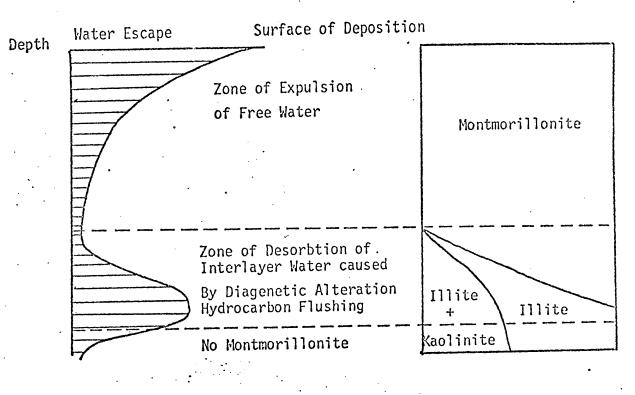
It is the diagenetic state (% montmorillonite) of the clays that shale factor reveals. If a crushed slurry of the shale is titrated with methylene blue solution, the dye will be absorbed onto the available sites by cation exchange mechanisms. The amount of dye required to saturate the cation exchange capacity of the shale will depend upon the latter's geologic maturity.

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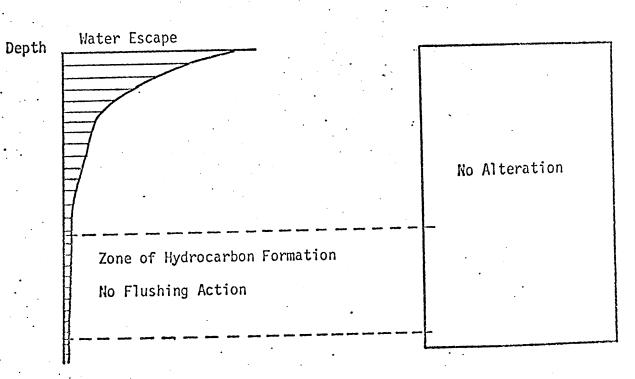
TYPICAL CLAY DIAGENESIS (AFTER MC POWERS (1967) FIGURE 3

1. MONTMORILLONITE

WATER LOSS vs DEPTH OF BURIAL DIAGENETIC HISTORY



2. ILLITE/KAOLINITE



If the principle primary clay is montmorillonite, which undergoes compaction to "mixed-layer" clays and then illite, the shale factor values would initially be high, and would show a steady decline with diagenesis. Overpressured, undercompacted sections would theoretically show an increase of the shale factor due to the increased porosity and hence larger surface areas for cation exchange. Were illite and kaolinite the primary clays, the shale factor would be low initially. In the case of an overpressured section of such clays, the shale factor may show no increase whatsoever. Hence in sections of mature, reworked clays, shale factor may be of little use in the detection of geopressures.

If the geopressures is generated by tectonic forces rather than by abnormal compaction through gravity loading, shale factor ceases to be useful as a pressure indicator.

(7) Hole Condition (Carbide Results, Hole Behaviour, Cuttings Size)

Hole condition has to be used in conjunction with all other data. Tight hole on connections and trips, increased rotary torque, connection gases, swab gases, % and size of cuttings, texture of cuttings (i.e. gumbo or splintery), carbide lag time versus theoretical lag time are all indicators of hole condition and will tend to indicate the presence of abnormal pressure.

B. Pore Pressure Quantification

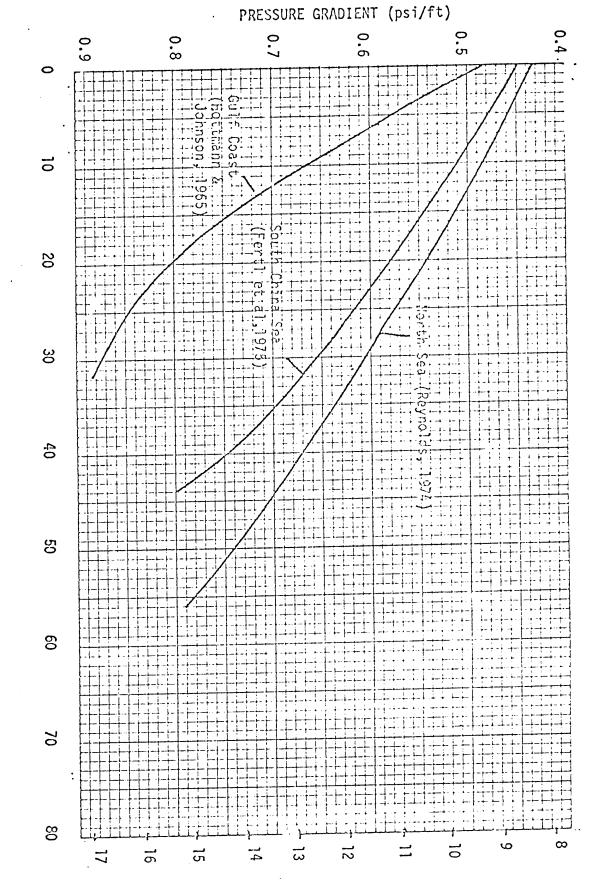
Pore pressure quantification can be made from either empirical data such as tight hole or kick information, or from pressure parameter data such as seismic data (ITT), drilling data including Dxc and cuttings Sh S, and wireline log data including Δt , R_{SH} , Sh S. The quantification of pore pressure from pressure parameter data requires knowledge of the normal pore pressure for the area, the establishment of a normal shale compaction trend line on a plot of the pressure parameter data, and a quantitative relationship between the pressure parameter deviation from normal and the abnormal pore pressure which causes such deviation.

The normal pore pressure for the area can either be assumed to be 8.3 - 9 ppg EMW on a rank wildcat well, estimated from area pressure data, or calculated from wireline log formation salinity data.

All the above mentioned pressure parameters usually increase (Dxc, Sh \mathscr{S} , R_{SH}) or decrease (ITT, Δ t) exponentially with depth in clean normally pressured shales. Thus a best fit line drawn through the normally compacted clean shale points will generally be straight when the pressure parameter scale is log and the depth scale is linear. After a normal trend line has been established, and knowing the pore pressure that this trend line represents, quantification of the pore pressure for abnormally pressured shale points may be made.

It should be emphasised that the above mentioned pressure parameters reflect changes in porosity, and hence compaction only, and do not reflect changes in pore pressure from other causes.

The degree of deviation of a pressure parameter value in shale from the normal trend is usually directly proportional to the amount of pore pressure increase. Several methods have been derived for relating the pressure parameter deviation from normal and the pore pressure change, with each method's reliability being questionable in a new geographical area until supported by empirical data.

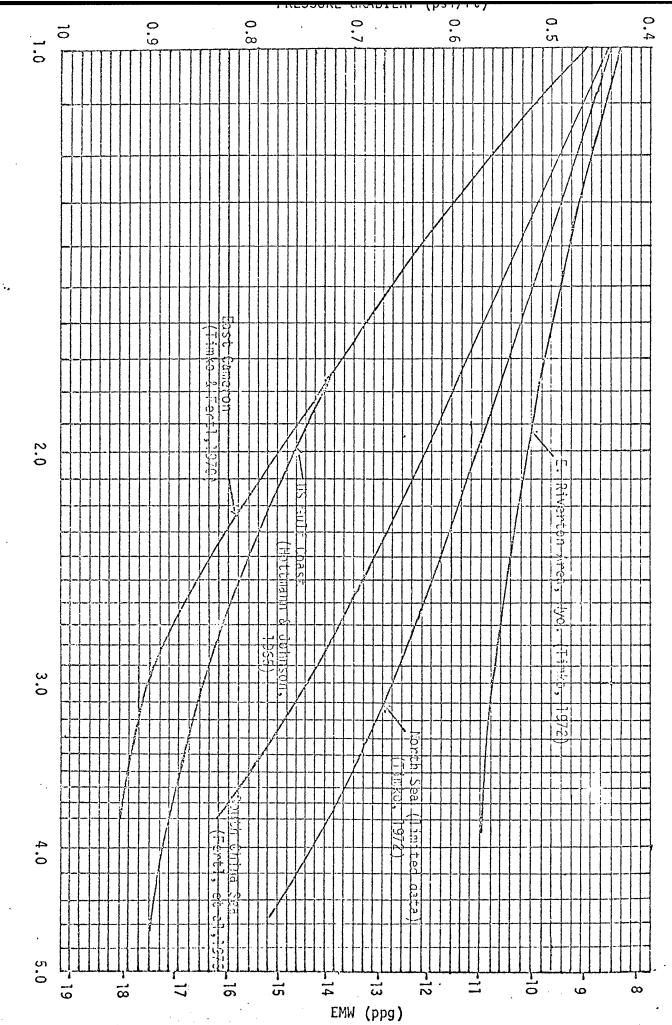


SONIC LOG DEPARTURE VS PORE PRESSURE

EMW (ppg)

X

 $\Delta t_{obs} \Delta t_{norm} \mu sec/ft$



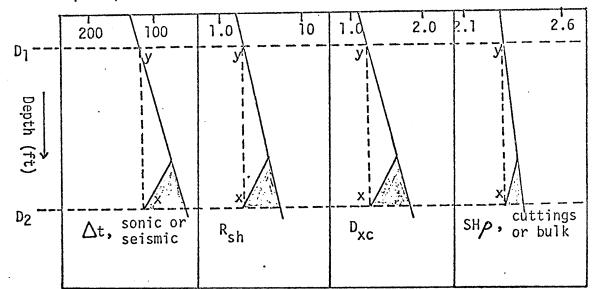
NORMAL R_{sh} / OBSERVED R_{sh}

TAX

SHALE RESISTIVITY RATIO vs PORE PRESSURE

Matrix Stress or Equivalent Depth Method

The matrix stress or equivalent depth method assumes that the part of the overburden supported by the clay matrix will be constant for clays with the same porosity. More precisely it assumes that the rock matrix stress at a particular depth in an overpressured zone is equal to the rock matrix stress at a shallower depth point where the pressure parameter value on the parameter normal trend is equal to the pressure parameter value at the depth of interest in the overpressured zone. In the diagram below point X at the point of interest has the same pressure parameter value as point Y on the normal pressure parameter trend line. With the overburden gradient and normal pore pressure known, the pore pressure at the depth of interest may be calculated as shown.



 $P_2 = D_2 P_2 - D_1 (P_0 - P_1)$

 $P_2 = Pore pressure at D_2, psi$

- D_2 = Depth of interest, feet
- Po2= Overburden gradient at D2, psi/ft

 $D_1 = Equivalent Depth$

 $P_1 = Pore pressure at D_1, a normal gradient, psi/ft$

Po₁= Overburden gradient at D₁, psi/ft

Eaton's Variable Overburden Method

Geopressure magnitude may be calculated from pressure parameter data using the following equations or charts.

1.
$$P/D = S/D - \sqrt{S/D} - (P/D)n \sqrt{7} \times (\frac{Ro}{Rn})^{1.2}$$

2.
$$P/D = S/D - \int S/D - (P/D)n_7 \times (\frac{\Delta tn}{\Delta to})^{3.0}$$

B.
$$P/D = S/D - (S/D - (P/D)n_7 \times (\frac{dc_0}{dc_n})^{1.2}$$

- (P/D)n = Normal water gradient in the area such as 0.465 in and along the Gulf of Mexico, or 0.433 in West Texas, psi per foot

Rn = Shale resistivity from normal line, ohm-meters

Ro = Shale resistivity from well log, ohm-meters

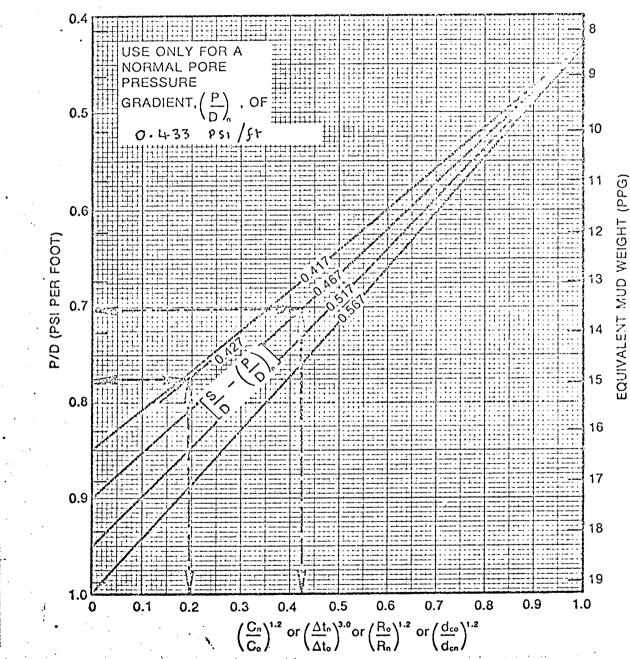
S/D = Overburden stress gradient, psi per foot

Atn = Normal shale travel time, micro-seconds per foot

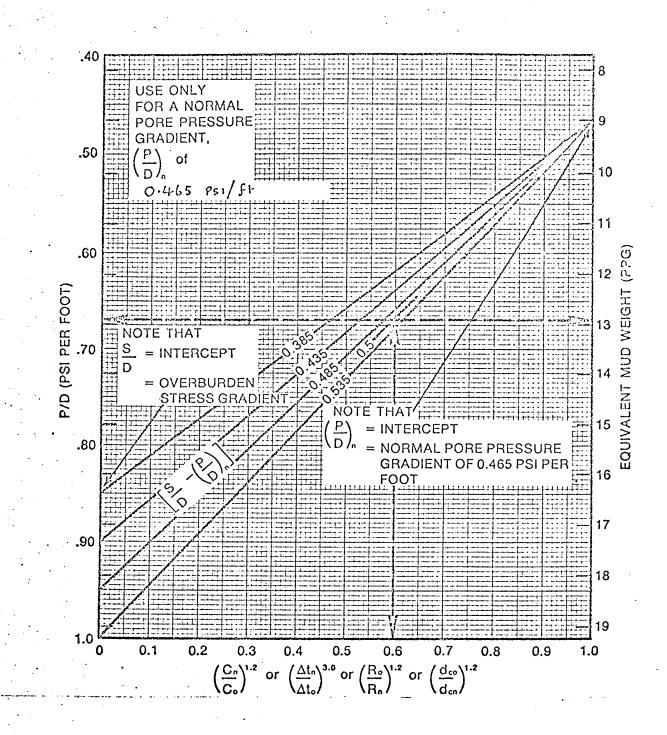
Ato = Shale travel time value, micro-seconds per foot

 $dc_n = Actual d_c$ from trend line

 $dc_0 = Actual d_c$ calculated



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The Dxc compaction trend line is in general parallel to a line joining 1.4 and 1.7 (values of Dxc) 5,000 ft. apart. The quantification of pore pressure from Dxc is most usually effected by using the following equation.

Po = Pn x $\frac{Dxc^n}{Dxc^0}$ Po = Pore pressure at depth of interest (ppg) Pn = Normal Pore Pressure (ppg) Dxc^0 = Observed Dxc at depth of interest Dxc^n = The Dxc value on the trend line at the depth of interest

From this equation overlays can be constructed.

Shale density data is sometimes plotted on a linear-linear plot and sometimes on a linear (depth) log (Sh S) plot. The matrix stress or equivalent depth technique is most usually utilised to quantify pore pressure from this pressure parameter.

C. Overburden Pressure Determination

The average density for each successive 50 feet interval from surface to total depth is obtained from cuttings or, preferably, from the FDC log. The bulk density data are converted from gm/cc to psi/ft to give overburden pressure.

D. Fracture Pressure Determination

Both empirical and theoretical methods are utilised to determine the fracture pressure of the formation. Empirical data from loss circulation and formation integrity tests are the most reliable. Fracture data from well histories can be very beneficial. The following theoretical methods are currently accepted:

a) HUBBERT AND WILLIS

$$\frac{Fp}{D} = \frac{Pp}{D} + \frac{1}{3} \left(\frac{Po - Pp}{D} \right) \dots \min$$
$$= \frac{Pp}{D} + \frac{1}{2} \left(\frac{Po - Pp}{D} \right) \dots \max$$

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Where Po is unknown an approximation of Fp can be derived making Po = 1.0 thus:

$$\frac{Fp}{D} = (1 + \frac{2Pp}{D}) \frac{1}{3} \quad \dots \quad \min$$

= $(1 + \frac{Pp}{D}) \frac{1}{2}$ max

b) MATHEWS AND KELLY

$$\frac{Fp}{D} = \frac{Pp}{D} + \frac{Ki(Po-Pp)}{Di}$$

Where Di = D in normally pressured sections. If the formation pressure is greater than normal then:

Di =
$$\left(\frac{\frac{Po}{D} - \frac{Pp}{D}}{\frac{Po}{D} - \frac{Pn}{D}}\right) D$$

Ki is a variable matrix stress coefficient i.e. A variable horizontal to vertical stress ratio back calculated or using Gulf Coast and West Texas Data represented as a curve of Di versus Ki.

c) EATON

$$\frac{\text{Fp}}{\text{D}} = \frac{\text{Pp}}{\text{D}} + (\frac{\text{v}}{1-\text{v}})(\frac{\text{Po} - \text{Pp}}{\text{D}})$$

Where v is Poisson's ratio, either back calculated or using original Gulf Coast Data, a curve of <u>Po</u> versus v.

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d) ANDERSON, INGRAM AND ZANIER

$$\frac{F_{D}}{D} = \frac{P_{D}}{D} \left(\frac{1-3v}{1-v}\right) + \frac{P_{O}}{D} \left(\frac{2v}{-1v}\right)$$

Where v is Poisson's ratio, either back calculated for a given area or using original Gulf Coast data of v versus a formation shaliness index.

Symbols	used	
Fp	=	Fracture Pressure, psi
Ро	=	Overburden Pressure, psi
Рр	=	Formation Pressure, psi
Pn .	=	Normal or Hydropressure Graident, psi/ft
D	=	Depth, ft

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A P P E N D I X B

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INSTRUMENTATION AND DATA COLLECTION METHODS

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INSTRUMENTATION AND DATA COLLECTION METHODS

INSTRUMENTATION -

The Gemdas Level VI system consists of the following equipment packages:

- a) Two Hewlett Packard 21MX, 36K memory computer systems with associated link tape drives, operator consols, printer-plotter outputs and remote video display units. One system is online and the other is used for offline work and as a backup in the event of breakdown.
- b) Drill Monitor System (DMS Mk II) which monitors the drilling variables hook load, weight on bit, rotary RPM, total bit revolution, depth, kelly height, drill rate, torque, pump and casing pressures. The system monitors displays and records these variables and feeds them to the online computer system for analysis and final tape storage.
- c) Mud Monitoring System for recording total and individual pit volumes, mud weights in and out, mud temperatures in and out and pump flow in and out. These variables are also linked to the online computer.
- d) Gas detection system for the analysis of mud stream and blendor gases which includes the standard hot wire detectors for total gas and petrol vapours; standard chromatograph for hydrocarbons C_1 through C_5 ; FIDflame ionization detectors for total gas and C_1-C_5 for high percentage of these gases which would saturate a normal system; a thermoconductivity chromatograph for the detection of non combustible gases; and a H₂S detection system.

SOFTWARE CAPABILITIES -

The Gemdas System incorporates software capabilities that have been developed to monitor drilling operations, aid in drilling control and pressure detection and provide a permanent easy-recall record of all pertinent drilling data. The following basic units are involved:

- a) The drill monitor program which reads the various DMS equipment during drilling to provide a continuous readout of drilling variables. The program also computes such parameters as cost per foot, estimated tooth wear, Dxc and estimated pore pressure over a fixed depth or time interval.
- b) The trip monitor program which provides a critical monitoring of all necessary parameters during trips on a continuous real time basis. By monitoring the number of stands the program computes expected hookload and pit level and compares these with the actual values. Pipe running speed, surge pressures and estimated completion time are also computed and displayed.
- c) The kick and kill monitor program provies a valuable method of analysing a kick situation. The program can be run prior to killing the well to compute the results of various kill mud weights and pump rates. The program also monitors and records the actual kill procedure.
- d) Data Collection:

The complete drilling data for Fortescue No. 2 is stored on data tapes 1. to 3.

Tape 1	256 m	to	1408m
Tape 2	1408 m	to	2435m
Tape 3	2435 m	to	2653m

A complete printout of this data is presented in Appendix E and selected parameters have been plotted on a 1:1000 scale and presented in Appendix F.

Handplots on a 1:2500 scale of drill rate, Dxc, background gas, shale density and mud temperature are presented in Appendix D.

APPENDIX C

MANUAL PLOTS AND CHARTS -

- (i) Drilling Data Pressure Log
- (ii) Temperature Data Log
- (iii) Pressure Analysis Log

A P P E N D I X D

COMPUTER PRINTS (+) AND PLOTS (X) -

+ (i) Drilling Data Printout

+ (ii) Hydraulics Pressure Loss Data Printout

x (iii) Drilling Data Plot 1:1000

(i) DRILLING DATA PRINTOUT

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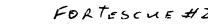
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(ii) BOREHOLE HYDRAULICS PRESSURE LOSS DATA PRINTOUT



alle in the lines of a second state of the second second second second second second second second second secon FORTESCUE No. 2 - 390m 1 NOVEMBER 1978. PRESSURE LOSS ANALYSIS a na anti-a contra da seconda da s DATA: DEPTH = 1283.0 (VERTICAL = 1283.0), RPM = 120 PUMP PST = 2580, MUD we IGHT = 9.30 MUD FLOW RATE = 1030, DRILL RATE = 600.0, BULK GM/CC = 2.50 n RHEOLOGY: K LOW 1.955 .399 MID 1.955 .399 PV = 7.0, YP = 15.0RFACE PRESSURE LOSS WEFFICIENT = 3 ASIC RESULTS: 453 BBLS, 2543 CUBIC FT. HOLE VOLUME ANNULAR VOLUME 407 2283 1283 VERPICAL DEPTH FORMATION FLUID DEPTH 102 610

 HY LROSTATIC FS1

 MUD CYCLE TIME (MIN)
 17

 NOZZLES (1/32 INCH):
 20.00 20.00

 359 FT/SEC
 359 FT/SEC

 HYLROSTATIC PSI 20.00 20.00 JET PRESSURE LEUP 645 BIT HYLKAULIC HP 1780 IMPACT FORCE (Lb) SURFACE ISI LOSS 112

FROM DEPTH OF 835 TO 1283 ft

American and the second

LENGTH: 448 ft

DIAWETERS: ANNULUS = 17.500, PIPE 1D, OD, JD = 2.813 7 750 7 750 inches

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	_ in#	660.4	IURBULENT			
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ANNULUS			14,031			
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LENGTH: 67 f DIAMETERS: ANNULUS DOWNHOLE	Et = 17.500,	PIPŁ ID, OD, J 1380.8 ft/min	D = 4.276 5.000	6.500 inche	5	n an
LENGTH: 67 f DIAMETERS: ANNULUS DOWNHOLE VELOCITY: 23.0	<pre>Et = 17.500, 0 ft/sec,</pre>	1380.8 ft/min BINGHAM	D = 4.276 5.000 POWER LAW	6.500 inches	n,	n an
LENGTH: 67 f DIAMETERS: ANNULUS DOWNHOLE VELOCITY: 23.0 REYNOLDS NUMBER:	<pre>ft = 17.500,) ft/sec,</pre>	1380.8 ft/min BINGHAM 121352	le and the concernence and along the second second second	6.500 inches	5	t i son transformer State State States State State States
LENGTH: 67 f DIAMLTERS: ANNULUS DOWNHOLE VELOCITY: 23.0 REYNOLDS NUMBER: CRITICAL VELOCIT	Et = 17.500,) ft/sec, Y: fpm	1380.8 ft/min BINGHAM 121352 300.2	POWER LAW	6.500 inches	5	n - an sea Saintean Saintean
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LENGTH: 67 f DIAME TERS: ANNULUS DOWNHOLE VELOCITY: 23.0 REYNOLDS NUMBER: CRITICAL VELOCIT FLOW REGIME: PRESSURE LOSS:	<pre>ft = 17.500, 0 ft/sec, Y: fpm psi</pre>	1380.8 ft/min BINGHAM 121352 300.2 TURBULENT 13.2	POWER 1Aw 34132 322.5 TURBULENT 8.6	6.500 inches	5 5	n o an o gui
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<pre>Y: fpm psi psi/100ft S S 31,ft ft = 21.200,) >ft/sec, 1:</pre>	BINGHAM 21510 292.0 LAMINAR 2.1 .475	12.785 FOWER LAW 427 266.7 LAMINAR .6 .146 JD = 4.276 5.000	nen a ser en en en en en en en en en en en en en		
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<pre>Y: fpm psi psi/100ft S S 31,ft ft = 21.200,) >ft/sec, 1:</pre>	292.0 LAMINAR 2.1 .475 PIPE ID, OD, . 380.8,ft/min	266.7 IAMINAR .6 .146	1800	n olice ngender networks in eine – in de andre eine state in eine state in eine state andre eine state in eine state in eine state	
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		POWER LAW		A.W. 1	
	121352	34132			
Y: fpm	300.2	322.5			
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psi Acces	Solar March 1997 - 1997 - 1998 - 2008 - 2008 - 2008 - 2008 - 2008 - 2008 - 2008 - 2008 - 2008 - 2008 - 2008 - 2	and the second		• • • • • • • • • • • • • • • • • • •	
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	BINGHAM	•	POWER		
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CI, lb/gal	9.20 9.26				
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	psi/100ft ft/sec, 59 Y: fpm psi psi/100ft S S BIT ENSITY,,16/ CT, 16/gal DR MUD WI	psi/100ft 19.750 ft/sec, 59.5 ft/min BINGHAM 19805 Y: fpm 291.6 IAMINAR 291.6 psi 1.4 psi/100ft .413 BINGHAM 112 S 825 1073 7 2580 563 BIT 617 ENSITY,, 1b/gal 9.20	psi/100ft 19.750 12.785 ft/sec, 59.5 ft/min FOWER LAW 19805 319 Y: fpm 291.6 257.2 LAMINAR LAMINAR LAMINAR psi 1.4 .4 opsi/100ft .413 .110 BINSHAM 112 S 825 1073 7 2580 563 BIT 617 ENSITY, , 1b/gal 9.26 OR MUD WI 9.30	psi/100ft 19.750 12.785 ft/sec, 59.5 ft/min BINGHAM FOWER LAW 19805 319 Y: fpm 291.6 257.2 LAMINAR LAMINAR psi 1.4 .4 psi/100ft .413 .110 BINGHAM .805 .110 S 825 .431 1073 1073 1073 7 2 .2580 2580 2560 2560 563 962 .12 BIT .617 .612 LNSITY,, 1b/gal 9.26 .19 .0R #UD WI 9.30 9.30	psi/100ft 19.750 12.785 ft/sec, 59.5 ft/min BINCHAM FOWER LAW 19805 319 Y: fpm 291.6 257.2 LAMINAR LAMINAR psi 1.4 .4 psi/100ft .413 .110 POWER / LAW S 825 112 112 S 825 1073 1073 1073 1073 7 2 2580 2580 563 962 BIT 617 612 9.19 CT, 1b/gal 9.26 9.19 OR MUD WF 9.30 9.30



FORTESCUE No. 2 - 878 m 2 NOVEMBER 1978

PRESSURE LOSS ANALYSIS

DEPTH = 2880.0 (VERTICAL = PUMP PSI = 2320, MUD WEIK	= 2880.0), RPM $= 120GHT = 9.30$	ميريو و در من مدينية مريد و دري درين در ه
1 1 455 300		
CE PRESSURE LOSS CUEFFICIENT RESULTS:	T = 3	
	DEPTH = 2880.0 (VERTICAL PUMP PSI = 2320, MUD WEIF MUD FLOW RATE = 1040, DR OGY: K n W 1.955 .399 L 1.955 .399 = 7.0, YP = 15.0 CE PRESSURE LOSS (DEFFICIENT	W 1.955 .399 L 1.955 .399 = 7.0, YP = 15.0 CE PRESSURE LOSS COEFFICIENT = 3

4

FORTESCUE #2

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HOLE VOLUME	928	BBLS,		CUBIC F	r.
ANNULAR VOLUME	843		4732		
VERFICAL DEPTH	2880	1997 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 -			
MUD HYDRUSTATIC DEPT	a 2860				
FURMALION FLUID LEPTH	i .102				
HYDROSTATIC FSI	1360		· ·	1999年1月,11年1月。	• • • • • • • • • • • • • • • • • • •
MUD CYCLE TIME (MIN)	36				
NOZZIES (1/32 INCH):	20.00	20.00	20.00		
JET VELOCITY	363	FT/SEC		. قىرى	2
JET PRESSURE DROP	1094				
BIT HYDRAULIC HP	664				
MPACI FORCE (LL)	1614	analasi di sunan sunan suna	e, edución posto entre en el co	و با معنون من الم	ay may an an ar ar ar ar ar
SURFACE PSI LOSS	114				
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FROM DEPTH OF 2432 TO 2880 ft

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LENGTH: 448 ft and the second se

DIAMETERS: ANNULUS = 17.500, PIPE ID, OD, JD = 2.813 7.750 7.750 inches DOWN HOLE VELACTIVE. 53 7 ft/sec 3221 5 . f+/min

	3221.5 ft/min	
	BINGHAM	POWER LAW
REYNOLDS NUMBER:	186256	112176
CRITICAL VELOCITY: fpm	306.4	357.9
FLOW REGIME:	IURBULLNT	TURBULENT
PRESSURE LUSS: psi	672.0	328.9
psi/100ft	: 150.001	73.409
ANINUEUS		
VELOCITY: 1.7.ft/sec,	103.5 ft/min	
	BINGHAM	POWER LAW
REYNOLDS NUMBER:	20750	621
CRITICAL VELOCTIY: frm	293.6	295.2
FLOW REGIME:	LAMINAR	LAMINAR

a")	psi/100tt	.692	. 284		5
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PRESSURE LOSS AN	NALYSIS			ร สารสมับ ให้ปี สนุขโรสารใหญ่ สารชิญชีวิธีบรรมสรรม สาร เทริจาร์ของเห็บเหตุ	anest stepping of the stepping
FROM DEPTH OF 76	58 IO 2432)ft	and a substantial and a substantial data for a substantial substantial data and a substantial data and a substa	าสขัสหรัฐอาสุการ: กิสของ ราสุการกระหาร์ คอ กรุงอุละ สงขาง	ి. ఇప్పకు పోలాకుకురింగి కె.రె.్. ఆర్.కె.రె.ల్ లా రె. రె. రె. రె. రె. రె. రె. రె. రె. రె.	alman (j. 1924). S. (min sydropologialaethautha
LENGTH:	1664 ft				
	NULUS = 17.500, PI	PE ID, OD, JD	= 4.276 5.000 (6.500 inches	
DOWNHOLE VELOCITY:	23.2 ft/sec, 139	4.2>tt/min INGHAM	PERSONAL OF THE CARACTER OF THE COLOR OF THE CARACTER OF THE O	தன்கதார் வலைவலாம் பிருதாக மாட்டி படித்துக்குத்தத்தை நது	an anglari sangangkangkangkangkangkangkang sa
FLOW REGIME	JMBER: ELOCITY: fpm C: TUR	122530 300.2 BULENT	34664 322.5 TURBULENT		
ANNULUS	55: psi psi/100ft		215.9 12.972	enter orreante e conserva e conseguero da e	
VELOCITY: REYNOLDS NU	MBER:	INGHAM 23286	POWER LAW 561		
CRITICAL VE FLOW REGIME PRESSURE LO		292.5	275.5 LAMINAR 3.1 .188	agawa ka ye ya ya ke	с. _С . н. с. в.
FROM DEPTH OF 33	31 TO 768)ft		ትት የሚያቸው የሚያት የሚያት እንዲ የትርጉ እንግ እንግ የትርጉ እንግ የመንግ እንግ እንግ እንግ እንግ እንግ እንግ እንግ እንግ እንግ እ	1999 (B. 1997) - Elit Salandar, 2007 (1994) - 27 Sand (1997) - 17 (1997) - Alfred Salandar, Barrya, Barrya Sal	ೆ ಗೋರಿ ಈ ಕೈ ಸಿಗಿಕೊಂಡಿಯಿಂದ ಮುಸ್ತಾನ ಕ
)LENGTH:	437)1t				. •
DIAMETERS: ANN DOWNHOLE VELOCITY:	ULUS = 19.124,		= ∘4.276 ∞ 5.000 ∞ 6	.500 inches	na cana, sa kana ana ara sa sa ang
	В	INGHAM	POWER LAW		
	LOCITY: fpm	122530 300.2	34664 322.5		
CRITICAL VE FLOW REGIME PRESSURE LO	LOCITY: fpm	300.2 BULENT 87.8	322.5	and the second second second second second second second second second second second second second second second	
CRITICAL VE	ELOCITY: fpm : TOR SS: psi psi/100ft 1.2 ft/sec, 74.8	300.2 BULENT 87.8 20.097	322.5 'IURBULENT 56.7 12.972	and the second second second second second second second second second second second second second second second	
CRITICAL VE FLOW REGIME PRESSURE LO ANNULUS VELOCITY: REYNOLDS NU	ELOCITY: fpm : TOR SS: psi psi/100ft 1.2 ft/sec, 74.8 MEER: ELOCTIY: fpm : L	300.2 BULENT 87.8 20.097 ft/min	322.5 TURBULENT 56.7 12.972 POWER LAW	ante es se se se	• •



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PRESSURE LOSS ANALYSIS

LENGPH: 3	31)ft				
DIAMETERS: ANNULL				6.500 inches	
		1394.2 tt/min	μαφφαλφόζα β (μ.ε.ε. τι ζενειτώδαειακτου).	്റ്റുള്താം നോന്നും പുംത്രത്താം പുംത്രത്താം പ്രത്യാത്താം പ്രത്യാത്താം പ്രത്യാത്താം പ്രത്യാത്താം പ്രത്യാത്താം പ്	u, e se se serendendende
	•	BINGHAM	POWER LAW		
REYNULDS NUMBE	R:	122530	34664		
CRITICAL VBLOC	ITY: →fpm	300.2	322.5		
FLOW REGIME:	-	TURBULENT	TURBULENT		
PRESSURE LOBS:	an psi maa a		42.9		·
	psi/100ft	20.097	12.972		•
ANNULUS		· · ·		40 ×	
VELOCITY: 1.	0 it/sec, (50.1 ft/min			
		BINGHAM	POWER LAW		
REYNOLDS NUMBE		19998	324		
	1IY: fpm	-291.6		and a second product of the second second second second second second second second second second second second	* y x = ×*
FLOW RELIME:		LAMINAR	LAMINAR		
PRESSURE LCSS		1.4	.4		
	psi/100ft	.413	.110		
	ور جون مرت خي خي مارد بين من من الله م	ی بین بود بود بند بین بود بی بین زند بی بی بی بی بی بی ب			
SUMMARY:					

TOTAL SURFACE LOSS	BINGHAM	POWER LAW
	114	114
TOTAL DOWNHOLE LOSS	1161	644
TOTAL BIT LOSS	1094	1094
TOTAL ANNULAR LOSS		
PUMP PRESSURE	2320	2320
UNACCOUNTED LOSSES	-64	463
CIRCULATING PSI AT BIT	1396	1386
EQUIVALENT CIRC. DENSITY,)1b/gal	9.34	9.27
ECD W/CUTTINGS EFFECT, 1b/gal	9.34	9.27
Contraction of the second state of the FOR MUD. WI compared		9.30

FORTESCUE NO. 2 - 1135 m 4	4 NOVEMBER 1978		7
PRESSURE LOSS ANALYSIS		TOR TESCU	E#Z 4Nor
LATA: DEPTH = 3772.0 (VERTICA PUMP PSI = 850 , MUD WE	IGHT = 9.15		
MUD FLOW RATE = 505, L RHEOLOGY: K n LOW 1.228 .466 MID 1.228 .466 FV = 8.0, YP = 13.0	KILL KATE = JU.U,	$\mathbf{BUIK} \; \mathbf{GW} \; \mathbf{CC} = 2.25$	· · · · · · · · · · · · · · · · · · ·
SURFACE PRESSURE LOSS COEFFICI BASIC RESULTS:	ENT = 3	า มีสีรีสีมภูร์สูงใหม่เห็นสูงสร้างการสรดสรางการสรดสรางสรางสรางการการการการการการการ	gentin oneann i commanne ne coisge e est or ben suiter.
HOLE VOLUME ANNULAR VOLUME VERTICAL DEPIH	668 BBLS, 558 3772	3751 CUBIC FT. 3134	
MUD HYDROSTATIC DEPTH FURMATION FLUID DEPTH HYDROSTATIC PSI	3752 3752 102 1782	gippung punpara ganakargangangan kanaka ang saka sara s	n an an an ann an an an an an an an an a
MUD CYCLE TIME (MIN) NOZZLES (1/32 INCH): JE4 VELCCIAY	52	18.00	
JET PRESSURE DROP BIT HYLRAULIC HP IMPACT FORCE (L5)	387 114 520	an gent see ee eense sense sense oor oor oor oor oor oor oor oor oor oo	ار اینان پر برای از داران میشوند. ا ^{یر} دینده داران ایر ایر
SURFACE IS1 LOSS	29		
FROM DEPTH OF 3234 TO 3772 ft	en fan de fan de fan de fan de fan de fan de fan de fan de fan de fan de fan de fan de fan de fan de fan de fan	รี ซีนี่ เหตุการที่เสียงไปการที่ 2 ได้เหตุดสุดอาณิสตรา (an an an an an an an an an an an an an a
LENGIH: 536 ft			
отделятеся: аммитик = 12 250.	PTPE THE ON SID	= 2 812 7 750 7 750 i	nchor

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DOWNHOLL VELOCITY: 26.	lft/sec, 1	L564.3 ft/min	
		BINGHAM	POWER LAW
REYNOLDS NOMEER	nn instill		35386
CRITICAL VELOCI		291.7	328.8
FLOW REGIME :		URBULENT	IURBULENT
PRESSURE LOSS:	DSI	222.9	147.2
	psi/100ft	41.429	27.367
ANNULUS			
VEICU11Y: 2.3	ft/sec, 1	37.5 ft/min BINGHAM	POWER LAW
REYNULLS NUMBER		10951	848
CRITICAL VELOCT.		283.7	329.0
FLOW REGIME:	rr. rban	LAMINAR	TAMINAR
PRESSURE LASS:	psi	7.2	4.2
THEFT	psi/100ft	1.344	.781
	میں برنے میں برنے میں میں میں میں میں میں میں ا	ار خار خار کا دارد دی می می بید بین بین بین می می م	
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M DBPTH OF 2824 TO 3234 ft	가 가지 있다. 특히 가 있다. 가지 가지 않는 것이 가지 않는 것이다. 				× .
LENGPH: 410 ft	•	ang berna tana kang baran sa sa sa sa sa sa sa sa sa sa sa sa sa	un i ug daa anaa saagaa da ayagaa ya aha	ngelgeene op in terministen in Station of	earlien was earlightig
METERS: ANNUGUS = 12.250,)	PIPE ID, W, JI	$J = 4.270 \ J.000$	0.500 Inches		
VELOCITY: 11.3 ft/sec, 6	577.0 ft/min				
	BINGHAM	HOWER LAW			-
REYNULDS NUMBER:					
CRITTCAL VELOVITY • Frm	28A A	289.6	an in the second states of the states of the second	ವರ್ಷ-ನಿಯ್ದೆ ಕ್ರೀಟ್ ಕ್ರಮ್ಮ ನಿರ್ದಾರಣ ನಿರ್ದಾರಣ ನಿರ್ದಾರಣ ನಿರ್ದಾರಣ ನಿರ್ದಾರಣ ನಿರ್ದಾರಣ ನಿರ್ದಾರಣ ನಿರ್ದಾರಣ ನಿರ್ದಾರಣ ನಿರ	(1,9%)
FLOW REGIME: 1	URBULENT	IURBULENT			
PRESSURE LOSS: psi	22.8	19.1			
psi/100ft	5.551	4.663			
ANNULUS					
, VELOCITY: 1.6 ft/sec, 99		n ang kan	t i sanang a nagnata itali kitu i	New States State (Sciences States 1996)	in or a substance of
	BINGHAM	POWER LAW			
	12697	645			
CRITICAL VELOCTIY: fpm	278.7	283.0			
	LAMINAR	LAMINAR			
psi/100tt		.330	and the second second second	برايح المعترية بالا	ang tan kana
PRESSURE ILSS: psi psi/100ft 	3.3 .614		1.4 .330		
MIN 2024 . FE	in i an gerief. 1995 - State Constanting and an an an an an an an an an an an an an				
2824 ft					
LENGTH: 2493 ft	e to for the set of the set of the set of the set of the set of the set of the set of the set of the set of the	e i kon y konstructione konstructione e	en en en en en en en en en en en en en e	$(x,y) \in (\mathbb{Z}_{p+1}) \times (w_1,y_2,y_3,\dots,y_n) \qquad (1,2)$	a ta se sa se se

VEICCITY: 11.3 ft/sec, 677.0 ft/min HING HAM

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1992 - 1992 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 -

REYNOLLS NUMBER: CRITICAL VELOCITY: fpm FLOW REGIME: PRESSURE LCSS: 1051 051 psi/100ft		11897 289.6 TURBULENT 116.3 4.663		a
ANNULUS VELOCITY: 1.5 ft/sec, REYNOLDS NUMBER: CRITICAL VELOCTIY: fpm FLOW RESIME: PRESSURE LLSS: psi	92.3 ft/min BINGHAM 12434 278.4 LAMINAR 19.3	POWER LAW 593 278.7 LAMINAR 7.4	nga uga ku – singa anggapaka ku nunga ga bab unan naga nunganakak	блайна — на сякульта уб. на наймайтарана ий
psi/100ti	- Construction of the Second S Second Second S Second Second S Second Second S Second Second Seco	. 297 ^{***} • 297	ுலையுக்கு குறைப்பட பியல்றதுத்து கொண்டுத்து	※ (あかだ) いかだいた (新生社的2)) (数 380×1) いた
	a for each of the second second second second second second second second second second second second second s	and the second se	neordar in farithe du id nigeranning, e nig unnaffin edarad.	a a wa wa naurata an kiloni dhamanikila ikilon
		Martinda and a start start of a start o		and advantantical states and advantages by
PRESSURE LOSS ANALYSIS FROM DEPTH OF 0 TO 331 tt		in an	lan manufas rusta lan mangan din asalas a nasas k	unann
LENGTH: 331 ft DIAMETERS: ANNULUS = 21.200 DOWNHOLE VBLCCITY: 11.3.ft/sec, REYNOLDS NUMBER:	677.U/it/min BINGHAM	JD = 4.276 5.000 POWER LAW 11897	6.500 inches	nigur 19640 - 14 oktoberðin gunts försaustur
CRITICAL VELOCITY: fpm FLOW REGIME: PRESSURE LOSS: psi	284.4 TURBULENT 18.4 t 5.551	289.6 TURBULENT 15.4 4.663	ng an an ang ang ang ang ang ang ang ang	i Generative of the state of th
REYNOLDS NUMBER: CRITICAL VELOCTIY: fpm FLOW REGIME: PRESSURE LOSS: psi psi/1001	BINGHAM 8360 274.3 LAMINAR 1.2	POWER IAW 146 219.3 LAMINAR .2 .057	 Contraction (1996) Contraction (19	, τ _{ηδ} φ(1 41.2) - ε - Εξε Φιττρ, 903 - Νθβοθβορία του Ο Αλαγγού - Αλαγγού - Αλαγγού - Αλαγγού - Αλαγγού - Αλαγγού - Αλαγγού - Αλαγγού - Αλαγγού - Αλαγγού - Αλαγγού -
Brief Landowskie American (1994) - 1994 - 1996 - 1996 - 1996 - 1996 - 1996 - 1996 - 1996 - 1996 - 1997 - 19 - 1997 - 199 - 1997 - 19	BINGHAM)FOWER LAW	naad service Scans an naaeseg (opplicatings voe sowe

	BINGHAM	POWER LAW
TOTAL SURFACE LOSS	29	25
TOTAL DOWNHOLE)LOSS	402	in the information of the presentation of the two structures 298
TOTAL BIT LASS	387	387
TOTAL ANNULAR LOSS	3 1	13
HUMP PRESSURE	850	850
UNACCOUNTEL LUSSES	1	123
CIRCULATING EST AT BITT	ไม่จ	1795

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EQUIVALENT CIRC. LENSITY, ID/GAL ECD W/CUTTINGS EFFECT, TD/GAL FUR MUL WI	9.26 9.26 9.15	د .د 9. ا 9. ا	.7
		μποι κα ν του ματομού τραγοριατικά το του και το Νουρία η επισμότια ει απόρησα του Αλάβουρου Το μουρία Το το διατισμού του το το το του το του του του του του	ನ ದೆಯಾಗಿಕೆಯನ್ನು ಬಂದು ಬಿಂದು ಬಿಂದು ವಿಷಯಿತ್ರಿ ಕೇಳಿದರು. ಬಿನೆಗಿ ಕೊಡಿಸಿದ್ದಾರೆ. ಇದು ಸೇರಿ ಕೊ
	Anna alato Barto agan Marasan		

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. ACTIVE CONTRACTOR	NATION AND AND AND AND AND AND AND AND AND AN	9 1996 1916 19 7 47	19 VAUKO 80 VI. Gotenna meniat

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FORTESCUE No. 2 - 1374 m 5 NOVEMBI	R. 1978 - 1979 - 197	andelan companyation and the device of a contract of an anti-	n – mannatoninska soviten o om det støddi vils val høldestaden sæster i sov
0 PRESSURE LOSS ANALYSIS			
DATA: DEPTH = 4508.0 (VERTICAL = 4508)	ау ула мар, алт - посаналарос у нача муру данадаанала дона . О) RPM = 120	nasis (os), nasistabilitatumatatumikkat kilae° (nasisten asist) (os) un un	n aanalaa in gaara ahaa ku in taali in taali in taali in taala ka ka ahaa ahaa ahaa ahaa ahaa ahaa
PUMP PSI = 2730, MUD WEIGHT = 1 MUD FLOW RATE = 950, DKILL RATE	9.10	2.20	
RHEOLOGY: K n	sefliggericanticale or measurgegere at the anterior of the second second second second second second second se	alipati i wina an ne interventive de la Salenta di S	ութերութել ու մարի տարի չուքի հանրել է է ու նուն ու հետանում եր տարումը է նետնո
LOW 1.684 .415 MID 1.684 .415 PV = 7.0, YP = 14.0			ر دی
SURFACE PRESSURE LOSS COEFFICIENT = 2 BASIC RESULTS:			
	BBLS, 4354 CUBIC F 3636	T.	anunding an in for u i ang ang ang ang ang ang ang ang ang ang
JET VELOCITY 409 JET PRESSURE DROP 1361	18.00 18.00 FT/SEC	αν τημαδικά μεταγγάζει το ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά Το ποιοιοιοιοίο ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά ματαγγά	, 2000), 2000 states in the states of the
BIT HYDRAULIC HP 754 IMPACT FORCE (LB) 1829 SURFACE PSI LOSS 63	ชีพิพิพ มีมหาสิญญาและคายที่กระสติตต่าง สูงที่หมา 56.47 ค.ศวกรสอกรรค พ.ศ.ศร 	s monarco margine margine managenzano presionamo o margino (como	က္မမားက က်က္ကားေလး လွေ့ရက ဆားက်က္ကားက ခုန္ပင္းက်က္နဲ့ က်က္ကား က်က္ကားကို က်က္ကားကို က်က္ကားကို က်က္ကားကို က်က္ကားကို က်က္ကားကို
FROM DEPTH OF 3970 TO 4508 ft	観光 記録の記 見ために ふうしつかれてい シューマント・マーマン マーマー		
LENGTH: 538 ft		na fina fina an an an an an an an an an an an an a	Min Managaran Karaka Ing Karakan Karakan Karakan Karakan Karakan Karakan Karakan Karakan Karakan Karakan Karaka Karakan Karakan br>Karakan Karakan
DIAMETERS: ANNULUS = 12.250, PIPE 11 DOWNHOLE		0 7.750 inches	
VELLCITY: 49.0 ft/sec, 2942.8 f BINGHA		an an an an an an an an an an an an an a	
REYNOLDS NUMBER: 16647 CRITICAL VELOCITY: fpm 300. FLOW REGIME: TORBULEN PRESSURE LOSS: psi 673.	9 97771 1 347.0 T IURBULENT		

	VELOCITY: 4 REYNOLIS' NOME CRITICAL VELOU FLOW REGIME: PRESSURE LOSS	er: ····································	253.1 IAMINAR 8.0	FOWER LAW 2063 348.1 LAMINAR 6.1 1.131	** ** 、	
n i San Sangera	and an analysis and an and an and an and an and an and an and an and an and an and an and an and an and an and	1 41 11 11 12 14 14 14 14 14 14 14 14 14 14 14 14 14		ngganggapang sige ta sakaya na kangga ne na jeruntu manu.	N S - 28 - 2 ^{- 1} - Krywsadje stre i oskonogijajski - 1903. god ji ji -	n a an an an an an an an an an an an an
						У-
an <mark>ad a</mark> tangi	an an an an an an an an an an an an an a	a ya baya na manaka ini ini na mina na	jani ngan manalah kan ingkan kanan saran sa	i gandingan atau atau atau atau atau atau atau at	mamenennergenergenergenergenergenergenerge	and the second sec
006-	SURE LOSS ANAL	UC TO				
FREAD	SOLE INDS HINHLI	C1 C1				_
a na si si si si si si si si si si si si si	ala na manana manana manana ang kanana manana ang kanana. Na manana man	anna an an Anna ann Claighe Chàine an Anna Anna an Anna Anna Claighe Chàine an Anna	usur gebolerskilsterisk kinten ar undere	Beelfielderings bank in an order in a second source and the second second second second second second second se	Renter and constant and approximate and the constant of the co	 V. 11 - Hothleyer Hybrids Electronic 111
FROM	DEPTH OF 2824	TO 3970 ft	1983년 - 1984년 1987년 1987년 - 1997년 1987년 - 1987년 - 1987년 1987년 - 1987년 - 1987년 1987년 - 1987년 - 198			
(L)	ENGTH: 11	146, f t				
	ETERS: ANNULL	JS = 12,250,	JEIFE ID, OD, JD	= 4.276 5.000	6.500 inches	
DO	WNHOLE					
	VELOCITY: 2]	1.2.ft/sec,	1273.6 ft/min		ې يې	
			BINGHAM	POWER LAW		
	REYNULDS NUMBE		109519	30845		
	CRITICAL VELOC	.ITY:)fpm	293.7	311.0		
in a star y	FLOW REGIME:	and the second second second second second second second second second second second second second second second	'IURBULLNT	IURBULENT	and the second second second second second second second second second second second second second second second	
	PRESSURE LOSS:	: psi	192.3	129.8		
		· · ·				
		psi/100ft	16.781	11.323		
	NULUS	1.00	16.781			
	NULUS	1.00	16.781 186.2 ft/min	11.323		
ANI	NULUS VELCCITY: 3.	lit/sec,	16.781 186.2 ft/min BINGHAM	11.323 HOWER LAW		
ANI	NULUS Velocity: 3. Reynolds Numbe	l tt/sec,	16.781 186.2 ft/min BINGHAM 27148	11.323 HOWER LAW 1505		
ANI	NULUS VELOCITY: 3. REYNOLDS NUMBE CRITICAL VELOC	l it/sec, R: CTIY: fpm	16.781 186.2 ft/min BINGHAM 27148 288.8	11.323 HOWER LAW 1505 305.6	ار به مورو از این این می وارد از این این این این این این این این این این	
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ANNULUS...

VBLCC11Y: 2.9)It/sec, 173.6 ft/min BINGHAM

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REYNOLDS IN CRI TICAL V FLOW REGIN PRESSURE T	ELCCTIY: E: CSS: psi	-		1376 301.5 LAMINAR 11.2 .451			ß
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PRESSURE LOSS A	NALYSIS			an an an an an an an an an an an an an a	54-598-499 (2007) 55-59 		nonanan ana ana an
FROM DEPTH OF C	TO 331.ft	t		જેમાં દીધ છે. તે કે પ્રોય કરે છે. છે. તે પ્રોય છે. જેમ જેમ જેમ જેમ જેમ જેમ જેમ જેમ જેમ જેમ	. ક્રમ્યુલીએ પશ્ચિત્રિક્ષિક્ષિક્ષ અને ગેણે કુશવાર જેવે પૈરાવ્યું છે દિવસ	an an tha an tha thu tha an an an an an an an an an an an an an	างค <i>รรมสมัยนายมมีมีมีมีมีมีมีมีม</i> ี
IAMETERS: AN	NULUS = 2			JD = 4.276 5.000	6.500 inche	25	
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REYNOLDS IN CRITICAL V FLOW REGIN PRESSURE I	/ELUCTIY: E: OSS: psi	fpm	17874 284.9 LAMINAR 1.3 .386	308 245.0 IAMINAR .3 .095	an na shekararan karkararan karkararan n	tra ar e televista eserente pet y	ለተ ጋር በታምር ነው በሚያዋቋፍ ምርምጽ ምርቶ ወይ ጊ ፅ
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TUTAL ANNULA PUMP PRESSUA UNACCOUNTED CIRCUTATING EQUIVALENT C ECD W/CUTTIN	losses PSI AT BI .Ikc. Lens	ITY, lb/		53 53		16 16	9 6000342-900 <u>500</u> 20-90035564 6444
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FURIDRATION LOGENG BIDASTONAT OF ECRTESONE #2

FORTESCUE No. 2 - 1615 m 6 NOVEMBER 1978

PRESSURE LLSS ANALYSIS

DATA: DEPTH = 5298.6 (VERTICAL = 5298.6), RPM = 158 PUMP PSI = 2760, MUD WEIGHT = 9.10 MUD FLOW RATE = 930, DRILL RATE = 20.0, BULK GM/CC = 2.20

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RHEOLOGY: K n LOW 2.483 .387 MID 2.483 .387 FV = 8.0, YP = 18.0

SURFACE PRESSURE LOSS COEFFICIENT = 2 BASIC RESULTS:

	HULL VOLUME	891	BBLS,	5001 CUBIC FT.
	ANNULAR WILLIME	744	a de la companya de	4175 .
	VERTICAL DEFIN	5299		
	MUD HYLKUSTATIC DEPTH	5279		
	FURMATION FLUID LEPTH	102		
una canyago	HYDROSTATIC PSI	2493	an an an an an an an an an an an an an a	an an an an an an an an an an an an an a
	MUD CYCLE TIME (MIN) -	38		
	NOZZIES (1/32 INCH):	18.00	18.00	18.00
	JET VELLETTY	400	F1/SEC	
	JET PRESSURE DRUP	1304	•	
	BIT HYLKAULIC HP	708		
in weather and a	IMPALT FURCE (LB)	1753	an series and a constant of the	Sila ali dinanda dinangka malaina disana i saraha
1	SURFACE FSI LUGS	60		

psi/l00tt

FROM DEFIH OF 4761 TO 5299 ft

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LENGI'H:	536 f	t						
Diane'ilks: Downhole	ANNULLS =	12.250,	PIPE 1.,	UL, JD	= 2.613	7.750	7.750	inches
VELOCIT	¥: 48.0	it/sec,	2880.8 ft	/min				
en la la factoria de la compañía de		ren i - Lon Spin - Schrieblich		· · · · · · · · · · · · · · · · · · ·	POWER	LAW	o bo agara seri a	e contra contrator analysi
REYNOLD	5 NUMBER:		142602			8583		
CRITICA	L VEICCITY	: fpm	340.4			06.6		
FLW KE	slife:	-	TUREULLNT		1UKEU			
PRESSURI	e Mos: p	si	666.1			36.5		

123.808

62.544

ANNULUD					15
VELULIIY: 4.2	tt/sec, 25				
AND THE REAL PROPERTY AND THE		BINGHAM	POWER LAW		
REYNOLDS NUMBER:	AR LDEGUN	20057	1545		
CRITICAL VELOCIT	Yaustym	332.4	408.4		
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PRESSURE LOSS:			7.8	n en la menera a la composición de la composición de la composición de la composición de la composición de la c	, i vo en contra a s
	psi/100ft	1.889	1.446		
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PRESSURE LOSS ANALYSI	re hetseler	A. Bride States Pro-			and the second second
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FROM DEPTH OF 2824 TO) 4/01)IT				
	7 ft				
LENGTH: 1937	/ift of an is a	²¹ NumB Reserves			
				e de la la se	
AMETERS: ANNULUS	= 12.250,	PIPE ID, OD, OD	= 4.276 5.000	6.500 inches	
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VELOCITY: 20.8	Dit/sec, J	1246.7 ft/min			
	n na cristi a litera.	BINGHAM	POWER IAW		
REYNOLDS NUMEER:		93812	23934		
CRETICAL VELCCLI		333.1	367.7		
FLOW REGIME:		IUREULLNT	'IURBULENT		
PRESSURE LASS:	psi	321.2	215.5	ം പറ്റാം 11 പ്രത്യെക്ക് പറച്ചെടുത്തും കുറ്റവാള്ക്കെടുങ്ങള്ള്ള്ള്ള്ള്ള്ള്ള്ള് മെക്ക്	
	psi/100tt	16.588	11.126		· · · · · · · · ·
ANNULUS	Famely and a second	का च व का ते का 19 20		د شم	
VELOCITY: 3.0	++/cor][27 2 ++/min		•	¹
VELANCE AND COUL	LL/Del /	BINGHAM	POWER LAW		
TRACKINT THE - NA IMEDIA			1103		
REYNOLDS NUMBER:		23254			
CRITICAL VEICCTI	Y: TEW	327.5	362.4	ாட்டிரிசிய, , டி. உங்கள் கொடி கொடி காடலாம்/திருகண்டும் துட நடி	an an thus and a substantian a sub- t
FLOW REGIME:		LAMINAR	LAMINAR		
PRESSURE LOSS:	psi	22.0	12.6	·	
1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -	psi/100tt	1.134	.652	,	
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na nakonanyo ni oro nakono nakanyo kata kata kata kata kata kata kata kat	an na an anns a thata a thatain tha thatain a thatai	• · · · · · · · · · · · · · · · · · · ·	lantai declarante e e ce ce ce co la transci datti cile cinedatti datte i	urense en settetta solar da Barbaiada iskolaise en angenaen sigte 🖧 Sakipitaging es en ekse	ىرى يەرىمە ھەرەۋەۋەرمەرمە خەرەمە ھەرەمە ھەرەمە ھەرەمەر
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FROM DEPTH OF 331 TU	2824)ft				
LENGTH: 2493					
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DTAMPTERS. ANNULUS	- 12 615	DIDE TH. OU. JD	- 4 276 5.000	6.500 inches	
DIAMETERS: ANNULUS DOWNHOLE	a ⁿⁿ galadan Uatar parya	ELEL JUS	a ¹⁹ a 12 a 4 / U angoon d a tara ara ya ka		ு பிரானத்தைத்து குறித்து புடை
	- Fr Iman	1046 7.44 min			
VELCLIY: 20.8	SIT/Sec,	1246.7) tt/min			
المراجع والمراجع		BINGHAM	POWER LAW		
REYNOLDS NUMBER:		93812	23934		
CRETICAL VELOUI			367.7		
		IUKBULLNT		an an an an an an an an an an an an an a	>
PRESSURE LOSS:		413.5	277.4		
•		16.588	11.126		
ANNULUS					
VELCELLY: 2.8	ft/sec, lf				
		BINGHAM	FOWER LAW		
REYNULES NUMBER:	2	22773		1. 1. The second s second second sec second second sec	· · · · · · · · · · · · · · · · · · ·
CRITICAL VELOCTI		327.1	357.9	 2.2.15039553 (2008) 2.250 (2.1 million documents in the second secon second second sec	n in the Ministry and the
FLOW REGIME:	and the second second	IAMINAR	LAMINAR	-	
PRESSURE LOSS:			14.8		
		1.077	.592		
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FROM DEPTH OF	0 TO 331 it				
LENGTH:	331 ft				
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DIAME TERS:	ANNULUS = 21.200 ,	PIPE ID, OD, JD	= 4.276 5.000	6.500 inches	
DOWNHOLE					
VEICCLIT	: 20.8 it/sec,				
		BINGHAM	FOWER LAW		
REYNOLLS		93012	23934	en and and the second of the second	waa ahaa in ka chikaa kaakiisa
	VELOCITY: fpm	333.1	367.7		
FLOW REL		TURBULENT	TURBULENT		
PRESSURE	LOS: psi	54.9	36.8		
	2015L	16.588	11.126		
	psi/iuurt	10.000	11.120		
ANNULUS			11.120		
Annulus Velucity				مەرىقى يەر بەر چېچىچىنى بىر	
VELACT'IY	: .9 ft/sec., 5	3.7 ft/min BINGHAM	POWER LAW	مراجع والمراجع والمراجع والمراجع	
VELUCITY REYNULDS	: .9 ft/sec, 5 NUMEER:	3.7 ft/min BINGHAM 15311	POWER LAW 213	مەر مېر . د يەر يەر چېرە مەر يەر ي	
VELLCITY REYNOLDS CRITICAL	: .9 ft/sec, 5 NUMEER: VELOCTIY: fym	3.7 ft/min BINGHAM 15311 323.1	POWER LAW	na sa	
VELCCITY REYNOLISS CRITICAL FLOW REG	: .9 ft/sec, 5 NUMEER: VEIXTIY: fpm Int:	3.7 ft/min BINGHAM 15311 323.1 LAMINAR	POWER LAW 213	aan ah ah ah ah ah ah ah ah ah ah ah ah ah	
VELCCITY REYNOLISS CRITICAL FLOW REG	: .9 ft/sec, 5 NUMEER: VELOCTIY: fym	3.7 ft/min BINGHAM 15311 323.1 LAMINAK 1.6	POWER LAW 213 295.8	مې مې او د د د ورې هېره مې کې د د د ورې د وې د د د د ورې د وې د د د د ورې وې وې د د د د د وې وې وې د د د د د د د د د وې وې وې وې وې وې وې وې وې وې وې وې وې	

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		BINGHAM	POWER LAW
662-	TUIAL SUKFACE LUSS	60	
чж	TOTAL DOWNHULE LOSS	1456	866
	TUTAL BIT LLES	1304	1304
	TOTAL ANNULAR ILCSS	61	36
	PUMP PRESSURE	2760	2760
	UNACCUUNTEL LOSSES	-121	494
	CINCULATING PSI AT BIT	2554	2529
	EQUIVALENT CIRC. LENSITY, 16/0	al 9.29	9.20
	ECL W/CUITINGS EFFECT, 1b/gal	9.29	9.20
	FUR MUD WI	9.10	9.10

FORTESCUE #2

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EXPLORATION LOGGING

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PRESSURE LLDS ANALYSIS

DATA: LEPIH = 6618.0 (VERTICAL = 6618.0), RPM = 160PUMP PSI = 1025, MUD WEIGHT = 9.10MUD FLOW RATE = 525, LATLL RATE = 66.0, BULK GM/CC = 2.25

	RHEOLOGY	: K	'n		
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	MIL PV =	.667 12.0,	.585 YP = 12.	0	ана (Арала). Алар

SURFACE PRESSURE LOSS WEFFICIENT = 2 SIC RESULTS:

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•	HOLE VOLUME		1083	BBLS,	6080	CUBIC	FT.		
	ANNULAR VOLUME		901		5058				н у ⁴ т
	VERIICAL LEPin		6618						
	MUL HYLKOSTATIC	LEPIH	6598						
	FURMATION FLUID) LEFTH	102						
	HYDROSTATIC PSI	an an an an an an an an an an an an an a	3116	ىي د تىرىكىتىتىك مىرى ۋېتىكىنى دا ئىشىكىكىتىك	n er værdeget i ridskryd	1	and and a stand of the second second second second second second second second second second second second seco	A la se la serie de la serie	and the second state of the se
	MUD CYCLE TIME	(MIN)	81	• . • .					
	NOZ2LES (1/32]	INCH):	18.00	18.00	18.0	0			
	JET VELICITY		226	FT/SEC					
	JET PRESSURE LE	(CH ²	416						
	BI'I HYCKAULIC H	P	127						
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-EROM DEFIN OF 5991 TO 6618 ft

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LENGTH: 62	7 ft*		n an an Anna Anna Anna Anna Anna Anna A	an Na ang ang ang ang ang ang ang ang ang an	
DIAML'IERS: ANNULU	5 = 12.250,	PIPE 1D, OD, JI	0 = 2.813 7.750	7.750 inches	
DUWNHOLL					
VELOCITY: 27	.1 ft/sec,	1626.3 ft/min			
n () normaline benann g ele e en normann () - n Kurdiger eigen hage sterren sage -	ann de anna de de de la dela de la construction de la dela de la dela de la dela de la dela de	BINGHAM	POWER LAW	and and an an an an an an an an an an an an an	an an an an an an an an an an an an an a
REYNULDS NUMBE	R:	53667	31126		
CRITICAL VELOC	17Y: fpm	293.0	316.3		· · ·
FLW REGIME:	-	TURBULLNT	TURBULENT		
PRESSURE LOSS:	psi	300.8	227.9		
	psi/100ft	47.971	36.352		
ANNULUS	ner 🕯 🚛 - e e - ng saya di selar e na na nati	anna an an b>	Anterin en	ant allanda gana sayangan sati	· 1993 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994 - 1994
VELCCITY: 2.	4 ft/sec, 1	43.0 ft/min			
		BINGHAM	POWER LAW		
REYNOLLS NUMBE	R:	7548	1009		
CRITICAL VELCC	IIY: fpm	260.6	313.8		
FLOW REGIME:		LAMINGK	LAMINAR		
PRESSURE LASS:	psi	8.0	4.4	To control and the state metric and a series of a slightly of	ுத்பார். இப்பாலில் திழைத்திற்குத்தில் சுதார்த்த க
- 19 04	psi/100ft	1.279	.706		

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VELLEITY:	11.7 ft/sec,	703.8 ft/min				
		BINGHAM	POWER LAW			
REYNULLS I		35306	12156			
	VELUCITY: fpm		266.1			4
FLW RELI		TURBULENT	IUKBULLNT	, statistics a construction of the	e y Maria ana ara	
PRESSURE I	LCS: psi	203.5	185.1			
است في دري خاطبت به وه	psi/100ft	6.427	5.846			
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VELOCITY:	1.7 tt/sec,	•	MARKEN AND			
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FLUW REGI	/EICCTIX: Ipm	272.9 LAMINAR	256.0 IAMIMR			
		24.1	LAMINAR 8.6		472 J	
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	For 10010	• / VL	• 2 / 1			
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JAMETERS: ANNULUS	= 21,200,	PIPE ID. OD. J	$\omega = 4.276 5.000$	6.500 inches	
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VELOCITY: 11.7					
		BINGHAM	POWER LAW		
REYNOLDS NUMBER:		35306	12156		
CRETICAL VELOCIT	-	261.6	266.1		
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	psi/100ft	6.427	5.846		1997 x
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	psi psi/100ft	.331	.1 .U36		
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UNACCOUNTED LOSSES	• • • • • • • • • • • • • • • • • • •	-149		1025	
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FV = 11.0, YF = 14					
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SASIC RESULTS:		· · ·			
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ANNULAR VOLUME		988	5546		
VERIICAL DEFIN		7333			
MUD HYDRUSTATIC DEL	PTH	7313	alaala ahaanaa daha baha badaha ka sa	ana gana sa	· · · · · · · · · · · · · · · · · · ·
FURNATION FLUID LE		102			
HYDROSTATIC PSI		3454			
MUD CYCLE 'HERE (MIT	n de servici se composition de la composition de	40			
NU24123 (1/32 INT)			20.00		-
JET VELOCITY	-	367 FT/SEC			
JET PRESSURE DROP			കുറഞ്ഞും ഉപ്പെങ്ങളും പ്രംപം മങ്ങളും തുന്നും പ്രംഗം മുദ്ദേഹം പ്രംപം മങ്ങളും പ്രംഗം മങ്ങളും പ്രംഗം മുത്തം പ്രംഗം	en nezet kan komen ja ja sa	
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Length: 627 i Diametters: Annulus =	tt = 12.250, 1 tt/sec, 3	004.7 ft/min	· ·	./50 inches	
Length: 627 i Diametters: Annulus = Downhole	tt = 12.250, 1 tt/sec, 3	•	EUWER Low	./50 inches	. / / · · · · · · · · · · · · · · · · ·
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TUIAL ANNULAR LUSS			1220 36	
FUMP PRESSURE	2660	್ಷ ಕುಲ್ಲೂ ಮಾಲನಿ ಹೆಸಲಿದ್ದ ೧೯೯೭ ಶಿಕ್ಷಿ ಹೆಸಿರು ಸೋತಿತ ರಾಗನಾಡಿ ೯೯೭	2660	· · · · ·
UNACCOUNTED LOSSES	-864		-198	
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PRESSURE LOSS ANALYSIS		VEMBER 1978			
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PRESSURE LOSS ANALYSIS

- Exploration Logging

STREET CAUSE IN VARIANCE IN

LENGTH: 4489 FE

STATISTICS OF STATISTICS

FROM DEPIN OF 2824 10 7313 Lt

DIAMETERS: ANNULUS = 12.250, PIPE 1D, OD, JD = 4.276 5.000 6.500 inches
DUWNHULE...
VELOUITY: 21.3 it/sec, 1260.3 it/min

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appear is conclusive and

REYNOLDS NUMBER: 56258 CRITICAL VELCCITY: fpm 321.7 FLOW RESIME: TURBULENT TUR PRESENT LOSS: psi 566.8 psi/1001t 19.801 ANNOLUS VELCCITY: 3.1 It/sec, 187.2 It/min	ER LAW 22981 321.8 BULENT 710.2
CRITICAL VELOCITY: fpm 321.7 FLOW REGIME: TURBULENT TUP PRESENT LOSS: psi 588.8 psi/1001t 19.801 ANNOLLE VELOCITY: 3.1 rt/sec, 187.2 ft/min	321.8 BULENT 710.2
HLW RESIME: TURBULENT TUP PRESENT LOS: psi 568.8 psi/lult 19.801 ANNULUS VELACITY: 3.1 rt/sec, 187.2 ft/min	BULENT 710.2
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VELCCITY: 3.1 It/sec, 187.2 It/min	15.623
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CRETICAL VERCETTY: 1pm 311.8	311.1
FLOW RED INE: LAPILMAR 1	Anliar
Erlosung Llos: esi 46.5	. · · · · · · · · · · · · · · · · · · ·
rsi/100ft 1.036	23.3

FROM DBP111 OF 331 TO 2824 It

LENGIH: 2493 ft

DiARETERS: ANNULUS = 12.615, FIFL 1D, CD, JD = 4.276 5.000 6.500 inches LOWNHOLE...

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		BINGHAM	POWER IAW
REYNGLDS NUMBLE	•	56258	22981
CRUTICAL VELOCI	ii: fpm	321.7	321.8
rlu kilite:		TOPPOTT MJ.	TURDURENT
FRESSURE LUSS:	rsi	493.6	354.5
	rsi/1001t	19.801	15.823
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VELICITY: 2.9	tt/sec,	174.5 ft/min	an an an an an an an an an an an an an a
		BINGHAM	ROWER LAW
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Charlense VELLER	lY: fpm	311.1	305.1
FLOW RECIPE:		IAP. INSI.	Levels
PRESSURE LASS:	psi	24.4 " en en en en en en en en en en en en en	11.5
	psi/100ft	.981	.462
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-	ELUIVALENT CIRC. DENSITY,		9.38	
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FRESSURE LUSS ANALISIS

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VERTICAL DEPTH	8531		
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LOWNHOLE	c, 2044.4 tt/min BlNsHAM	ROWER LAW	
LOWNHOLE	с, 2044.4 tt/min BlNsHAM 54567	25372	
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DOWNHOLE VELOCITY: 34.1 ft/sec REYNOLDS NOMBER:	с, 2044.4 tt/min BlNsHAM 54567		
DOWNHOLE VELOCITY: 34.1 ft/sec REYNOLDS NOMBER: CRITICAL VELOCITY: fpm	с, 2044.4 ±t/min BlNsнAM 54567 n 398.7	25372 476.8	
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PRESSURE LOSS ANALYS						
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PRESSURE LOSS:						
PRESSURE LOSS:	psi/100ft	2.420	1.559			
°KM-DBPTH-CP-2824-1	psi/100ft	2.420		Stature Schödensteren I. 2000, Sanarcasan	una anteresta de la compañsión de la compañsi La compañsión de la compañs	au von uneen in die Amerikaan
'KM DEPTH CP 2824 1	psi/100ft	2.420		цанцион фацирирания и алган раналсаннас	พระ 1 สาระดีหลังได้เหลือกับรูลเรื่องร่างได้เรื่องรู	เขาดารณหญาญสูสหรัญชา
rom depth of 2824 t Length: 493	psi/100ft IO 7754)IL 30 ,ft	2.420	1.559	one-superiore successions and	~ 1 405998439945249249348394	anorment of the states
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FROM DEPTH CP 2824 LENGTH: 493 DIAFETERS: ANNULUS DOWNHOLE	psi/100ft 10 7754) It 30 , ft 5 = 12.250,	2.420 PIPE 1L, OD, JD	1.559	6.500 inches	ich yn cyffogdyl feiniau r y fryn fryn fryn gan yn gan yn gan gan gan gan gan gan gan gan gan ga	and network a subject of the subject
rom depth of 2824 t Length: 493 Diameters: Annulue	psi/100ft 10 7754) It 30 , ft 5 = 12.250,	2.420 PIPE 1L, OD, JD 884.8 ft/min	1.559 	ილიალი ეგელებალიალი აა არიე იდაიადიალი ს. 500 inches	alar or district a stable district are a friend are distributed as a friend are distributed as a friend as	andersteine er dag ei utföri terkonutiveliktioteridet
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ASIC RESULTS:	CM1 - J			· · · · · · · · · · · · · · · · · · ·
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MUD HYDROSTATIC DEPTH	8679			
FORMATION FLUID DEPI'H	102			
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MUD CYCLE TIME (MIN)	81 15.00 15.00	16.00		
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ROM DEPTH OF 8215 TO 8699 ft			n general de la companya de la companya de la companya de la companya de la companya de la companya de la compa	
AND MARIN OF USID IN DUDY IT		·		
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IAMETERS: ANNULUS = 12.250, DOWNHOLE	ATER TO' OD' OD		. /ou inches	•
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	BILIGHAM	POWER LAW		
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	403.5	281.2		
psi/100ft	83.372	58.092		·
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VERNETT: Jet IC Deck	BINGHAM	POWER LAW		
REYNOLDS NUMBER:	7053	813	and the constant product of the constant	والمحاجب والمحاجب والمحاجب
CRITICAL VELOCTIY: fpm	376.7	463.5		
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REYNOLDS NUMBER:	8177 7: from 366.1	389.3			
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LENGTH: 2493	ft				
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	= 12.013, PIPE 10, 00,	UD			
DOWNHOLE VELOCITY: 15.2	ft/sec, 911.6 ft/min		an in an air air an an an an an an an an an an an an an	termine in the formation in the provide states in the	unu pangating sikati
VELACITI: 1J.2	BINGHAM	POWER LAW	<pre>state to the state of the</pre>		
REYNOLDS NUMBER:	32989	10618			
CRITICAL VELOCITY	Y: fpm 378.2	401.1	•		*
FLOW REGIME:	TURBULENT	TURBULENT 239.9			
PRESSURE LOSS:	psi 278.5	239.9 9.623			
	psi/100ft 11.170		n 1997 - Anna Santara Anglan Santara Santaran Santar (j. 19 1997 - Anna Santara Sant	al California (1995) and a state of the second second second second second second second second second second s	in an anna an 1960. An anna anns an 1980
ANNULUS	ft/sec. 124.3 ft/min				
VELACTIT: COT	BINGHAM	POWER LAW			· ·
REYNOLDS NUMBER:	8008	599			
CRITICAL VELOCTI	Y: fpm 365.3				
FLOW REGIME:	LAMINAR			and the second second	e (k. 1997) Berlinkerske
PRESSURE LOSS:					
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REYNOLDS NUME CRITICAL VELO		32989 378.2	10618 401.1	- •• •• •	
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TOTAL DOWNHOLE	LOSS	1321 1351		1072 1351	
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(iii)	DRILLING DATA PLOT 1:1000
(a)	ROP, Dxc, Torque, WOB, RPM

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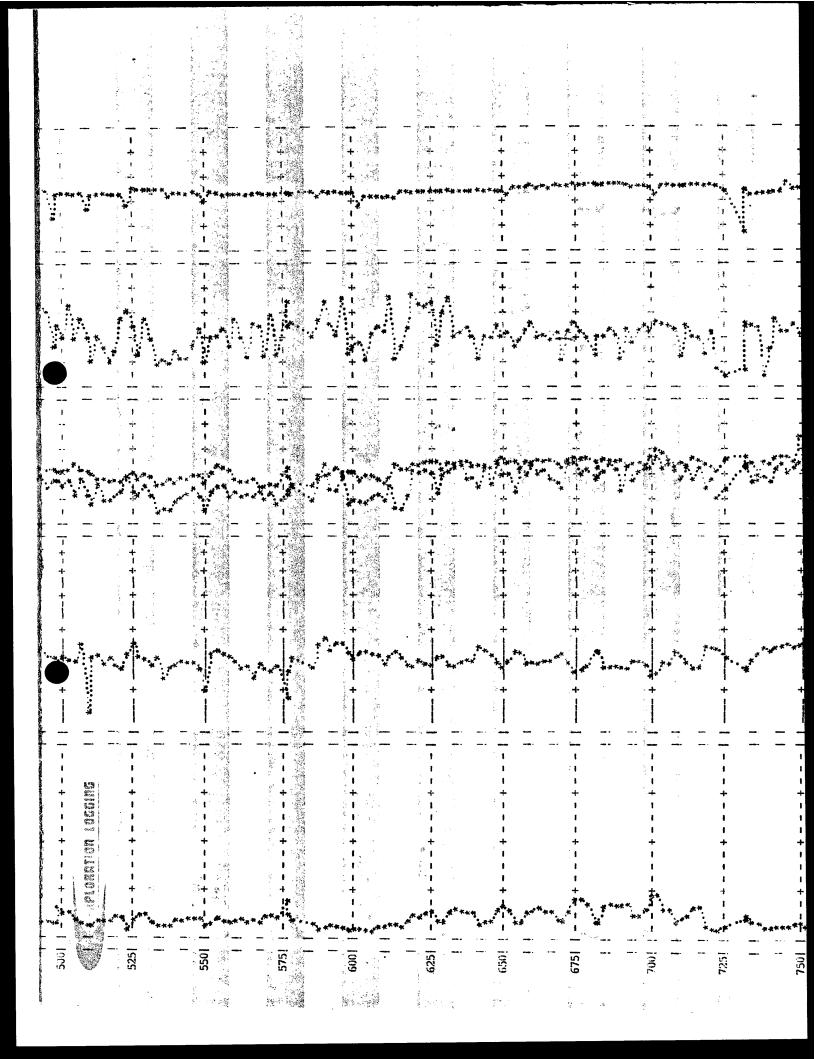
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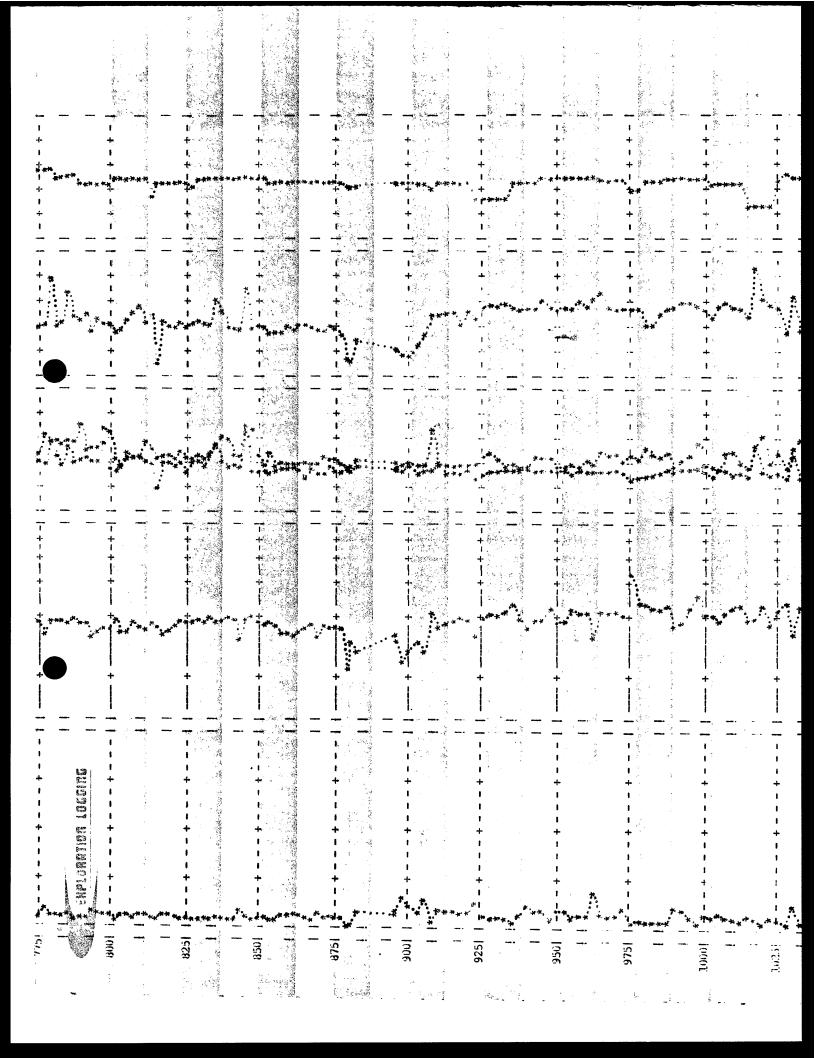
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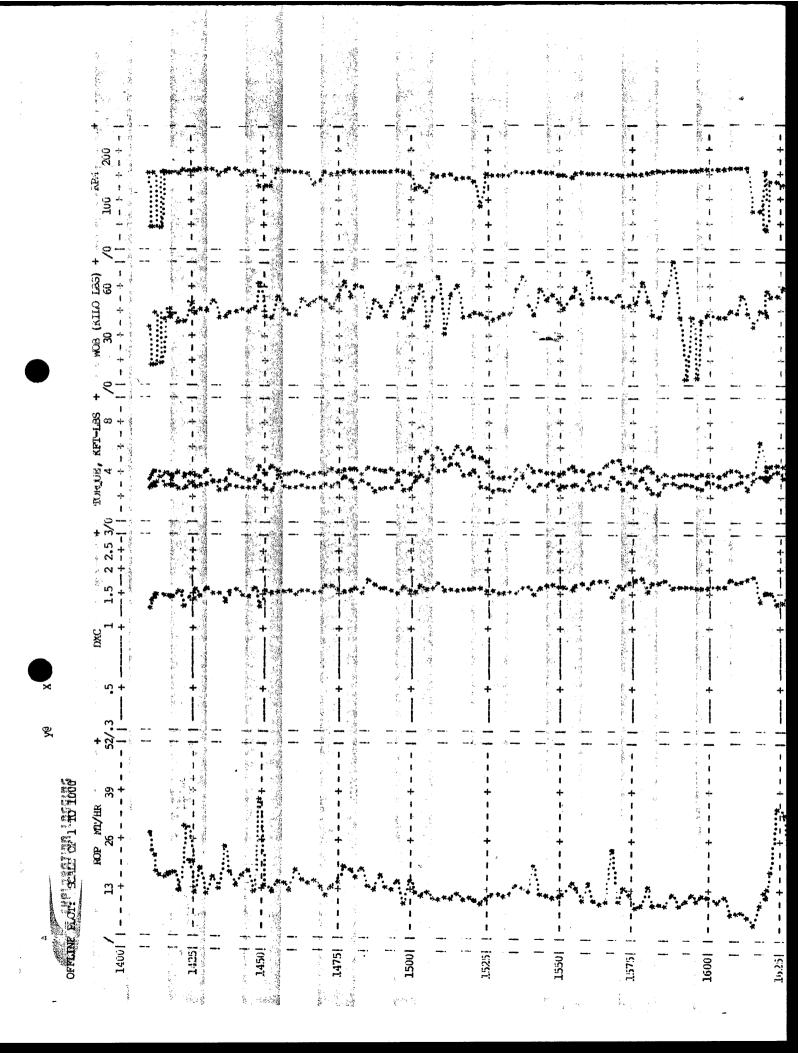


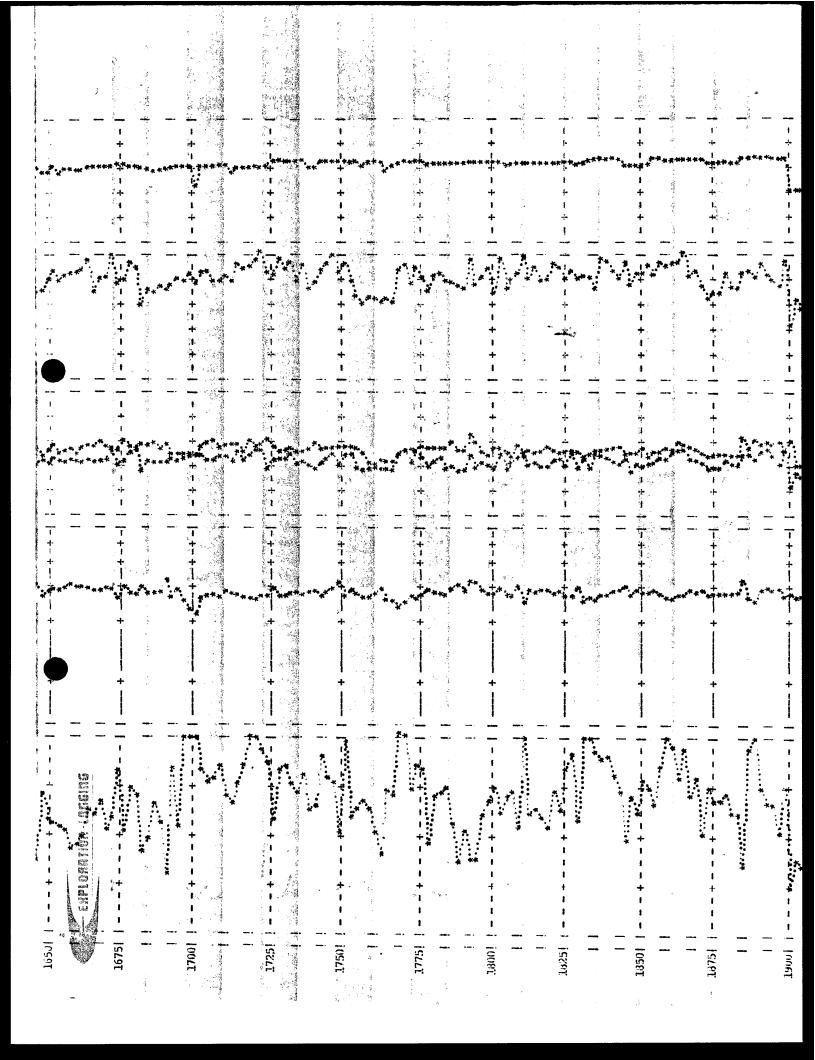
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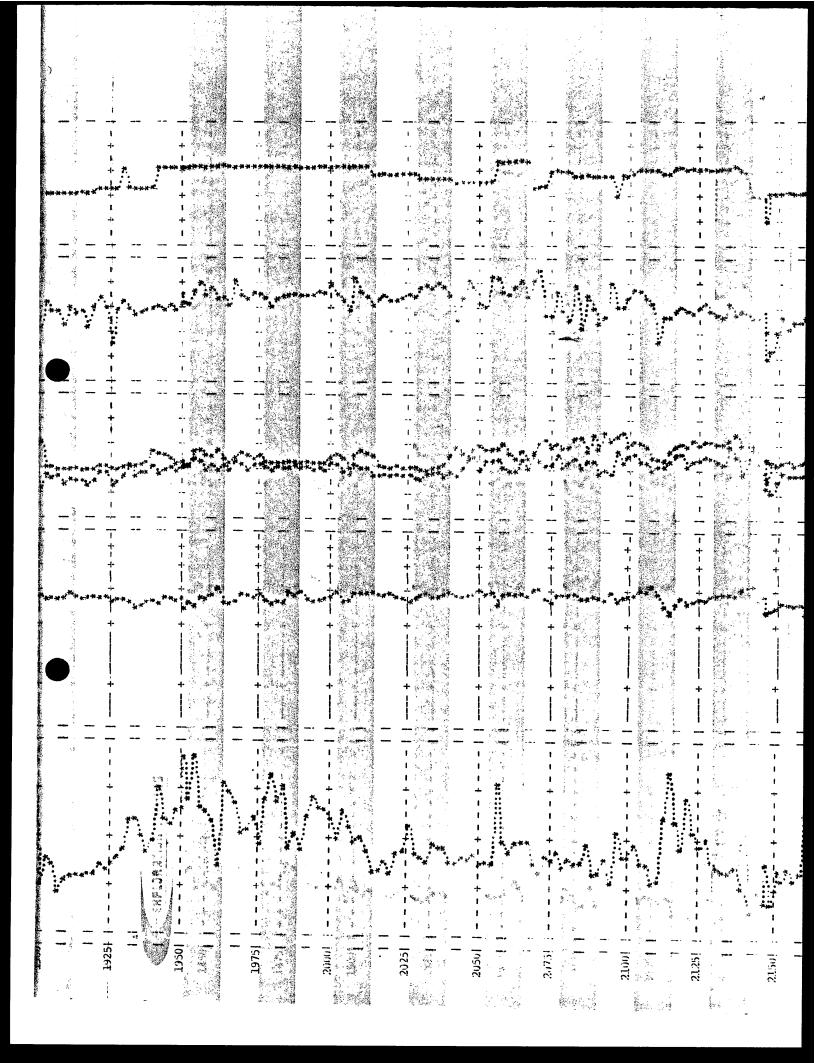
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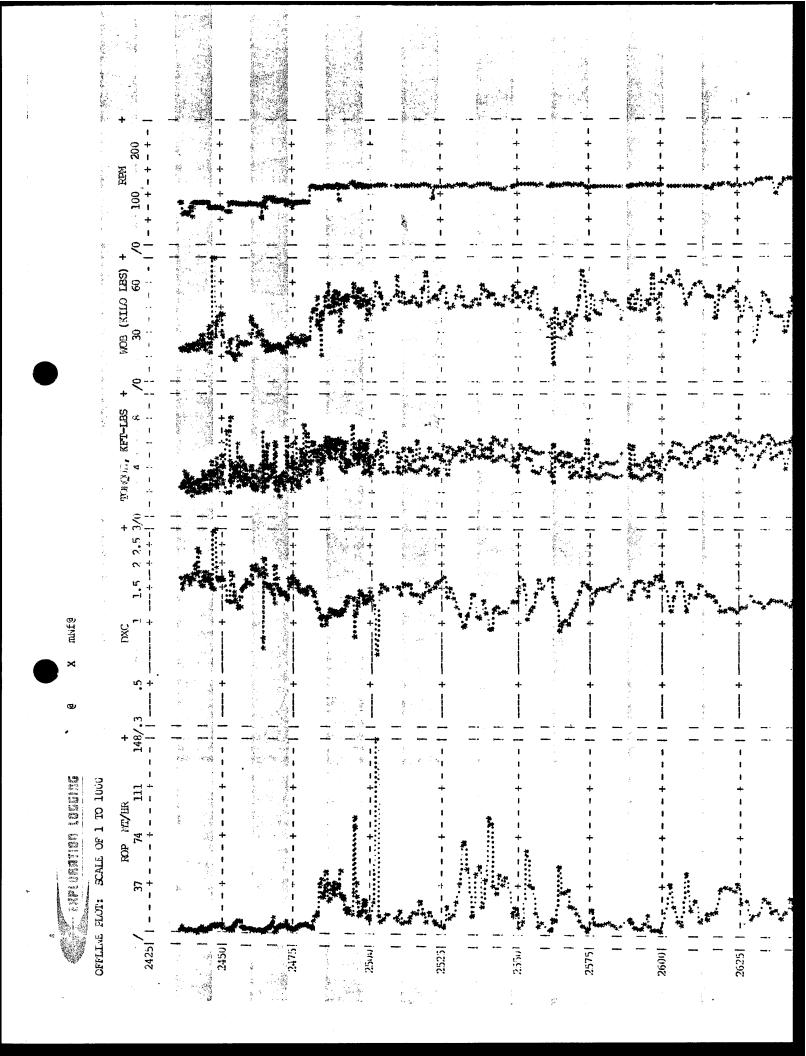


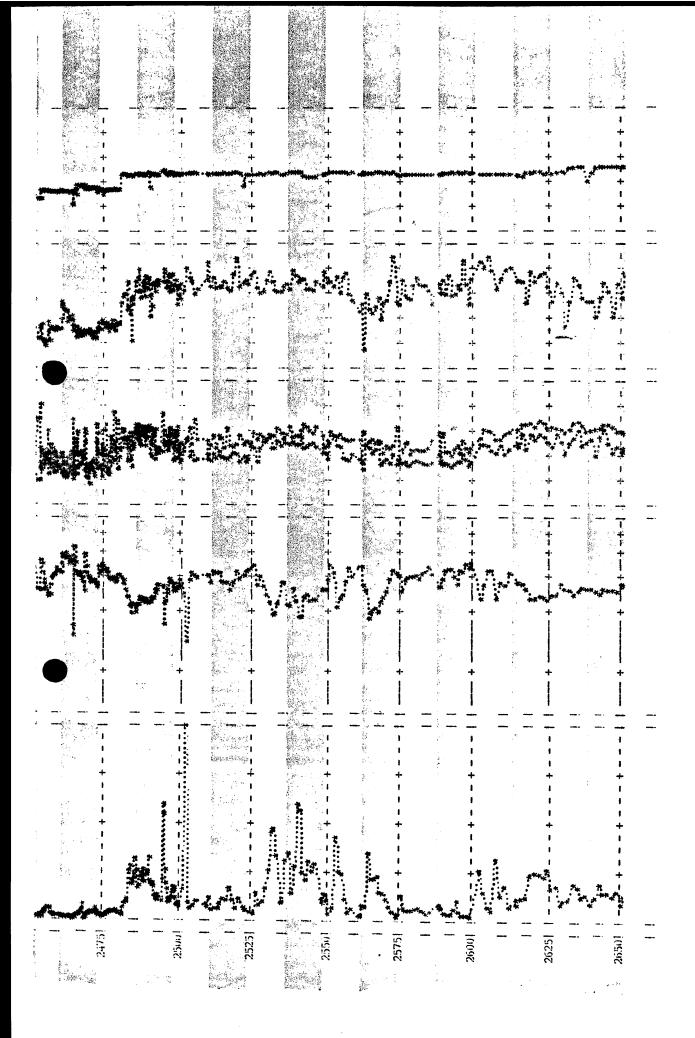




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(iii) DRILLING DATA PLOT 1:1000

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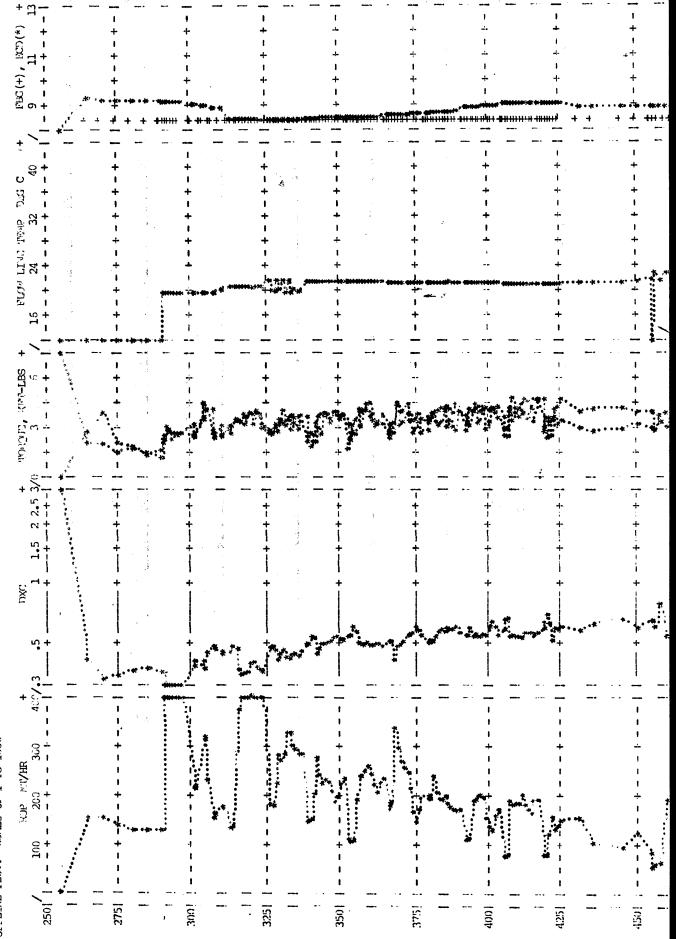
(b) ROP, Dxc, Torque, Flowline Temp, Pore Pressure, ECD



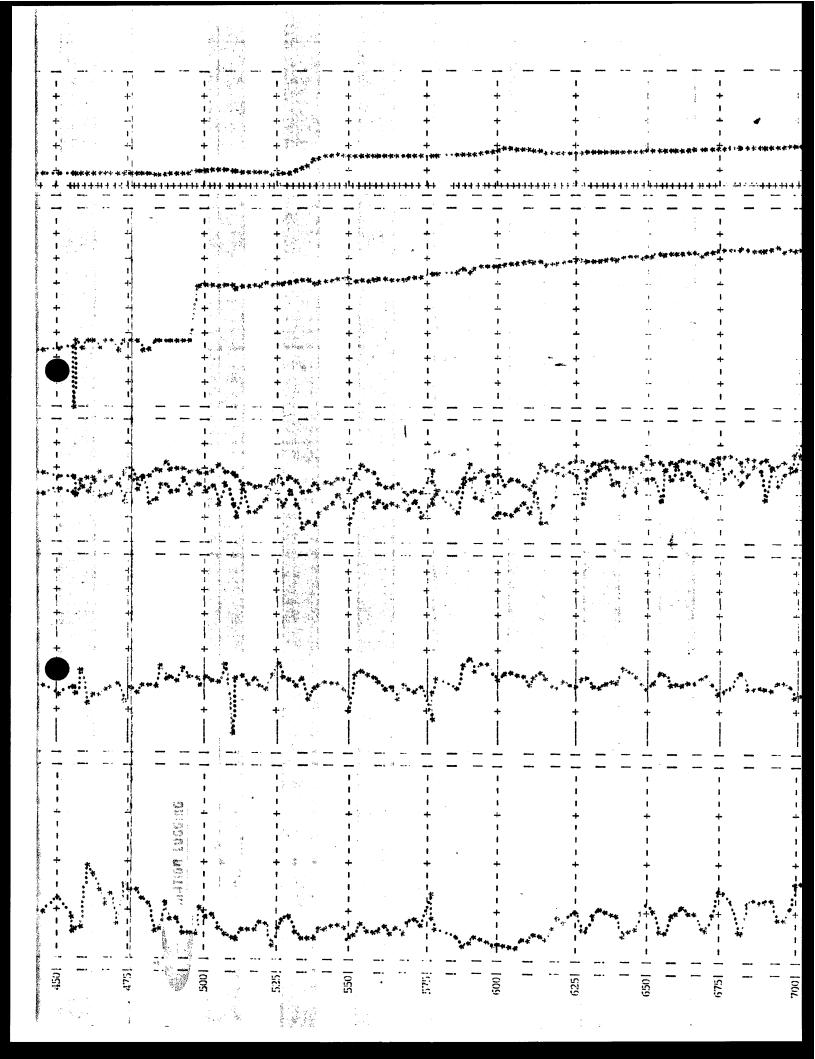


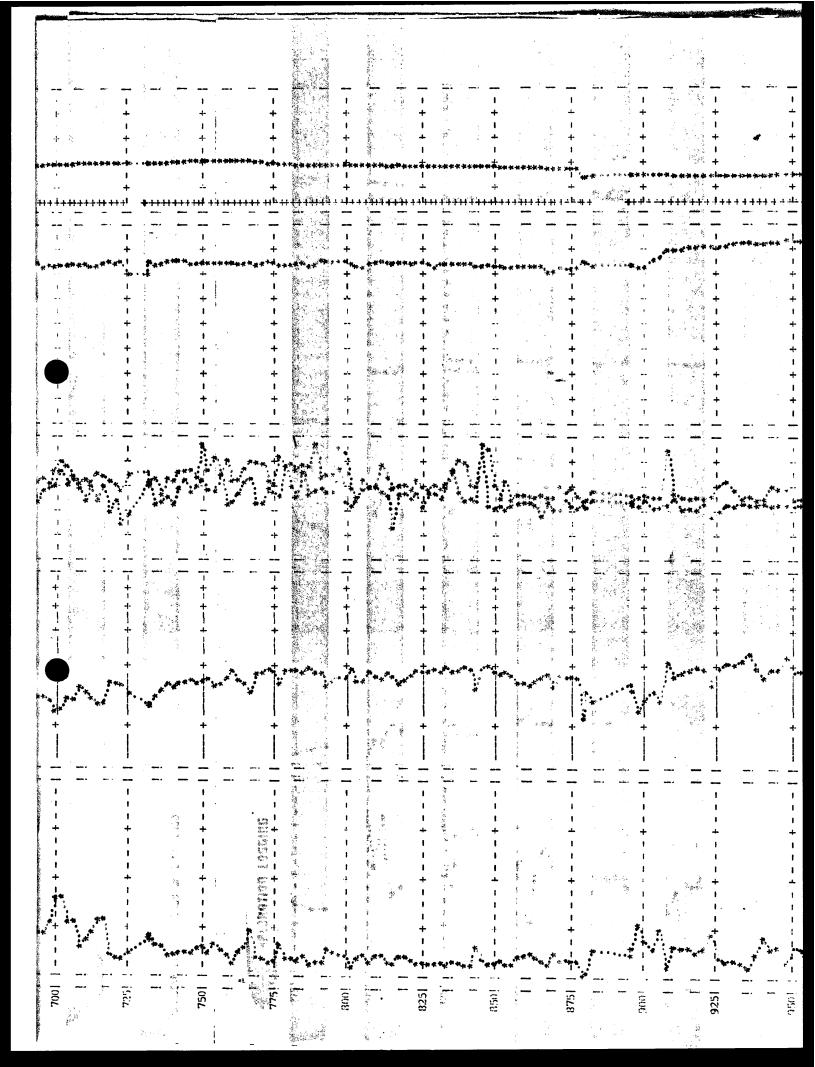
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OFFLINE PLOT: SCALE OF 1 TO 1000

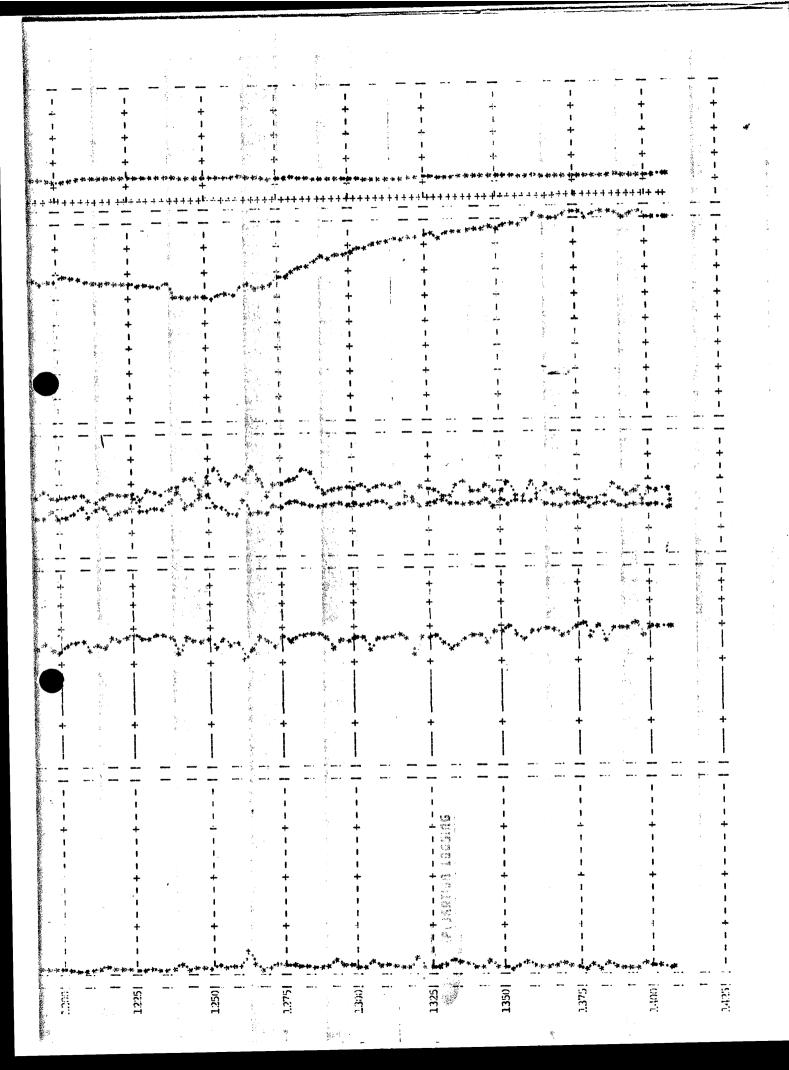


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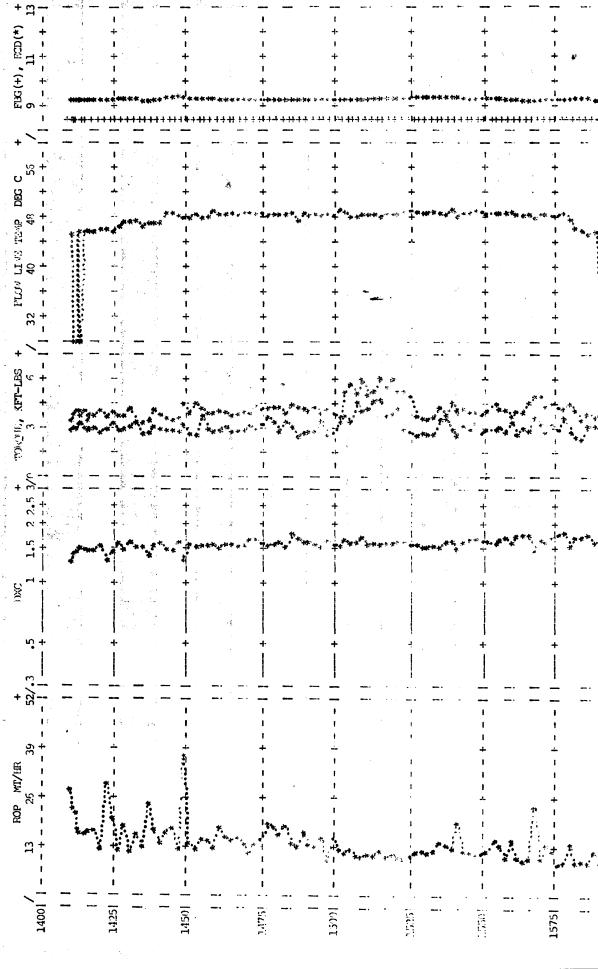
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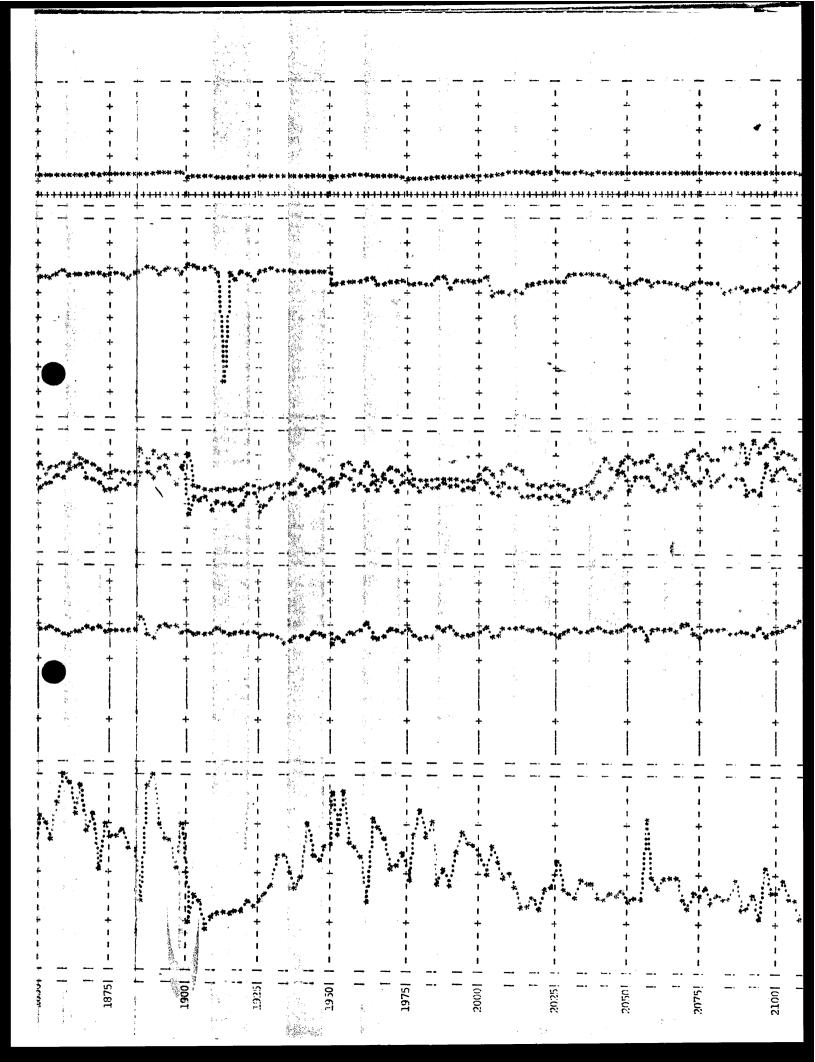




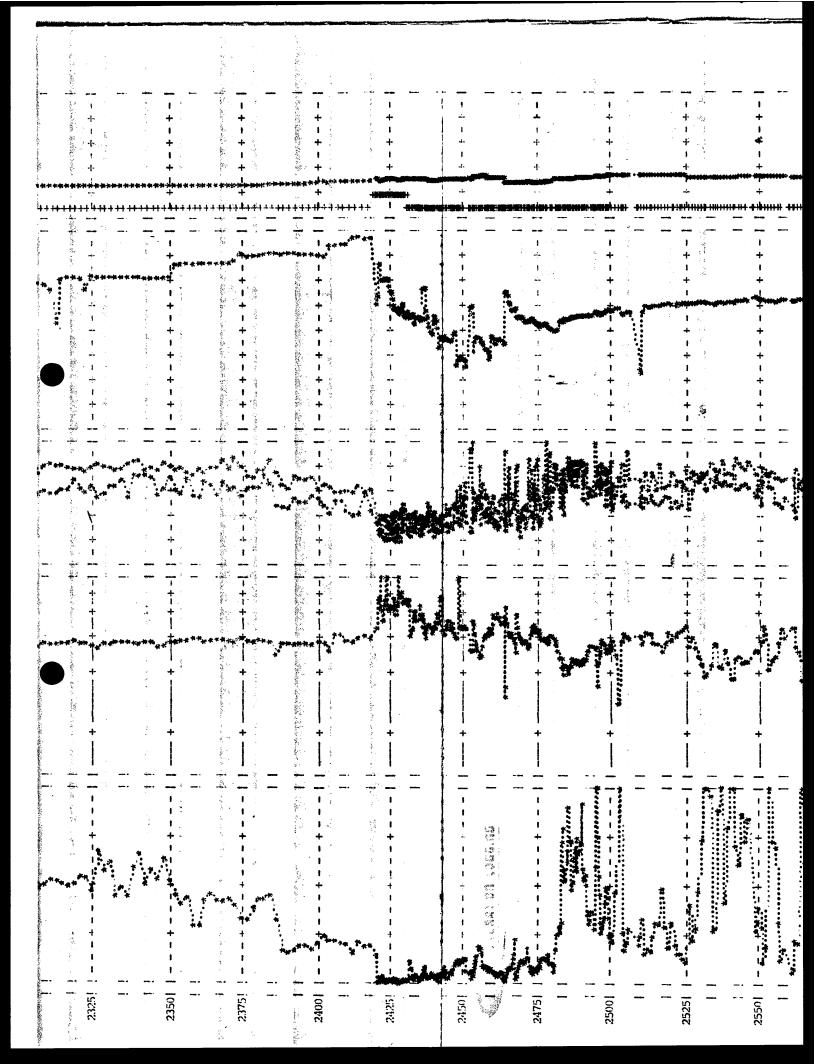
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A P P E N D I X E

MORNING AND WEEKLY REPORTS

PETROLEUM ENGINEERING SUMMARY REPOR	RT
COMPANY <u>ESSO AUSTRALIA</u> Well NANE <u>FORTESCUE NO2.</u> Date <u>7. Nou. 1978</u> Depth <u>2017 M</u> Last Report Depth	
BRILL PATE 20 m /HR average CORRECTED D EXPONENT 1.37@ 1920H 1.48@2015H FLOWLINE TEMPERATURE 47.7°C SHALE DENSITY - SHALE FACTOR - MAX. FORMATION GAS 8 units 0 1790H BACK GROUND GAS 4 units 0 1790H BACK GROUND GAS 12 units 0 1615m. TRIP GAS 12 units 1615m. LITHOLOGY: CALCAREOUS MUDSTONE - MUD WT. IN 9.1 b/GA1 PV/YP 12/12	SPM 61 GPM FS 525 DP AN VEL 959 FT /Min DC AN VEL 143 FT /Min CRITICAL VEL 280.6 FT /Min PRESS(TOTAL) 1174 PS1 PRESS(TOTAL) 1174 PS1 PRESS(BIT) 3167 PS1 PRESS(SYSTEN) 1025 PS1 BIT NOZ VEL 226 FT/SEC HOLE VOL 1083 BB1 AN. VOL 901 BB1 PIPE VOL 109 BB1 PIPE DISPL. 74 BB1 BIT TYPE HTC X3A JETS 3x18 Av. WOB 52000 16
MLD WT. OUT <u>7.3 /6/GA/</u> ECD <u>7.2 + 16/GA/</u> CL- <u>3000</u> ESTIMATED PORE PRES <u>S</u> <u>8.5 /6/GAL</u> MAX. ESTIMATED PORE PRESS IN OPEN HOLE <u>8.5</u> ESTIMATED FRACTURE PRESS <u>15.7 16/GA/</u> MIN. EST. FRAC. PRESS. IN OPEN HOLE <u>14.0 16/GA/</u>	AV. RPM 158 AV. TORQUE 4500 FT 16 TIGHT HOLE ON TRIP IN @ 181547 FILL A LAG EST. & CAVINGS
COMMENTS:	

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PETROLEUM ENGINEERING SUMMARY REPORT

	COMPANY <u>ESSO</u> <u><i>PUSTRALIA</i></u> WELL NAME <u>FORTESCUE</u> # 2	
DEPTH	DATE B. NOV. 1978	TIME 0600
CORRECTED D EXPONENT 1.58 C. 15.5.4 1.82 CO 1615A GPM 9.30 FLOWLINE TEMPERATURE 49.9°C DP AN VEL 182 3 FT/MIN SHALE DENSITY - DC AN VEL 25.3.3 FT/MIN		13
SHALE FACTOR CRITICAL VEL 332.4 FT/Min MAX. FORMATION GAS 40.0000 @ 1564 BACKGROUND GAS 40.0000 @ 1564 BACKGROUND GAS 40.0000 @ 1564 CONNECTION GAS 40.0000 @ 1564 PRESS(BIT) 2554 PSI PRESS(BIT) 2554 PSI PRESS(SYSTEM) 2760 PSI BIT NOZ VEL 4000 PSI CALCILUTITE AN. VOL PIPE VOL 391 FIPE DISPL. 44 BIT TYPE HTC X3A	CORRECTED D EXPONENT <u>1.58 (c. 15.54 1.82 (c. 16154</u> FLOWLINE TEMPERATURE <u>49.9 °C</u> SHALE DENSITY <u>-</u> SHALE FACTOR MAX. FORMATION GAS <u>40 units</u> CONNECTION GAS <u>1564</u> TRIP GAS <u>-</u> LITHOLOGY:	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
JETS 3×18		JETS 3×18
MUD WT. IN 9×1 $PV/YP B/13$ Av. WOB $4C$ MUD WT. OUT $9 \cdot 3$ $CL - 60\pi$ Av. RPM 158 ECD $9 \cdot 3$ 6 SOLIDS 6Av. TORQUE 4000	MLD WT. OUT 9.3 CL- 602	AV. WOB 40 AV. RPM 158
ESTIMATED PORE PRESS 8.5 22/902 TIGHT HOLE - MAX. ESTIMATED PORE PRESS IN OPEN HOLE 8.5 FILL - ESTIMATED FRACTURE PRESS 15.7 18/902 Δ LAG + 120 STROKES MIN. EST. FRAC. PRESS. IN OPEN HOLE 14.016/90 EST. CAVINGS -	ESTIMATED PORE PRESS 8:5 22 gal Max. ESTIMATED PORE PRESS IN OPEN HOLE 8:5 ESTIMATED FRACTURE PRESS 15.7 16/and	FILL - A LAS + IDO STROKES
COMMENTS:		

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4 1 , constant and the second PETROLEUM ENGINEERING SUMMARY REPORT COMPANY ESSO AUSTRALIA WELL NAME FORTESCUE NO. 2 DATE 5. + NOV. 1978 TIME 0600 DEPTH - 1374 LAST REPORT DEPTH _____ 1135 M SPM ______ DAILL RATE 15M/HR average. CORRECTED D EXPONENT 1.27 @ 1260m 1.45 P135M GPM_____ 950 DP AN VEL 186.2 FT/MIN FLOWLINE TEMPERATURE 45.2°C 258.7 FT/MIN DC AN VEL SHALE DENSITY CRITICAL VEL 293.1 FT /MIN SHALE FAGTOR 16 units @ 1135M PRESS(TOTAL) 2656PS1 MAX. FORMATION GAS BACKGROUND GAS <u>5 To 8 units</u> PRESS(BIT) 2/60 PS/ PRESS(SYSTEN) 2730 PSI CONNECTION GAS ______ BIT NOZ VEL 409 FT /SEC 60 units @ 1237M TRIP GAS 777 881 HOLE VOL LITHOLOGY1 649 881 AN. VOL____ CALCISILTITE. 74 881 PIPE VOL FIPE DISPL. 56 BB1 #4. HTC X3A BIT TYPE 3×18. JETS 38000 16 PV/ P - 7/14 MUD WT. IN 9.1 16/cal AV. WOB 121 CL- 8600 AV. RPM MUD NT. OUT 9.2 16/GAL 9.2 16/0A1 \$ SOLIDS 7 3800 FT 16 AV. TORQUE ECD ESTIMATED PORE PRESS 8.5 16/641 TIGHT HOLE FILL MAX. ESTIMATED PORE PRESS IN OPEN HOLE 8.5 A LAG _ EATIMATED PRACTURE PRESS 15.7 16/601 EST. LCAVINGS HEN. EST FRAC. PRESS. IN OPEN HOLE 14.0 16(0) _ CONNENTS: ينبع كوالد المتواد

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PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY <u>ESSO AUSTRALIA</u> WELL NAME <u>FORTESCUE #2</u> DATE <u>4. NOV. 1978</u> DEPTH <u>1135</u> LAST REPORT DEFTH	
DRILL RATE $15m/HR$ CORRECTED D EXPONENT $1.14@1020m + 1.22@1135m$ FLOWLINE TEMPERATURE $36.1^{\circ}C$ SHALE DENSITY	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
MUD NT. IN 9.1* 16/01 PV/YP 8/13 MUD NT. OUT 9.3 16/01 CL- 8 CCC ECD 9.3 16/01 % SOLIDS 7 ESTIMATED PORE PRESS 8.5 16/001 MAX. ESTIMATED PORE PRESS IN OPEN HOLE 8.5 ESTIMATED FRACTURE PRESS IN OPEN HOLE 8.5 MIN. EST. FRAC. PRESS. IN OPEN HOLE 14 16/001	Av. WOB 28000 16 Av. RPM 120 Av. TORQUE 3500 FT 16 TIGHT HOLE - FILL - ALAG - 150 STROKES EST. & CAVINGS -

COMMENTS:

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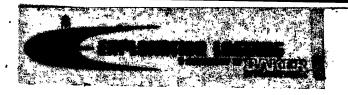
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PETROLEUM ENGINEERING SUMMARY REPORT

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COMPAN	Y ESSO AUSTRALIA		
WELL NAN	E FORTESCUE #2	_	•
DATE	2. Nov. 1978	_ TIME 060	0
	878M LAST REPORT DEFT		
SHALE DENSIT Shale factor Max, formati Background g Connection g Trip gas Lithology:		DC AN VEL CRITICAL VE PRESS(TOTAL PRESS(BIT) PRESS(SYSTER BIT NOZ VEL HOLE VOL AN, VOL	90.6 FT /MIN 103.5 FT /MIN 293.6 FT /MIN 2256 PSI 1396 PSI 363 FT /SEC 928 BBI 843 BBI 445 BBI
ECD	1 <u>N 9.4 16/6A1</u> PV/YP 7/15 OUI 10.0 16/6A1 CL- 9.8 16/6A1 % SOLIDS	BIT TYPE JETS	HTC OSC 3A5 3×20 29000 16 120 4000 FT 16
LOTIMATED PO	PE PRESS 8.5 16/6AI	TIGHT HOLE FILL A LAG	
MIN, EST. FRA	AC. PRESS. IN OPEN HOLE	EST. SCAVINGS	
COMMENTS :	DRILLING WITH SEAWA BACK GROUND GAS INCREASE AT 450 M TO AN AVERAGE POOH @ 878M TO RUN AND 1330' CASING.	D STEADILY) OF 40 UNIT	5 AT 878M



PETROLEUM ENGINEERING SUMMARY REFORT

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i.

COMPANY <u>ESSO AUSTRALIA</u> WELL NANE <u>FORTESCUE #2</u> DATE <u>J. NOU. 1978</u> DEPTH - 390 M LAG DEPOSE DETER	
DEPTH 390 M LAST REPORT DEPTH	
DRILL PATE <u>180 m /HR AVE</u> CORRECTED D EXPONENT <u>0.47 To 0.60</u> FLOWLINE TEMPERATURE <u>21.2°C</u> SHALE DENSITY <u>-</u> SHALE FACTOR <u>-</u> MAX, FORMATION GAS <u>10 UNITS</u> BACKGROUND GAS <u>3 To 6 UNITS</u> CONNECTION GAS <u>NIL</u> TRIP GAS <u>NO TRIPS</u> LITHOLOGY: <u>CALCARENITE WITH MINCR</u> <u>CALCAREOUS SILTSTONE</u>	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
MUD WT, IN 8.5 TO 9.3 16/001 PV/YP 7/15	BIT TYPE HTC OSC 3AS JETS 3 × 20 AV. WOB 25000 1b
MLO 1 + OUI 8.6 To 9.4 16/601 CL	AV. RPM - 120
ECD 9.2 16/6A1 % SOLIDS - ESTIMATED POPE PRESS 8.5 16/6A1	AV. TORQUE 3500 FT 16 TIGHT HOLE -
MAX. ESTIMATED PORE PRESS IN OPEN HOLE 8.5 ESTIMATED FRACTURE PRESS MIN. EST. FRAC. PRESS. IN OPEN HOLE	FILL - A LAG - EST. & CAVINGS -
COMMENTS: DRILLING WITH SEAW	oter [solids

. با مشاهد ا FETROLEUM ENGINEERING SUMMARY REFORT COMPANY ESSO AUSTRALIA WELL NAME FORTESCUE #2 DATE 9. NOV. 1978 TIME 0600 DEPTH _ 2235M LAST REPORT DEFTH ____ 2017M SPM______112_____ ORILL PATE 36m/HR average GPM 970 FORHECTED I EXPONENT 1.21 @ 22354 DP AN VEL 190.1 FT/MIN FLOWLINE TEMPERATURE 50.8°C DC AN VEL 264.2 FT/MIN SHALE DENSETY -CHINEAL VEL 299.7 FT/MIN ----SHALE FACTOR ____ PRESS(TOTAL) 3524 PSI 9 UNITS MAX, FORMATION GAS PHESS(BIT) 3521 PSI BACKGROUND GAS 775 8 UNITS FRESS (SYSTER) 2660 PSI CUNNECTION GAS _____ NiL BIT NOT VEL 387 FT/SEC 5 UNITS @ 2142M TRIP GAS 1198 BBI HOLE VOI LITHOLOGY: 988 BBI AN. VEL CALCAREOUS HUDSTONE 120 BBI PIPE VOL FIRE DISFL. 80 BBI HTC X3A BIT TYPE 18,18,20 JI 13 42000 lb MUD VT. IN 9.1 16/6AL P.V/YP 11/14 AV. WOB MLD #1. OUI 9.4 15/6A1 CL- 4100 155 AV. RPM 6000 FTID ECD 9.3 16/6A1 % SOLIDS 11 AV. TORQUE ESTIMATED POPE PRISS 8.5 TIGHT HOLE _ FILL MAX. ESTIMATED PORE PRESS IN OPEN HOLE 8.5 + 613 STROKES A LAG ESTIMATED FRACTURE PRESS 15.7 16/6A1 EST. SCAVINGS MIN. EST. FRAC. PRESS. IN OPEN HOLE 14 16/CAI Blocked flowline @ 2146 m. COMMENTS:

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PETR	OLEUM ENGINEERING	SUMMARY REF	RI	_
COMPANY _	ESSO AUSTRI	akiA		
WELL NAME	FORTESCUE	No. 2		
DATE	<u> .</u> NOV. 1978	,	TIME	0600
DEPTH	2420M LAST	REPORT DEFTH	2	235-
ORPECTED D EX	10 m /HR are PONENT 148 Q. HATCHE 5870	8420m	GPM	
MALE DENSETY	-		DC AN VEI	260.1 ft/min
HALE FACTOR				VI: 320.4 ft forin
AX. FORMATION		•	1	1 AL) <u>3732 PS1</u> 1) <u>3906 PS1</u>
	<u>3 to 4 n</u>	inits	1	, · [N) 23.70 ps 1
	nil nil	24200	RET NOT	VI: 381 ft /sic
RIF GAS	12 units 1	rom 2420m	HOLE VOL	1276 ft
ITHOLUGY:	Calcareous Mudsto	ne /marl.		1061 bbl
	Carcer a loss		PIPE VOL	135 UU
		·	FIFE DISI	
			Bit Type	
			JETS	18,18,20
Mico wit	IN 9.3 16/gal	EV/VP 14/16	AV. WOB	35000 11-
	001 9.4 lb/gal		AV. PPM	
ECD	9.4° 14/001	% SOLIDS 20	AV. TOR	EUE 5500 ft lbs
ESTIMATED POP	E PRESS 8.	\$ SOLIDS 20 5 lb/gal	ТІСНТ Н	
MAX. ESTIMATE	D PORE PRESS IN	OPEN HOLE 8.5	FILL	-
ESTEMATED FRA	ACTURE PPESS	5.7 lb/ga	A LAG	+ 613 stroken
	C. PRESS. IN OPE			
COMMENTS:	Strapped out Currently in	of hole @ 2 culating to	420m 1 toms up	Made up core borrell prior to culting
	Core #1	<i>v</i>		

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PETROLEUM ENGINEERING SUMMARY REFO	71
COMPANY ESSO AUSTRALIA	
WELL NAME FORTESCUE No. 2	-
DATE 10. Nov. 1978	TIME0600
DEPTH 2436m LAST REPORT DEFTH	2420M
	30
CRILL PATE <u>D.8m/Hr average</u>	SPM30 GPM260
FLOWLINE TEMPERATURE 47% 0C	DP AN VEL
SHALE DENSITY -	DC AN VEL
SHALE FACTOR	CHEVECAL VEL
MAX, FORMATION HAS 2 units	PHESS(TOTAL)
BACKERDUND CAS 1 to 2 units	FRESS(BIT)
CONNECTION GAS <u>nil</u>	FRESS(SYSTER) 970 PSI
IPIN GAS 12 units @ 2420m	BIT NOT VEL
LITHOLOGY:	HOLE VOI 12 79 HL
Calcareous mudstone / mart	AN, VIL 1062 CUL PIPE VCL 136-5 COL
	FIFE DISIL. SOST
	Ell TYPE Chris C22
	()
MUD VT. IN 9-3 11/gal EV/YP 14/16	AV. WOB 2800 ll
MUD WT. IN 9-3 lt/gal PV/YP 14/16 MUD WT. OUT 9-6 lt/gal CL- 3400	AV. RPM 85
ECD 9.5 lt/gal % Solid: 13	AV. TORQUE 3100 It ll
ESTIMATED POPE PRESS 85	TIGHT HOLE
MAX. ESTIMATED PORE PRESS IN OPEN HOLE 8.5	FILL -
ESTIMATED FRACTURE PRESS 15.7 W/gal	A LAG. T 613 stroken
MIN. EST. FRAC. PRESS. IN OPEN HOLE H lifed	EST. & CAVINGS -
COMMENTS: Cut Core # 1 from 24 Port with core for	20m to 2436m
TOOH With Core for	
	22 - 17 - 2 17 - 2 17 - 17 - 17 - 17 - 1

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(0 PETROLEUM ENGINEERING SUMMARY REFORT COMPANY ESSO AUSTRALIA WELL NAME FORTHESCUE NO. 2 DATE 12. NOV. 1978 TIME 0600 DEPTH 2464M. LAST REPORT DEFTH 2436m. DRILL PATE Reaming @ 23m/HR. SPM 74 640 GPM CORRECTED D EXPONENT DP AN VEL FLOWLINE TEMPERATURE 4-3-3°C DC AN VEL SHALE DENSITY CRITICAL VEL SHALE FACTOR PRESS(TOTAL) 4 units MAX, FORMATION GAS PRESS(BIT) BACKGROUND GAS 15 units. PRESS(SYSTEN) 2550 PSI. CONNECTION GAS _____ rie 35 units @ 2464m. BET NOZ VEL TRIP GAS 1296 600 HOLE VOI LITHOLOGY: Sand. 1073 bl AN. VCL 137 bll PIPE VOL 86 bll FIPE DISPL. HTC XDG BIY TYPE 14, 15, 15 JITS MUD VT. IN 9.3 ll/gal PV/YP 13/15 30000 Ur. AV. WOB MLD WI. OUT 9.6+ lu/gel CL- 3900 AV. REM 120 9.5 W/gel 1% SOLIDS 12 3000 H U E CD AV. TORQUE 8.5 lr /gal TIGHT HOLE ESTIMATED PORE PRESS FILL MAX. ESTIMATED PORE PRESS IN OPEN HOLE 85 +613 stoken ESTIMATED FRACTURE PRESS 15.7 World AND A LAS EST. BOAVINGS MIN. EST. FRAC. PRESS. IN OPEN HOLE 14 lb/gal. Reamed out not hole from 2420m to 2464m, POOH to cut Core #3. COMMENTS:

PETROLEUM ENGINEERING SUMMARY REFORT COMPANY ESSO AUSTRALIA WELL NAME FORTESCUE No. 2 1412 NOV. 1968 TIME 0600 DATE 2600 LAST REPORT DEFTH 2464M DEPTH 76 DRILL RATE <u>32m/HR OTD.</u> SPM 660 GPM_____ CORRECTED D EXPONENT 1.16 @ 2490m to 1.78@ 26000 DP AN VIL 129.4 ft/men FLOWLINE TEMPERATUR<u>E 50.2°C</u> 179.8 ft/min DC AN VEL SHALE DENSITY 383.4 ft/min CRETECAL VEL SHALE FACTOR PHESS (TOTAL) 2922 PSI 4 units MAX. FORMATION GAS PRESS(BIT) 4190 PSI BACKGROUND GAS _____ I to 2 units PRESS (SYSTEN) 2710 PSI CONNECTION GAS ______ 409 pt/sec 22 units @ 2480m BET NOZ VEL TRIP GAS 1360.4 bll. HOLE VOL LITHOLOGY: 1124.7 661 filtations & Coal @ 2580m AN, VCL 143.5 661 PIPE VOL 92·2 bbl EIPE DISPL. HTC XDG BIT TYPE 3×15. JETS 43000 ll . MUD VT. IN 9.2 Ulgal PV/YP 15/23 AV. WOB 120 MLD WT. OUT 9.6 lb/gal CL- 3900 AV. RPM 4500 FT lb. 9.6 lb/gal \$ SOLIDS 12 AV. TORQUE ECD TIGHT HOLE ESTIMATED PORE PRESS 8.5 6/10 FILL MAX. ESTIMATED PORE PRESS IN OPEN HOLE 8-5 A LAG ESTIMATED FRACTURE PRESS 15.7 lb/gal EST. &CAVINGS MIN. EST. FRAC. PRESS. IN OPEN HOLE 14/11/100 Poot @ 2600m for new bit. COMMENTS:

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PETRULEUM ENGINEERING SUMMARY REFORT COMPANY ESSO AUSTRALIA WELL NAME FORTESCUE No 2 15th Nov 78 TIME 0600 am DATE 2600 DEPTR 2653 LAST REPORT DEPTH ____ Average 18 m/hr SEM CPICS PATE DRHEECED J EINGNENT 1215 at 2620 to 1-63 et 2604 680 S-MA 133 H/mi DP AN VEN FLOVEFRE SEMPERATORS 4977 C 185 A DC AN VEL SPACE BEN STY 366 H/m CHEFTERS VEL SHALE - ACTON 3 units PHESSERDIAL) 268a HAR, FORMATEON CAS r 1351 66ESS (017) BACHGROUNDIGAS 1=2 mits B29 FEFES(SVATEN) FUNNECTEDS GAS 403 Ft / sec 2600 m 18 mits BIN NOT VEL TRIN CAS 1388 bbl HELE VOL 70% sandstone ETTHOLOGY: 666 1153 30% AN. YEL siltston /shale 150 PIPE VCL FIRE DISSL. 85 NE # 12 HTC XDG BIT TYPE 15,15,16 JE 13 1 V/YP 17/22 45,000 / 9×2 AV. ACB MUD WT. HN 128 9,5 AV. DEM MUN AT. CUT CI- 3900 5,000 A/L 13 9,6 Scill: AV. TORSUL ECD TIGHT HOLE 8.5 1619A ESTEMATED POTE PRE FILL MAX. ESTIMATED PORE PRESS IN OFFIL HOLE 8.5 A LAS ESTEMATED FRANTURE PRESS 16.0 Est Bravings -MIN, EST. FRAC. FRESS. IN OPEN HOLE 14.0 RIH with NR # 12 HTC XDG and drill COMMENTS: from 2600 m to 2653 m. of 2653m. log Poot h operation windline Present



REPLY TO: EXPLORATION LOGGING INTERNATIONAL INC. 2006, ORCHARD TOWERS, 400 ORCHARD ROAD, SINGAPORE 9. TELEPHONE: 2354544 (4 LINES) TELEX: RS 21084

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REGISTERED ADDRESS: APARTADO 850 PANAMA REPUBLIC OF PANAMA

ESSO AUSTRALIA, FORTESCUE NO.2 EXPLORATION LOCGING, UNIT 101, OCEAN DIGGER. WEEKLY REFORT NO.1 : 256 TO 879 M

24(0 HES 2ND NOV. 1978

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DRILLING SU"MARY

The well was spudded on the 30th of october 1978. 26" hole was drilled to 256 metres without a marine riser. A HTC OSC 3AJ was used and drilling time was $7\frac{3}{4}$ hours.

20" CASING WAS SET AT 236 METRES AND THE MARINE RISER AND STACK WERE RUN. THE CASING SHOE AND CEMENT WERE DRILLED OUT WITH A 17^3 " HTC SC 3AJ which was also used to drill 17^3 " Hole to 879 Netres. At 878 Metres the bit was pulled and the following Schlumberger Logs were run: 19F-SONIC, FDC-GR, and caliper. 13 3/8" casing was then run.

A SEAWATER/SOLIDS AND GEL MUD SYSTEM WAS USED TO DRILL THE SECTION. PECBUSE OF THE HIGH DRILLING RATE AND THE NATURE OF THE FORMATION. A LARGE AMOUNT OF SOLIDS WERE CONTRIBUTED TO THE SYSTEM BY THE FORMATION. As a result the mud weight increased rapidly from 8.6 LB/CAL to 10 LB/GAL. DESPITE THE AUDITION OF WATER TO THE SYSTEM THE WEIGHT MAINTAINED ITSELF AT ABOUT 9.4 LB/GAL.

DRILLING PARAMETERS

LITHOLOGY: OVER THE SECTION THE FORMATION CONSISTED OF A FAIRLY MONOTONDUS SEQUENCE OF SOFT ARENACEOUS AND ARGILLACEOUS LIMESTONES. THESE WERE NAMED ACCORDING TO GRAIN SIZE AND THE TERMS CALCARENITE, CALCISILTITE AND CALCILUTITE WERE USED. THESE LIMESTONES CONTAINED ABUNDANT FORAMS AND OTHER FOSSIL FRAGMENTS.

DRILL RATE: DRILL RATES WERE EXTREMELY FAST WITH 400 TO 500 M/HR BEEN COMMON IN THE TOPMOST SECTION WHICH CONSISTED OF COARSE AMENACEOUS LIMESTONE. A STEADY DECREASE IN DRILL RATE BECAME APPARENT AS THE ROCKS BECAME NORE COMPACTED WITH DEPTH. AT 725 NETPES AN ATEMPT WAS MADE TO CONTROL THE DRILL RATE AND WAS MAINTAINED AT 25 TO 30 M/HR UNTIL 879M.

DXC : AS A RESULT OF THE HOMOGENITY OF THE FORMATION IN THE SECTION THE DXC SHOWS A GOOD COMPACTION TREND, HOWEVER DUE TO THE ABSENSE OF CLEAN SHALES IN THE SECTION THE USE OF DXC FOR PRESSURE DETERMINATION IS LIMITED.

GAS: READINGS WERE TYPICALLY $\frac{1}{2}$ UNIT DOWN TO 450 METRES WHERE FOLLOWING A DRILLING BREAK THE BACK GROUND INCREASED TO 10 UNITS. FURTHER DRILLING BREAKS AT 600 METRES RESULTED IN A BACKGROUND OF 30 TO 40 UNITS. THE MAXIMUM GAS RECORDED WAS 74 UNITS AT 717 METRES. A WIPER TRIP PRIOR TO RUNNING 20" CASING GAVE TRIP GAS OF 15 UNITS ABOVE THE BACKGROUND.

CHPOMATAGIAPH ANALYSIS INDICATED THAT THE GAS WAS C1 (METHANE) WITH NO HEAVIER HYDROCAFBONS PRESENT.



REPLY TO: EXPLORATION LOGGING INTERNATIONAL INC. 2006, ORCHARD TOWERS, 400 ORCHARD ROAD, SINGAPORE 9. TELEPHONE: 2354544 (4 LINES) TELEX: RS 21084

> REGISTERED ADDRESS: APARTADO 850 PANAMA REPUBLIC OF PANAMA

TEMPERATURE: THE TEMPERATURE PLOT SHOWS A STEADY INCREASE OVER THE INTERVAL WITH NO ANOMOLOUS TRENDS APPARENT.

HOLE CONDITION .

THE HOLE CONDITION REMAINED GOOD WITH NO NOTFABLE DRAG ON CONNECTIONS OF ON TRIPS. THE CALIPER LOG SHOWED THE HOLE TO BE WASHED OUT AT 200 METRES, GENERALLY THE HOLE REMAINED IN GAUGE THROUGHOUT THE REST OF THE SECTION, HOWEVER SOME WASH OUT WAS APPARENT AT CONNECTIONS.

PPESSURE INDICATOPS

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NO ABNORMAL PRESSURE IS INDICATED BY THE DXC AND TEMPERATURE PLOTS. THIS TOGETHER WITH THE LACK OF CONNECTION GAS DESPITE A HIGH BACKGROUND INDICATES THAT THE PRESSURE GRADIENT REMAINS NORMAL AT 8.4 TO 8.5 LB/GAL.

S.R./J.H.

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REPLY TO: EXPLORATION LOGGING INTERNATIONAL INC. 2006, ORCHARD TOWERS, 400 ORCHARD ROAD, SINGAPORE 9. TELEPHONE: 2354544 (4 LINES) TELEX: RS 21084

> REGISTERED ADDRESS: APARTADO 850 PANAMA REPUBLIC OF PANAMA

ESSO AUSTRALIA, FORTESCUE NO.2 EXPLORATION LOGGING, UNIT 101, OCEAN DIGGER. WEEKLY REPORT NO.2 : 879m to 2436m

10TH Nov. 1978

DRILLING SUMMARY

The 13 3/8" casing was run and cemented at 861 metres. NB #3 a HTC X3A was run into the hole and used to drill out the cement and casing shoe. New hole was drilled to 894 metres where a pressure integrity test was performed. The hole was pressured to an equivalent mud wieght of 13.5 lb/gal without any leak off occurring. The fracture pressure at the shoe is estimated to be 15.7 lb/gal EMW, Bit #3 drilled to 1238m at an average rop of 19.4 m/hr, NB #4 also a HTC X3A drilled to 1615m at an average rop of 12.2m/hr, NB #5 another HTC X3A drilled to 2142m at an average rop of 19.9m/hr, NB #6 another HTC X3A drilled to 2420m at an average rop of 16.6 m/hr. At 2420m core barrell #1 with a Christensen C22 was run into the hole and a core cut from 2420m to 2436m. The average coring rate was 0.8 m/hr.Surveys were run at each bit change and the following results obtained; 0° at 879m , 2 3/4° at 1238m, 0° at 1615m , $\frac{1}{2}$ ° at 2142m , and 2° at 2420m. Mud wieght was kept at 9.1 lb/gal until 2345m where it was built up to 9.3 lb/gal.

AFTER THE TRIP.AT 2142M THE FLOW LINE BECAME BLOCKED AND TOOK APPROXIMATELY TWO HOURS TO CLEAR. IT AGAIN BECAME PARTIALLY BLOCKED AT 2311M AND WAS CLEARED AGAIN IN A FEW MINUTES.

DRILLING PARAMETERS

LITHOLOGY: FROM 879 TO 1690M : CALCISITITE, SOFT TO FIRM.WITH A MINOR INVASION OF MARL FROM 980M TO 1120M, WITH SOME SPARRY MICRITE AND CALCARENITE INTERBEDS.

FROM 1690 TO 1850N: MEDIUN GREY CALCAREOUS SILTSTONE

FROM 1850 TO 2420M: CALCAREOUS MUDSTONE GRADING LOCALLY TO MARL.

DXC : TREND VARIATIONS ARE DIVIDABLE INTO THREE SECTIONS RELATED TO THE LITHOLOGY IN EACH SECTION, UP TO 1615M A COMPACTION TREND FOR THE ARENACEOUS LIMESTONES IS PRESENT. FROM 1615 TO 1725M IS A TRANSITION ZONE OVER WHICH THE FORMATION CHANGES FROM A CALCAREOUS SILTSTONE TO CALCAREOUS MUDSTONE. FROM 1725 TO 2420 METRES A COMPACTION TREND IN THE MUDSTONE IS EVIDENT. IT IS NOT BELIEVED THAT THE KICKBACK IN TREND AT 1615 IS AN INDICATION OF ABNORMAL PRESSURE BUT RATHER A REFLECTION OF THE TRANSITIONAL NATURE OF THE LITHOLOGY IN THE INTERVAL.

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REPLY TO: EXPLORATION LOGGING INTERNATIONAL INC. 2006, ORCHARD TOWERS, 400 ORCHARD ROAD, SINGAPORE 9. TELEPHONE: 2354544 (4 LINES) TELEPK: RS 21084

4

REGISTERED ADDRESS: APARTADO 850 PANAMA REPUBLIC OF PANAMA

TEMPERATURE : A PLOT OF THE FLOWLINE TEMPERATURE GIVES A GRADIENT OF 1.21° C PER 100 METRES.FROM 1000 TO 1375M THE TREND FIRST DECREASES THEN SHARPLY INCREASES. THE DECREASE WAS CAUSED BY LARGE ADDITIONS OF WATER TO THE MUD SYSTEM AND THE INCREASE IS DUE TO RESTABILIZATION AFTER A TRIP. A SECOND LARGE DEVIATION OCCURRED OVER THE INTERVAL, 1615 TO 1725M. THIS IS BELIEVED TO HAVE BEEN CAUSED BY THE CHANGE IN LITHOLOGY AND FURTHER ACCENTUATED BY THE ADDITION OF WATER TO THE SYSTEM AND RESTABILIZATION AFTER A TRIP.

GAS : THERE HAS BEEN A STEADY OVERALL DECREASE IN FROM 879H TO TD, FROM 50 UNITS TO 4 UNITS. THERE WERE NO NOTABLE PEAKS AND NO CONNECTION GASES. TRIP GASES WERE 34,60,12,5, AND 12 UNITS. CHROMATAGRAPH ANALYSIS INDICATED THAT THE GAS WAS PREDOMINANTLY C1 WITH TRACE AMOUNTS OF C2.

HOLE CONDITION

A CARBIDE RUN AFTER THE BLOCKED FLOW LINE WAS CLEARED GAVE A DIFFERENCE OF \pm 613 strokes as compared to the theoretical lag. Before this the difference had been 120 strokes. This suggests that the hole may be washed out at around 2143m with possibly as much as 126 bbls increase in volume.

PRESSURE INDICATORS

ALL DEVIATIONS IN PRESSURE PARAMETER TRENDS ARE READILY ACCOUNTED FOR BY SURFACE ACTIVITY SUCH AS ADDING WATER TO THE MUD SYSTEM AND BY LITHOLOGICAL VARIATIONS. THE PRESSURE GRADIENT IS BELIEVED TO REMAIN NORMAL AT 8.4 TO 8.5 LB/GAL.

S.R./S.D.

A SUBSIDIARY OF BAYATIONAL

REPLY TO: EXPLORATION LOGGING INTERNATIONAL INC. 2006, ORCHARD TOWERS, 400 ORCHARD ROAD, SINGAPORE 9. TELEPHONE: 2354544 (4 LINES) TELEX: RS 21084

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REGISTERED ADDRESS: APARTADO 850 PANAMA REPUBLIC OF PANAMA

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ESSO AUSTRALIA FORTESCUE NO.2 ODECO OCEAN DIGGER EXPLORATION LOGGING UNIT #101 17 NOVEMBER 1978 2436H - 2653H WEEKLY REPORT #3

DRILLING SUMMARY

01111	BIT	START	FINISH	AV, ROP	RECOVERY	1KTP 045
CORE#1	C22	2420m	2436 M	0 . 8m/HR	97%	52u
CORE#2	C22	2436M	245 1 H	2.3M/HR	79%	2u
CORE#2 Core#3	C22	2451 m	246 4 m	3.3M/HR	81%	10u
CORE#4	C20	2464M	2480m	3.8m/HR	87.5%	22u

A REAMING TRIP WAS CONDUCTED WITH A $12\frac{1}{4}$ " bit at 2464m. New bit #8, A 124"HTC XDG, REAMED THE RAT-HOLE AND DRILLED ON TO 2600M AT AN AVERAGE PENETRATION RATE OF 13.1M/HR. BIT#9, ANOTHER 122"HTC XDG DRILLED TO T.D. AT 2653M AT AN AVERAGE PENETRATION RATE OF 18.8M/HR. THE AVERAGE MUD WEIGHTS USED THROUGHOUT THE INTERVAL WAS 9.4PPG. AFTER A WIPER TRIP THE HOLE WAS CIRCULATED CLEAN IN PREPARATION FOR WIRELINE LOGGING. LOGS RUN AT T.D. WERE IES/SONIC, FDC/CNL, HDT, CIS, RFT, CST.

DRILLING PARAMETERS

LITHOLOGY: OIL SAND WAS FOUND IN CORE#2 AND CORE#3, WITH THE OIL/ WATER CONTACT THOUGHT TO BE IN THE BASE OF CORE#3. NO OIL FLUORESCENCE WAS SEEN IN CORE#4. FROM 2480M TO TD THE SECTION CONSISTED OF COARSE SANDS IN THE UPPER PART, WITH NODERATELY FINE SANDS AND SILTSTONES WITH SHALES AND MINOR COAL IN THE LOWER PART OF THE INTERVAL. NO OIL SHOWS WERE DETECTED OTHER THAN THOSE IN THE CORES.

DXC: THE HIGHLY VARIABLE LITHOLOGY WAS REFLECTED IN THE DRILLING RATES, CONSEQUENTLY DXC VALUES VARIED ACCORDINGLY. OVER THE SECTION DRILLED THERE WAS NO INDICATION OF TREND DEVIATION AS A RESULT OF GEOPRESSURES.

TEMPERATURE: A TEMPERATURE TREND DURING CORING OPERATIONS WAS NOT OBTAINABLE DUE TO THE RELATIVELY SHORT PERIODS OF DRILLING AND "IRCULATION. HOWEVER, UPON RESUMING DRILLING AFTER CORING, THE

"VLINE TEMPERATURE STABILISED, PRODUCING A CONTINUING TREND OF °C /100m.



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211

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REPLY TO: EXPLORATION LOGGING INTERNATIONAL INC. 2006, ORCHARD TOWERS, 400 ORCHARD ROAD, SINGAPORE 9. TELEPHONE: 2354544 (4 LINES) TELEX: RS 21084

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REGISTERED ADDRESS: APARTADO 850 PANAMA REPUBLIC OF PANAMA

GAS: THROUGHOUT THE INTERVAL THE MAXIMUM DITCH GAS RECORDED WAS 4U, THE AVERAGE BACKGROUND BEING 2U. THE LOW RECORDINGS ARE A FUNCTION OF THE HIGH OVERBALANCE IN THE BOREHOLE.

HOLE CONDITION

CAVINGS IN THE SAMPLES TO 2490H WERE LESS THAN 5% IN THE CUTTINGS COLLECTED. BELOW 2490H COARSE SAND CAVED CONSISTANTLY FROM THE LATROBE GROUP. ALSO FROM 2600H TO TD THERE WAS A CONSISTANT 2-5% SHALE CAVINGS IN THE SAMPLE. THE SAND CAVING IS DUE TO THE LACK OF COHESION BETWEEN THE GRAINS IN THE FORMATION, AND IT IS THOUGHT THAT THE SHALE CAVINGS WERE FROM 2140H APPROX.

PRESSURE INDICATORS

GAS, DXC, QUALITY OF SAMPLE AND GEOLOGICAL PARAMETERS INDICATE THAT THE SECTION DRILLED HAS A NORNAL HYDROSTATIC PORE PRESSURE OF APPROX 8.5PPBEMW. LOW TRIP GASES AND NEGLIGIBLE BACKGROUND GAS IS A RESULT OF THE OVERBALANCE OF 1PPG (ECD WAS 9.5-9.6PPG), WHICH WOULD ALSO CAUSE EXTENSIVE FLUSHING OF FORMATION FLUIDS.

S.DAINES / J.NOLAN

This is an enclosure indicator page. The enclosure PE603445 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603445 has the following characteristics: ITEM_BARCODE = PE603445 CONTAINER_BARCODE = PE906133 NAME = Temperature Data Log BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELL SUBTYPE = WELL_LOG DESCRIPTION = Temperature Data Log for Fortescue-2. REMARKS = DATE_CREATED = 30/11/1978DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED

(Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603446 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603446 has the following characteristics: ITEM_BARCODE = PE603446CONTAINER_BARCODE = PE906133 NAME = Pressure Analysis Log BASIN = GIPPSLAND PERMIT = VIC/L5 TYPE = WELL SUBTYPE = WELL_LOG DESCRIPTION = Pressure Analysis Log for Fortescue-2 showing overburden gradient and fracture pressure curves. REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603447 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603447 has the following characteristics: ITEM_BARCODE = PE603447 CONTAINER_BARCODE = PE906133 NAME = Mud Log 1 of 27BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELL SUBTYPE = MUD_LOG DESCRIPTION = Mud Log 1 of 27 for Fortescue-2 (in separate pages) legend and title REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED

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This is an enclosure indicator page. The enclosure PE603448 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603448 has the following characteristics: $ITEM_BARCODE = PE603448$ CONTAINER_BARCODE = PE906133 NAME = Mud Log 2 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 2 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979 $W_{NO} = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603449 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603449 has the following characteristics: ITEM_BARCODE = PE603449 CONTAINER_BARCODE = PE906133 NAME = Mud Log 3 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 3 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ $DATE_RECEIVED = 26/04/1979$ $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED

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This is an enclosure indicator page. The enclosure PE603450 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603450 has the following characteristics: ITEM_BARCODE = PE603450 CONTAINER_BARCODE = PE906133 NAME = Mud Log 4 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5 TYPE = WELL SUBTYPE = MUD_LOG DESCRIPTION = Mud Log 4 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ $DATE_RECEIVED = 26/04/1979$ $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603451 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603451 has the following characteristics: ITEM_BARCODE = PE603451 CONTAINER_BARCODE = PE906133 NAME = Mud Log 5 of 27BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELL SUBTYPE = MUD_LOG DESCRIPTION = Mud Log 5 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979W NO = W709WELL NAME = FORTESCUE-2CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED

(Inserted by DNRE - Vic Govt Mines Dept)

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This is an enclosure indicator page. The enclosure PE603452 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603452 has the following characteristics: $ITEM_BARCODE = PE603452$ CONTAINER_BARCODE = PE906133 NAME = Mud Log 6 of 27BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELL SUBTYPE = MUD_LOG DESCRIPTION = Mud Log 6 of 27 for Fortescue-2 (in separate pages) REMARKS = DATE CREATED = 30/11/1978DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED

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This is an enclosure indicator page. The enclosure PE603453 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603453 has the following characteristics: ITEM_BARCODE = PE603453 CONTAINER_BARCODE = PE906133 NAME = Mud Log 7 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5 TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 7 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603454 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603454 has the following characteristics: ITEM_BARCODE = PE603454 CONTAINER_BARCODE = PE906133 NAME = Mud Log 8 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 8 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603455 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603455 has the following characteristics: $ITEM_BARCODE = PE603455$ CONTAINER_BARCODE = PE906133 NAME = Mud Log 9 of 27BASIN = GIPPSLAND PERMIT = VIC/L5 TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 9 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603456 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603456 has the following characteristics: ITEM_BARCODE = PE603456 CONTAINER_BARCODE = PE906133 NAME = Mud Log 10 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 10 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979W NO = W709WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603457 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603457 has the following characteristics: ITEM_BARCODE = PE603457 CONTAINER_BARCODE = PE906133 NAME = Mud Log 11 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 11 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ $DATE_RECEIVED = 26/04/1979$ $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED

(Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603458 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603458 has the following characteristics: ITEM_BARCODE = PE603458 CONTAINER_BARCODE = PE906133 NAME = Mud Log 12 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 12 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603459 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603459 has the following characteristics: $ITEM_BARCODE = PE603459$ CONTAINER_BARCODE = PE906133 NAME = Mud Log 13 of 27BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELL SUBTYPE = MUD_LOG DESCRIPTION = Mud Log 13 of 27 for Fortescue-2 (in separate pages) REMARKS = DATE_CREATED = 30/11/1978DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603460 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603460 has the following characteristics: $ITEM_BARCODE = PE603460$ CONTAINER_BARCODE = PE906133 NAME = Mud Log 14 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELL SUBTYPE = MUD_LOG DESCRIPTION = Mud Log 14 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979 $W_{NO} = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603461 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603461 has the following characteristics: ITEM_BARCODE = PE603461CONTAINER_BARCODE = PE906133 NAME = Mud Log 15 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 15 of 27 for Fortescue-2 (in separate pages) REMARKS = DATE_CREATED = 30/11/1978DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603462 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603462 has the following characteristics: ITEM_BARCODE = PE603462 CONTAINER_BARCODE = PE906133 NAME = Mud Log 16 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELL SUBTYPE = MUD_LOG DESCRIPTION = Mud Log 16 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ $DATE_RECEIVED = 26/04/1979$ $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603463 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603463 has the following characteristics: ITEM_BARCODE = PE603463 CONTAINER_BARCODE = PE906133 NAME = Mud Log 17 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 17 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ $DATE_RECEIVED = 26/04/1979$ $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED

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This is an enclosure indicator page. The enclosure PE603464 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603464 has the following characteristics: ITEM_BARCODE = PE603464 CONTAINER_BARCODE = PE906133 NAME = Mud Log 18 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 18 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603465 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603465 has the following characteristics: ITEM_BARCODE = PE603465 CONTAINER_BARCODE = PE906133 NAME = Mud Log 19 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 19 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ $DATE_RECEIVED = 26/04/1979$ $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603466 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603466 has the following characteristics: ITEM_BARCODE = PE603466 CONTAINER_BARCODE = PE906133 NAME = Mud Log 20 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5 TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 20 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ $DATE_RECEIVED = 26/04/1979$ $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603467 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603467 has the following characteristics: ITEM_BARCODE = PE603467 CONTAINER_BARCODE = PE906133 NAME = Mud Log 21 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 21 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ $DATE_RECEIVED = 26/04/1979$ $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603468 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603468 has the following characteristics: ITEM_BARCODE = PE603468 CONTAINER_BARCODE = PE906133 NAME = Mud Log 22 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELL SUBTYPE = MUD_LOG DESCRIPTION = Mud Log 22 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ $DATE_RECEIVED = 26/04/1979$ $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603469 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603469 has the following characteristics: ITEM_BARCODE = PE603469 CONTAINER_BARCODE = PE906133 NAME = Mud Log 23 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELL SUBTYPE = MUD_LOG DESCRIPTION = Mud Log 23 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979 $W_{MO} = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603470 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603470 has the following characteristics: $ITEM_BARCODE = PE603470$ CONTAINER_BARCODE = PE906133 NAME = Mud Log 24 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 24 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603471 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603471 has the following characteristics: ITEM_BARCODE = PE603471 CONTAINER_BARCODE = PE906133 NAME = Mud Log 25 of 27BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELL SUBTYPE = MUD_LOG DESCRIPTION = Mud Log 25 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED

(Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603472 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603472 has the following characteristics: ITEM_BARCODE = PE603472 CONTAINER_BARCODE = PE906133 NAME = Mud Log 26 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 26 of 27 for Fortescue-2 (in separate pages) REMARKS = $DATE_CREATED = 30/11/1978$ DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603473 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603473 has the following characteristics: ITEM_BARCODE = PE603473 CONTAINER_BARCODE = PE906133 NAME = Mud Log 27 of 27 BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = MUD_LOG DESCRIPTION = Mud Log 27 of 27 for Fortescue-2 (in separate pages) REMARKS = DATE_CREATED = 30/11/1978DATE_RECEIVED = 26/04/1979 $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE603474 is enclosed within the container PE906133 at this location in this document.

The enclosure PE603474 has the following characteristics: ITEM_BARCODE = PE603474 CONTAINER_BARCODE = PE906133 NAME = Drilling Pressure Log BASIN = GIPPSLAND PERMIT = VIC/L5TYPE = WELLSUBTYPE = WELL_LOG DESCRIPTION = Drilling Data Pressure Log including rate of penetration drilling exponent and gas units for Fortescue-2. REMARKS = $DATE_CREATED = 30/11/1978$ $DATE_RECEIVED = 26/04/1979$ $W_NO = W709$ WELL_NAME = FORTESCUE-2 CONTRACTOR = EXPLORATION LOGGING OF AUSTRALIA INC. CLIENT_OP_CO = ESSO AUSTRALIA LIMITED (Inserted by DNRE - Vic Govt Mines Dept)