



FINAL WELL REPORT

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PETROFINA EXPLORATION AUSTRALIA

ANGLER - 1

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020CT 1989

INTERPRETATIVE

ANGLER 1

VIC/P20 BASS STRAIT

FINAL WELL REPORT

FOR

PETROFINA EXPLORATION AUSTRALIA S.A.

PREPARED BY

GEOSERVICES OVERSEAS S.A.

Well : Angler # 1

Country : Australia

Angler # 1

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Well : Angler # 1

Country : Australia CONTENTS

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Well : Angler # 1

Country : Australia GENERAL WELL DATA

> Client : Petrofina Exploration Australia S.A.

Well Angler # 1

Field

VIC/P20 Block District Bass Strait Country Australia

38 deg 39' 35.3 " S Latitude : : 148 deg 26' 29.4 " E Longitude

UTM North 625,422 E UTM East 5,719,970 E

Elevation KB AMSL : 27.0 met Seawater Depth : 277.7 met Seawater Depth Proposed TD : 4000 met Actual TD : 4330 met TD Electric Logs 4337 met :

Spudded on : 24th MARCH 1989 Reached TD on : 13th MAY 1989

Rig Released on : pending logging

Well Status : plugged and abandoned

Drilling Contractors Zapata Offshore.

> Logging Geoservices

MWD Teleco.

Electric Logging : Schlumberger Cementing : Halliburton Casing Weatherford :

Mud Baroid ROV Sub-Sea Testing Flowpetrol

Catering SOS

Velocity Schlumberger Company: Petrofina Exploration Australia 1.4

Well: Angler # 1

Country: Australia INTRODUCTION

INTRODUCTION

Angler #1 was drilled as a vertical exploration well in permit VIC/P-20. The well was spudded on the 24th March 1989 in 277.7 mt of water, and reached a revised total depth of 4330 mt on the 13th May 1989 at 10.20 am.

The primary objective the Maastrichtian Selene Sandstone was penetrated at 3247.0 mt, 153 mt high of prognosis at 3400 mt. This sandstone proved water wet, and lacked the expected shale seal.

The secondary target the Campanian Sandstones of the Latrobe Group proved gas prone with intermittant hydrocarbon shows recorded from 3815 mt to a depth of 4330 mt (TD). At 3830 mt an increase in resistivity from the MWD tool indicated the presence of hydrocarbons. Due to the tightness and pyritic nature of this sandstone a drill break didn't compliment this increase in resistivity, however once bottoms up was circulated a total gas of 0.6% with trace amounts of C2 and C3 were recorded. Previous to this gas show no gas had been recorded since penetrating the thin coal seams overlying topmost Selene Sandstone at 3200 mt. The fluorescence from this resistivity peak was described as having a moderately bright direct fluorescence, with a fast streaming bright yellow cut, an abundant brown oil stain was also present. On the basis of these indicators a 9.0 mt core was taken from 3833.0 mt to 3842.0 mt with 99% recovery (Refer to the Petrofina Core description for a hydrocarbon evaluation).

Drilling continued from 3842.0 mt through a predominately siltstone lithology with a C1 background of 0.6%. At 4205 mt an increase to 25-30 m/hr in drill rate revealed the presence of a thin (20-25met) Lower Campanian Sandstone. This sandstone proved gas prone with a total gas of 9.0%, which included gas heavies iC4 & nC4. The associated fluorescence was described as having a pale yellow direct fluorescence, with a slow weak green-yellow cut, no stain or residual ring was observed. A RFT over this interval found a gas/condensate rich sandstone (Refer to RFT summary for further details).

Well : Angler # 1

Country : Australia TIME BREAKDOWN

TIME BREAKDOWN

Activity	:	Hours	%	Total Days : 55 24/03/89 to 16/05/89
Rig up/tear down	:	2.0	0.15	
Drilling	:	444.75	33.7	
Reaming	:	97.5	7.39	·
Circulating	:	43.50	3.3	
Tripping	. :	250.75	19.0	
Coring	:	8.5	0.64	
Rig Repair	:	62.25	4.71	
Nipple up/test BO	P:	166.50	12.5	
Deviation survey	:	7.00	0.53	
Cut and slip	:	7.25	0.54	
Casing/cementing	:	78.25	5.8	
Electric logs	:	83.00	6.2	
Fishing	:	17.75	1.34	
Other	:	56.0	4.3	, , ,
Total	:	1320	100.0	

Well : Angler # 1

Country: Australia WELL DIARY

WELL DIARY

DAY 1 24th MARCH 1989

00:00hrs depth: 0 met

Pick up 26" bit and 36" HO, make up BHA, and RIH to 20m off mud line. Wait on satellite position fix, then RIH and tag mud line @ 303.09m. Spud in @ 10:27 hrs and drill 36" hole to 320m, pumping hi-vis pill each connection. Run survey, pull up to check for fill (7m of fill). Wash to bottom and spot hole with 500 bbls hi-vis mud. POOH. Run in w/cement stinger and 30" casing running tool. Latch casing and fill with seawater. Continue RIH, stab hole and space out. Circulate 300 bbls seawater.

DAY 2 25th MARCH 1989 00:00hrs depth: 364 met

Test cement line to 2000 psi. ROV observe slope indicators to be 1 deg. mix and pump cement, displace with seawater. Wait on cement, observe mud line with camera. Break out circ hose, POOH to top of 30" casing. Stab mule shoe in PGB into 36"/30" annulus with ROV guidance. R/U cement hose, break circulation and RIH. Tag cement 5m in. Test cement line, mix and pump cement for top job, and displace. POOH. M/U 26" bit, RIH, stab casing. Tag cement @ 351m. Drill out cement, shoe and rat hole from 351m to 363m. Drill 26" hole to 365m, spot 50 bbls hi-vis. POOH. M/U 8 1/2" bit and RIH, stab casing, and continue to RIH. Drill 8 1/2" pilot 365-408m, observe returns with ROV.

DAY 3 26th MARCH 1989 00:00 hrs depth: 408 met

Continue to drill 8 1/2" hole from 408 to 455m, run wireline survey at 450m--1/4 deg. Drill ahead to 539m, run survey--1/4 deg. Drill ahead to 585m, pump 30 bbls hi vis sweep. Run survey and rack Kelly. POOH, recover survey--1/4 deg. Break out 8 1/2" bit and bit sub. P/U 20" hanger, M/U to running tool and rack in derrick. Break out 20" bit and M/U 26" HO. M/U 12 1/4" bit and 26" HO, stab into 30" casing and continue RIH. Drill 26" hole from 452 to 537m. Run survey at 531m--3/4 deg. Drill 26" hole from 537m to 578m.

Well : Angler # 1

Country : Australia WELL DIARY

DAY 4 27th MARCH 1989 00.00hrs depth: 578.0 met

Continue to drill 26" hole to 613m. Pump 50 bbls hi vis sweep and spot 500 bbls of 1.2 sg. hi vis. Drop survey, rack Kelly. POOH to wellhead, L/D string. Recover survey--misrun. Flush out 30" housing, POOH. M/U DP stinger under 30: running tool and RIH. Unable to stab in 30" running tool, POOH. M/U 26" stab and 30" running tool. RIH, stab casing engage tool. ROV retrieve slope indicator. Circulate with charge pump and check for returns to surface--none. Take 100K overpull, observe bulls eye, no movement. Disengage running tool and POOH. L/D tool, pick up 20" wellhead and install 1 jnt DP below running tool. M/U and run stinger in 20" casing, fill each jnt with seawater. M/U and run stinger, M/U 20" hanger. Stab 20" casing into 30" using ROV. P/U Kelly and fill casing with seawater, install plug in running tool. Run 20" casing on HWDP, fill each stand with seawater.

DAY 5 28th MARCH 1989 00.00hrs depth: 613.0 met

Continue running 20" casing. Land 20" casing and take 150K overpull. Slope indicator at 1 1/2". Circulate, hook up Howco and pressure test surface lines to 5000 psi. Cement 20" casing with 508 bbls cement @ 1.9 sg. Observe returns with ROV. Displace with 417 bbls seawater, bleed off OK. Back out running tool and POOH. Strap out of hole, jet well head area. R/U to run BOP's, attempt to test shear rams-negative. Open bonnets to check shear rams. Remove shear rams, place 5" shear rams and C/O lower test stump jnt. Fill BOP with seawater for pressure test.

DAY 6 29th MARCH 1989 00.00hrs depth: 613.0 met

L/D riser, M/U 17 1/2" bit, stab, and MWD tool. Test BOP's to 15klbs. STI failure. R/U and move BOP's and install joint riser. Remove LMRP, change out seals. Pressure test STI's after relatching LMRP. Choke STI failed. Remove LMRP and check seals. Relatch LMRP, remove joint riser. Fill BOP with water, test STI connector—test negative. M/U joint riser to LMRP and unlatch. Open shear ram bonnets and remove 5" pipe rams to install shear rams. Work on STI connector, relatch LMRP and remove. Fill BOP with water and test STI connectors—good. M/U TIW valve on DP stand to test annulus.

Well : Angler # 1

Country : Australia WELL DIARY

DAY 7 30th MARCH 1989 00.00hrs Depth: 613.0 met

Attempt to test shear ram--negative. Open bonnet and inspect seal-no visible problem. Close bonnet with 4 bolt and attempt lower pressure test. Leave at the center of rams, open bonnet, replace lateral T-seal and close bonnet. Pressure test to 15 klbs--good. Install DP and close upper annular. Pressure to 3500 to test riser connector--good. Remove drill pipe and move BOP's. M/U double riser, move BOP's to center and hook up guidelines. Grease connector, P/U BOP with 560 klbs overpull. C/O ring gasket, install beacon. Run riser pressure test. Test kill and choke lines to 3000 psi/5 min.

DAY 8 31st MARCH 1989 00.00hrs depth: 613.0 met

Continue running riser, test every 2nd jnt, choke and kill line to 7500 psi/5 min. P/U slip jnt and 50° landing jnt. P/O landing jnt and slip jnt. Hook up choke, kill and conduit lines. Latch on tensioner and land BOP's. Take 80K overpull. Stroke out inner barrel and L/O 50° landing jnt. Nipple up choke and kill lines. Pump 5 bbls down kill with Howco to maintain circulation. Test shear rams @ 1500 psi/15 min.--good. P/U diverter and test with 10K overpull. R/D BOP running gear. RIH and test plug @ 20K. Test BOP's to Petrofina standards--good. Retrieve test plug. Pressure test surface equipment.

DAY 9 1st APRIL 1989 00.00hrs Depth: 613.0 met

Continue testing surface equipment. RIH and set bore protector. M/U MWD and test. Continue to M/O BHA and RIH, tag cement @ 573m. P/U kelly and hold kill drill. Test diverter system. Drill out cement and shoe, clean out rathole from 573-607m. Ream to 613m. Drill from 613 to 618m. Pump 50 bbls hi-vis pill, perform formation leak-off test. Drill ahead--controlled drilling @ 3 singles per hour.

DAY 10 2nd APRIL 1989 00.00hrs Depth: 789.0 met

Continue drilling 17 1/2" hole from 789-1050m. Rotary torque 4500-5000 ft-lbs. Maximum overpull on connection-40Klbs. Drill ahead to TD @ 1165m. Spot 50 bbls hi-vis mud on bottom. POOH with wet pipe. Drag 60K. Slip and cut drilling line, and continue POOH.

Well : Angler # 1

WELL DIARY

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DAY 11

3rd APRIL 1989

00.00hrs depth: 1165.0 me

Continue POOH. Remove insert packer, threads appeared to be galled between NMDC and MWD tool. R/U Schlumberger, run DIT, MSFL and gamma-ray logs (2 runs) from 03:15-08:30 hrs. R/D Schlumberger. Breakout and L/D NMDC and MWD tool--threads galled. M/U 13 3/8" casing hanger to universal with seal assembly. RIH and tag bottom--no fill. Circulate and spot 50 bbls hi-vis pill and pump slug. POOH. RIH and retrieve wear bushing. POOH, R/U ref. line. R/U and run 13 3/8" casing.

DAY 12

4th APRIL 1989

00.00hrs depth: 1165.0 met

Continue running 13 3/8" casing, land same. R/U cement line, circulate. Test cement lines to 5000 psi, and pump cement. M/U pack off, test against middle pipe ram to 1500 psi/15 mins. L/D cement head, P/U Kelly, jet wellhead. POOH, L/D casing running tool. Set BOP test tool. Pressure test on pipe rams--fail safe values to 250-7000 psi. Annulus 1 and inner choke tested to 250-5000 psi. Annulus 2, upper outer choke to 250-5000 psi. Choke and kill manifold to 250-7000 psi. Function BOP's on yellow pod. POOH 3 stds, P/U Kelly, circulate riser and flush BOP. POOH with BOP test plug. M/U and RIH with jet sub, flush well head and BOP's. POOH and L/D jet sub, close shear ram. Pressure test casing to 1750 psi. M/U and RIH with wellhead wear bushing and set. POOH with bushing running tool. M/U 2 TIW valves and pressure test surface equipment to 250-5000psi.

DAY 13

5th APRIL 1989

00:00hrs depth: 1170.0 met

 $\ensuremath{\text{L/D}}$ 9.5" drill collars and crossovers. Attempt to run flex joint wear bushing--unable to run. P/U 12.25" bit, junk sub, and bit sub and RIH, tagging cement @1117m. Circulate with slow pump rates w 1.17 sg. mud. Drill cement and float collar. Continue drilling on float collar, shoe, and cement to 1165m. Drill 12.25" rathole from 1165 to 1170m. Circulate bottoms up. Junk sub had 7 lbs junk recovered. Hang off drill string on #3 ram-HOWCO, perform leak-off test. Mud wt. equivalent--1.80 sg. Slug pipe, POOH. R/U riser running equipment, close shear ram. Pull LMRP to check choke line leak. Unlatch with ROV observation.

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DAY 14

6th April 1989

00.00hrs depth: 1170.0 met

Pull lower marine riser package--static weight 270,000 lbs. Land on test stump. Replace choke line, flex joint gooseneck. Make up double joint riser to LMRP. Run riser. Check choke-kill and conduit couplings on all riser joints. Pick up and make up slip joint and diverter package.

DAY 15

7th April 1989

00.00hrs depth: 1170.0 met

Run LMRP. R/U lines to slip joint and land LMRP, and take 50Klbs overpull, land diverter. R/D riser equipment. Test choke line to 2000psi. Attempt to test kill-line. Test unsuccessful due to leak in ST 1 connector with ROV. Open choke values and observe zero well pressure. M/U running String, packer and storm valve-set at 366m. POOH w/-RTS. R/U riser equipment. L/O diverter, P/U and M/U riser joint to slip joint. Unlatch BOP and P/U- rig down kill and choke lines. Pull BOPs and L/D slip joint and 13 joints, rack double in derrick. Move BOPs carrier to rotary, sitting stack on stump. Unlatch LMRP, break-out STI spool kill side.

DAY 16

8th April 1989

00:00hrs depth: 1170.0 met

Continue repairs on BOPs.Pull double of riser and stand back in derrick. Fill BOP with water and test choke, kill lines and connectors to 15,000psi-test successful. M/U TIW valve on stands of drill pipe and install in BOP. L/O a stand of drill pipe and TIW valve. Test shear rams to 40,000 psi and finally at 7000psi. Function test BOPs. M/U double joint riser to BOPs. P/U BOPs and move carrier to port-install beacon, and change out conduit hose. Run BOPs, pressure test choke and kill lines. L/D 1 joint of marine riser.

DAY 17

9th April 1989

00.00hrs depth: 1170.0 met

Continue running riser, pressure testing choke, kill and conduit lines every 3rd joint. L/D 1 joint of marine riser w/-damaged pin on choke line. P/U and M/U slip joint and single of riser, connect kill, choke and conduit lines. P/U riser tensioner ring. Lower WT on riser tensioners. Lower BOP and set on wellhead latch-test w/ 50,000Klbs o/p. P/U and M/U diverter. Test locking dogs. Install hydraulic diverter packer lines.Rig down riser running equipment.Rig-up to RIH to retrieve wellhead wear bushing.

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DAY 18

10th April 1989

00.00hrs depth: 1341.0 met

P/U positive displacement motor, break connection and check assembly. L/D PDM because of incomplete assembly. P/U another PDM, install kelly and lower by-pass ports below table to measure pressures. Install 12.25" clamp on stabiliser at bottom of stator housing-torque to 25,000ftlbs. P/U MWD and M/U to BHA. P/U kelly and measure pressures. P/U and install Hughes PDC bit. RIH to 1159m-wash to TD at 1170m. Continue drilling 12.25" from 1170m to 1341m. Pump 50bbls hi-vis at 1315m.

DAY 19

11th April 1989

00.00hrs depth:1352.0met

Continue drilling 12.25" hole from 1341m to 1352m. Observe a 1200psi drop in stand pipe pressure. POOH-drillstring twisted off @ mud motor below dump connection. Prepare fish assembly. Cut and slip drill line. RIH with overshot. P/U kelly, break circulation. Tag fish. Commence fishing. Engage fish, and POOH hole with same. R/D bit, release fish from overshot. P/U mud motor and M/U to Kelly-test same. M/U mud motor to MWD and surface test MWD-test unsuccessful. Pull up test string, observe that mud motor had twisted off. Prepare to M/U Fishing tool.

DAY 20

12th April 1989

00.00hrs depth:1352.0met

RIH with overshot fishing assembly, tag fish @ 1344m. Break circulation and wash over fish, engage same. POOH-- fish not recovered. B/U overshot, wait for arrival of 11-3/4" overshot on rig. M/U new overshot assembly, dress with 8-3/8" basket grapple and mill control packer. RIH to top of fish and engage. Pull to 50klbs overpull. POOH. Fish successfully recovered. M/U bit and MWD tool--negative. L/D MWD tool. M/U BHA and RIH. Break circulation at shoe; wash to bottom. Drill 12.25" hole from 1352 to 1386m.

DAY 21

13th April 1989

00.00hrs depth:1386.0met

Drill 12.25" hole from 1386m to 1435m. Circulate, run survey-1/2 deg. Continue to drill 12-1/4" hole from 1435 to 1527m. Perform slow circulation rates. Drill from 1527 to 1537m. Circulate; run survey--.5 deg. Continue drilling 12.25" hole from 1537-1641m. Circulate, run survey--.5 deg. Continue to drill 12.25" hole from 1641 to 1653m.

DAY 22

14th April 1989

00.00hrs depth:1653.0met

Drill 12.25" hole from 1653m-1740m. Circulate, run survey. Slug pipe and POOH. L/D string. Surface test MWD and RIH with Bit #7.

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DAY 23

15th April 1989

00.00hrs depth 1740 met

RIH with new 5" drill pipe, clean and inspect. Walk in with chain tong. Strap 16 stds. Continue RIH to 1728m. Teleco survey check. Drill 12.25" hole from 1740m-1742m. Unable to make hole. Encountered 400 psi pressure loss while pumping @ 180 strokes per minute. Slug pipe and POOH. M/U PDM on Kelly and test. M/U bit, roller reamer and MWD and test. M/U BHA and RIH. M/U Kelly to jars, teat same. Continue RIH to shoe. Slip and cut drill line. RIH to 1735m. P/U Kelly and wash to bottom. Drill 12.25" hole from 1742 to 1756m.

DAY 24

16th April 1989

00.00hrs Depth:1889.0 met

Drill 12.25" hole from 1756.0m to 1889.0m. Encounter 400psi increase at 1779.0m-suspect blocked nozzle. Drill ahead with a reduced flow rate. Perform slow circulation rates at 1756.0m and 1840.0m.

DAY 25

17th April 1989

00.00hrs Depth:1992.0 met

Continue drilling 12.25" hole from 1889m to 1992m. Displace hole with gel/polymer mud at 1992.0m. Perform slow circulation rates at 1992m.

DAY 26

18th April 1989

00.00hrs Depth:1992.0 met

Circulate prior to POOH. Drop survey ,pump slug and begin POOH. RIH and retrieve flex joint and wellhead wear bushings. M/U test plug and RIH to test BOPs. POOH with test tool. Run wellhead/flex joint wear bushings. Test surface equipment. P/U and M/U BHA & RIH, breaking circulation at shoe.

DAY 27

19th April 1989

00.00hrs Depth:1992.0 met

Continue to RIH, fill pipe 10 stds off bottom, cont. to RIH Wash/ream from 1988m to 1922m and work junk basket. Drill 12.125" hole from 1992m to 2097m. Circulate BU. Drop totco and pump slug. POOH. P/U PDM, P/U kelly and test.

DAY 28

20th April 1989

00.00hrs Depth:2097.0 met

Test Navdril PDM. P/U TELECO, shock sub s/stab M/U bit. Fill pipe RIH to 2088m. Break circ wash 2088m-2206m. Drill from 2092m to 2535m.

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DAY 29

21st April 1989

00.00hrs Depth:2535.0 met

Drill 2535m to 2767m circulate B/U. Drill 2767m to 2918m. Circulate hole clean. POOH.

DAY 30

22nd April 1989

00.00hrs Depth:2918 met

Slip and cut the drill line at the shoe. Cont. to POOH. R/U Schlumberger. M/U Son, MSFL, DLT, GAMMA. Stuck at 2330m POOH. L/D and R/D Schlumberger. L/O Monel s/stab MWD, DBL PIN SUB, SHOCK SUB, NAVIDRILL. M/U bit R/Reamer, s/stab to BHA and RIH. Install insert packer. Break circ at shoe tag @ 2096m. Wash and ream 2096m-2918m. Pump 40bbl Hi-Vis and sweep. Inc MW 1.16 to 1.20 sg. Pump 40 bbl Hi-Vis pill. Sweep around clean up hole. pump slug. POOH.

DAY 31

23rd April 1989

00.00hrs Depth:2918 met

P/U kelly and flush wear bushings BOP. Cont. to POOH. R/u Schlumberger. Make up tools for Run #1. Make up tools for Run #2. P/U 9 5/8" csg hanger. Make up x-over/ring tool to STD of HWDP and stand back in derrick. RIH and retrieve the wear bushings. Establish reference mark on line, POOH. Pick up 9 5/5" CSG hanger and readjust measurement on pack off. Rig up and run 9 5/8" casing.

DAY 32

24th April 1989

00.00hrs depth: 2918 met

Cont. to run 9 5/8" CSG. Rig down 9 5/8" equipment. M/U hanger and RIH w/ HWDP. Land CSG at 07:20 hrs. M/U CMT hose. Circ. hole and work CSG. Test HOWCO lines to 400 psi. CMT casing. Drop dart and displace with 615 bbl mud. Bump plug with 3000 psi, hold 10 mins. Check for back flow, disconnect hose and back out R/Tool. Pressure test pack off to 4000 psi. Circ to flush well head - break out circ hose. Pull out of hole lay out RNG tool. Make up test plug, RIH and test BOP's. Test negative trace to surface leak. Beak CMT heads and POOH with test plug. Lay out 5" drill pipe.

DAY 33

25th April 1989

00.00hrs depth: 2918 met

Cont. to lay our excess DP and 1 std 8" DC. Make up test plug and RIH. Test BOP'S and RIH. Test BOP'S, Rams #2,3,4 to 250 psi low 7000 psi high. POOH with the test plug. RIH and set well head and flex joint bushings and POOH. RIH with 12 1/4" BHA and lay out. P/U and M/U new BHA. P/U kelly and test MWD pressure to high , pull back MWD and break off bit and replace nozzles. Cont to RIH and P/U BHA and 60 jnts "S" grade new DP. _____

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WELL DIARY

DAY 34

26th April 1989

00.00hrs depth: 2918 met

Continue to pick up and make up new drill pipe. Tag CMT @ 2822m. Drill CMT from 2822m to 2830m. 2830m to 2860m no weight no pumps, take weight at 2860m, Drill CMT and Float Collar from 2860m to 2918m. Drill 8 1/2" hole from 2918m to 2923m. Circ and condition mud, flush riser. Pull to shoe and perform LOT. LOT against No. # 3 Ram to 1.60 sg. RIH and drill from 2923m to 2985m. Displace hole with 1.10 sg mud. Stop drilling at 2983m and circulate for 15 mins. Flow check and POOH.

DAY 35

27th APRIL 1989

00.00hrs depth: 2985.0 met

Continue to POOH. M/U Diamond Bit (Christensen R437) and RIH to 57m. Test TELECO Tool. Cont. to RIH to 9 5/8" Shoe. Slip and cut drilling line. Cont. to RIH tag bottom at 2967m. Wash from 2967 to 2985m. Drill 8 1/2" hole from 2985m-2998m. Bit stalled out. Max o/pull 80 Klbs. Work free. Mix and pump 50 bbl detergent pill. Circ B/U and work pipe. POOH to shoe. Break circ. Work MWD. RIH to 2967.70 m. Ream and wash from 2967 to 2998m. Drill from 2998 to 3119m.

DAY 36

28th APRIL 1989

00.00hrs depth: 3119.0 met

Drill 8 1/2" hole from 3119m to 3227m. Circ and rack back kelly. Pull 10 std Wiper trip to 2930m. Max O/pull 20 Klbs. RIH to 3227m. Drill 8 1/2" hole from 3227m to 3354m. Pump 100 bbl torque reducer at 3340m.

DAY 37

29th APRIL 1989

1989 00.00hrs depth: 2918.0 met

Continue to drill 8.5" hole from 3354 to 3507m.

DAY 38

30th APRIL 1989

00.00hrs depth: 3507.0 met

Circulate and pump slug. POOH and lay out 60 joints. M/U bit and roller reamer. RIH to 56m, P/U Kelly and test Teleco tool. Rack back Kelly. Continue RIH. P/U 75 jnts of 'E' grade drill pipe and continue RIH to 3491m. Wash from 3491m to 3507m. Drill from 3507m to 3590m.

DAY 39

1st MAY 1989

00.00hrs depth: 3590.0 met

Drill 8.5" hole from 3590m to 3686m. Maximum torque--12,000 ft/lbs .Drill 8.5" hole from 3686m-3754m.

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DAY 40

2nd MAY 1989

00.00hrs depth: 3756.0 met

Continue drilling 8.5" hole from 3754 to 3833m. Check for flow. Circulate up sample, check for flow. Slug pipe and POOH. Check for flow at Continue POOH--105 stands. Slip and cut drill line. Resume POOH. Break out and lay down bit #10. P/U and M/U core barrel. L/D inner barrel and M/U fiberglass inner barrel. Check service connection and M/U core head.(DBS CT303). Continue RIH with BHA.

DAY 41

3rd MAY 1989

00.00hrs depth: 3833.0 met

Continue to RIH with the coring assembly to 3743. Bit sticks at 3743m worked free and run to 3773m. P/U kelly ream and wash to 3788m. POOH to 3740m taking 40 Klbs overpull. Pump slug, rack back kelly, POOH, B/O Core Bit. M/U wear bushings, retrieve tool, RIH retrieve flex joint wear bushings, POOH and disengage wear bushings. Press test choke manifold 250-700 on LP valves, 250-2500 on buffer tank valves. Test choke and kill lines to inner fail-safe valves on BOP. RIH retrieve wellhead wear bushing, R.B the same. M/U and RIH set BOP test plug. Press test BOP rams & all failsafe valves to 250 & 7000 psi. Annular $\sharp 1$ to 250 & 2500 psi. Annular \sharp 2 250-3500 psi.C/O well head wear bushings. Function test yellow pod. POOH L/D test plug. Rig up and test surface equipment. POOH wear bushing running tool. M/U wear bushings and set. Make up and RIH 8.5" Bit #12 & BHA P/U roller reamer ,2 stabilisers and new jars.

DAY 42

4th MAY 1989

00.00hrs depth: 3833.0 met

Continue to M/U BHA and RIH, take weight at 3274m. Ream and wash from 3255-3326m. Continue RIH to 3425, take weight--pipe stuck. P/U kelly, pump free. Pump back to 3311m, L/D 12 singles, RIH to 3440m. Ream and wash form 3472-3552m. Attempt to RIH--negative. POOH, L/D 27 joints. RIH with 9 stands. Continue to ream and wash from 3552-3595m--tight hole. Work free w/- 120Klbs overpull, continue to ream to 3645.

DAY 43

5th MAY 1989

00.00hrs depth: 3833.0 met

Ream from 3645-3713m--tight hole, jarring required each single. Maximum overpull up-480K, down-320K. Ream and wash from 3713-3717m. Slug pipe and POOH. Check for flow at shoe. B/O bit #12, junk sub, roller reamers and stabilizers. M/O and RIH with bit #13, junk sub, and near bit L/D stabilizer, and RIH 45 stands DP. Slip and cut drill stabilizers. line. Continue RIH with BHA to ream.

Well : Angler # 1

DAY 44 6th MAY 1989 00.00hrs depth: 3833.0 met

RIH with 8.5" BHA to 3700m. P/U kelly, wash and ream from 3700 to 3790m. Pickup and pull free. Maximum overpull--440K/up, 330K/down. Continue to ream and wash from 3790-3833m. Work junk sub, circulate and condition, slug pipe. POOH to 3177m to TD, maximum overpull 20K. RIH from 3177m to TD @ 3833m--no fill. Circulate and condition mud, work pipe while circulating. Slug pipe and POOH.

DAY 45 7th MAY 1989 00.00hrs depth: 3833.0 met

POOH, strap drill pipe. Break down BHA, 60 ft core barrel and M/U 30 ft barrel. RIH with coring assembly. Tag TD @ 3833m, M/U 2 x pup joints. Drop ball and check pressure a 60 strokes. Perform slow pump rates. Cut core #1 from 3833-3842m. Break core. Circulate prior to POOH. Flow check at shoe.

DAY 46 8th MAY 1989 00.00hrs depth: 3842.0 met

Continue to POOH with coring assembly. Recover core-99%-break out and lay down barrel. M/U Stratapax bit, MWD and BHA and RIH. Circulate test mud. Continue RIH, take wt @ 3796m. Ream and wash from 3796 to 3842m. Drill 8.5" hole from 3842m to 3944m.

DAY 47 9TH MAY 1989 00.00hrs depth: 3944.0 met

Drill 8.5" hole from 3944-4039m. Rotary torque--4,000 to 12,000 ft/lbs; weight up 405K, weight down 375K. Circulate hole, pump slug. Wiper trip back to 3775m. L/D 6 singles, RIH to 3825m. Ream from 3825 to 3842m. Teleco log hole. RIH to 4039m. Drill 4039m to 4058m. Rotary torque 9,000 to 10,000 ft/lbs.

DAY 48 10th MAY 1989 00.00hrs depth: 4058.0 met

Continue drilling to 4079m. Encountered high torque, unable to make sufficient penetration rate. Slug pipe and POOH. Slip and cut drill line. Continue POOH, B/O roller reamer and bit. RIH with wear bushing running tool to retrieve flex joint. String weight up--410Klbs; down 390klbs. Torque 6,000 to 10,000 ft/lbs. POOH with flex jnt wear bushing. M/U test plug with 2 stands of HWDP below and RIH. Test BOP's. #1 annular and #2 annular to 250-35,000 psi. Rams to 250-7000 psi. POOH with test plug, L/D same. RIH with flex joint wear bushing and POOH with running tool, L/O running tool. M/U bit and roller reamer to BHA and RIH. P/U kelly, test Teleco MWD tool--OK. Continue M/U BHA and RIH.

Well : Angler # 1

Country : Australia

WELL DIARY

DAY 49

11th MAY 1989

00.00hrs depth: 4079.0 met

Continue to RIH to 4043m. Ream/wash from 4043m to 4079m. Break in 8.5" bit and drill from 4079m to 4191m. At 4182m take 50 klbs overpull on connection. Circulate and work pipe. POOH 10 stands on wiper trip back to 3908m. Run back into hole to 4191m; drill to 4234m. Maximum overpull on connection was 15Klbs. Unable to make further depth, POOH. Check flow at shoe--negative. B/O bit #15. L/O Teleco tool. M/U new Teleco tool; walk in new threads. M/U 8.5" bit #16. P/U Kelly and function test MWD.

DAY 50

12th MAY 1989

00.00hrs depth: 4302.0 met

Make up BHA and RIH with Bit #16. Drill new formation from 4079m to 4302m. Maximum drag on connections was 15 klbs. Rotary torque 5500 to 6500 ft/lbs.

DAY 51

13th MAY 1989

00.00hrs depth: 4330.0 met

Continue to drill 8.5" hole from 4302m to 4330m. Circulate bottoms up, work pipe, wash and circulate. Pull wiper trip back to shoe. Maximum drag on connections--15 klbs. Slip and cut drill line. RIH to 4330m--no fill. Circulate, condition mud, slug pipe. POOH, strap out. Maximum drag--15klbs.

DAY 52

14th MAY 1989

00.00hrs depth: 4330.0 met

POOH, strap pipe. B/O bit #16. R/U Schlumberger and RIH A 4:08 hrs with log run #1.--DLL,MSFL,BHC,GR. Out of hole @ 05:40. Schlumberger check and service tools. Reterminate wireline log #1 in hole @ 09:30 hrs. Run log #2, LDT-CNT-GR, out of hole at 23.10hrs.

DAY 53

15th May 1989

00.00hrs depth: 4330.0 met

Lay down log #2 tools.P/u log #3 tools-RFT. Run and recover chamber samples. Rig down Schlumberger. M/U bit #16 and RIH to circulate and condition mud.

DAY 54

16th MAY 1989

00.00hrs depth: 4330.0 met

P/U Kelly break circulation. Tag bottom @ 4330met-no fill. and condition hole. Slug pipe.POOH for log #4.Rig Schlumberger.P/U & M/U FMS-GR. Run log #4.

Well : ANGLER1 #1

Constant Annaly I is

Country : Australia PHASE SUMMARIES

36" PHASE REPORT"

From: 303.9 met to: 363.0 met From: 10:27 to 18:30 on 24th March 1989

SUMMARY:

Angler \sharp 1 was spudded at 10:27 hrs on 24/03/89 with Bit \sharp 1, a 26" REED Y11 with 4 x 11 jets, and a 36" hole opener with 3 x 9 jets. The 36" hole was drilled from 304m to 363m in 8.0 hours with seawater and hi-vis pills. On reaching T.D., a hi-vis sweep was pumped to clean the hole, and the hole was spotted with 500 bbls of hi-vis mud prior to pulling out of hole to run 30" casing.

WOB/RPM/FLOW RATE PRACTICES:

WOB was maintained at 0-3 Klbs and RPM at 35 in order to ensure a vertical and gauge hole was drilled. An average ROP of 45.1 m/hr was obtained with the above parameters. Flow rates of 250-520 gpm were used to clean the hole of cuttings and maintain penetration.

Seawater with hi-vis pills was used to drill the 36" hole and clean the hole of cuttings. Bit hydraulic optimization was of little importance in the 36" hole where the main priority was to clean the hole of cuttings and drill the hole as quickly as possible.

CASING AND CEMENTING:

Five joints of 30" Vetco B casing (total length 57.5m) were run in the hole with the casing shoe set at 358m. Cementing was carried out as follows: 1260 sacks of 'G' grade cement was mixed with 150 bbls of drillwater and 1% CaCl2 to give 258 bbls of slurry. This was pumped and displaced with 19 bbls of sea water. A top up job followed with 300 sacks of class 'G' cement mixed with 36 bbls of 1% CaCl2 mix water to make 62 bbls of slurry which was pumped and displaced by 10 bbls of sea water.

Well : Angler # 1

Country: AUSTRALIA PHASE SUMMARIES

26" PHASE REPORT

From: 363.0 met

To: 613.0 met

From: 25 /03/89

To: 27/03/89

SUMMARY:

Bit 1RR, a REED Y11 with 3 x 8 jets on a 26" hole opener was run in the hole and tagged cement at 351m. Cement, shoe and rat hole was drilled out from 363m to 365m, in 1/2 hour. The hole was spotted with 50 bbl hi-vis mud and Bit 1RR was pulled out of the hole. Bit 2, an 8-1/2" REED HP11J with open jets, was run into the hole to drill an 8-1/2" pilot hole before proceeding further with the 26" bit. The smaller hole was drilled as a precaution in the event that possible shallow gas zones were encountered in this interval. The 8-1/2" hole was drilled from 365m to 585m in 10 hours and a 30 bbl hi-vis pill was used to clear cuttings from the hole before pulling out with the bit. No indications of gas were encountered while drilling the pilot hole. Bit 3, a 12-1/4" REED HP11J with 3 x 12 jets and a 26" hole opener was run into the hole, and a 26" hole was drilled from 365m to 613m in 3-1/2 hrs. A 50 bbl hi-vis sweep was pumped to clean the hole and the hole was spotted with 500 bbls of 1.2 s.g. hi-vis mud before pulling out of the hole.

WOB/RPM/FLOW RATE PRACTICES:

WOB was maintained between 0-2Klbs and RPM at 120 while drilling the 8.5" pilot hole, with a flow rate of 500 gpm. Wireline surveys were run to assure that the hole did not deviate. The 26" hole was then opened with WOB ranging between 0 and 10klbs, RPM between 60 and 85, and with a flow rate of 550 gpm to effectively clean the hole of cuttings. Wireline surveys were run to assure a straight hole was drilled.

CASING AND CEMENTING:

Twenty-five joints of Vetco X-56 R145 94 ppf 20" casing were run in the hole with the shoe set at 603.9 m. The casing was successfully stabbed into the 30" casing and landed as per program. The casing was cemented with 508 bbl of cement using 2500 sacks of class 'G' cement to give a slurry of 1.90 s.g.. Returns were observed with the ROV during cementing. The cement was then displaced with 47 bbl of seawater.

Well : Angler # 1

Country: Australia PHASE SUMMARIES

17 1/2" PHASE REPORT

From: 613 m to: 1165 m From: 01/04/89 to: 02/04/89

SUMMARY:

The 17.5" phase of Angler # 1 was drilled in 29.5 hrs using one bit. Bit # 4, a HTC CX34 with 4 x 14 jets, drilled out cement, casing shoe, rat hole and new formation from 613m to 1165m, drilling ahead with seawater and 50 bbl hi-vis pills pumped as required. Teleco telemetric surveys were taken every three stands at the top of the section and once every 5 stands toward the base. A 50 bbl hi-vis sweep was pumped to clean the hole and the hole was spotted with 50 bbls of hi-vis mud before pulling out of the hole.

The casing was landed and cement pumped as per program. No problems were encountered during the casing or cementing jobs. All surface equipment was tested satisfactorily to 5000psi.

WOB/RPM/FLOW RATE PRACTICES:

The drilling rate was controlled at an average rate of three singles per hour throughout the 17.5" phase but varied from 10-40 m/hr, generally around 30 m/hr. RPM averaged 95 and WOB ranged from 0 - 15 Klbs. Flow rates of between 800-890 gpm were maintained in this section of hole.

HYDRAULICS

Hydraulic optimization was not an important factor, cleaning the hole of cuttings and maintaining circulation was most important. Flow rates of 800 -890 gpm along with hi-vis sweeps was enough to clean the hole of cuttings. Seawater was used as the drilling fluid in order to keep mud weight to a minimum and in balance with formation pressure. Bit #4, a HTC CX34 with 4 x 14, was the only bit used to drill the 17.5" hole.

CEMENT AND CASING

Seventy four joints of N80 68 lb/ft BUTT 13 3/8" casing was run to a depth of 1151.47m. This was then was cemented with a lead of 442.36 bbl, made up of 433.7 bbl of sea water 1149 sacs of class 'G' cement and 0.43 gps of econolite to give a slurry of 12.5 ppg. This was followed by a tail of 102.4 bbl slurry made up from 500 sacs class 'G' cement and 60 bbl seawater to give a weight of 15.8 ppg.

The volumes of cement were calculated to give a 60% excess and the cement was then displaced with 422 bbl of sea water.

Well : Angler # 1

PHASE SUMMARIES Country : Australia

12 1/4" PHASE REPORT

to: 2918m From : 1165m

to: 21- 04- 89 From: 10 - 04 - 89

PHASE INTRODUCTION

The 12 1/4" drilling phase of Angler # 1 was completed over seven bit runs using four Reed insert bits, and a Hughes PDC bit(HTC B9M+). The PDC bit was re-run on 3 occasions due to continuing problems with Drillex PDM motors.

Phase Statistics

- 13 3/8" Casing Shoe set at 1151.43m.

Depth Range: 1165m - 2918m.

- Phase Run: 1753.0m.

- Phase Rotary Hours:115.6hrs. - Phase Average ROP:15.16m/hr.

Phase Summary

Bit #3RR;

Type: Reed HP11J.

Nozzles:3 x 15. In:1165m.

Out:1170m.

Rot hrs:1.0hrs.

ROP:5m/hr. Wear: 2/2/I. BHA:Slick.

Bit #3 was RIH after setting the 13 3/8" casing. Cement was tagged at 1117.0m. The cement, float collar and casing shoe were then drilled out. An additional 5m of rathole was drilled from 1165m to 1170m. Prior to POOH the junk basket was surged with 71bs of junk being recovered.

Bit #5;

Type:Hughes HTC B9M+

Nozzles: $5 \times 13, 12$. In:1170m.

Out:1352m.

Rot:11.5hrs.

ROP: 16m/hr. Wear: 10%. BHA: packed.

Bit #5 was RIH with a positive displacement mud motor and a MWD tool situated 9.4m behind the bit. The bit was RIH to 1159.0m, circulation was then broken, washing and reaming continued to TD at 1170m. Drilling continued from 1170m. A depth of 1352m was reached before a 1200psi drop in stand pipe pressure made it necessary to POOH. On surface it was revealed that the PDM motor had twisted off below the dump valve. A fishing assembly was rigged and RIH. The fish was engaged and retrieved on the first run.

Well : Angler # 1

PHASE SUMMARIES Country : Australia

12 1/4" PHASE REPORT cont'd

An attempt to rerun the PDM was temporarily setback when a pin sheared in the stabilizer above the mud motor while surface testing the MWD tool.

The mud motor had twisted off at surface. The fishing assembly was rigged and run for a second time. Circulation was broken above the fish at approximately 1344m. An attempt to engage the fish was thought to be successful. It was later revealed that it fact the overshot had not caught the fish. Consequently a new fishing assembly was rigged and RIH. The fish was eventually engaged and POOH with 50Klbs overpull. The mud motor was subsequently retired from drilling operations.

Bit #6;

Rot:27.0hrs Type: Reed HP43A. Nozzles:2 x 13,14. ROP:13.0m/hr. Wear:1/1/I. In:1352m. Out:1740m. BHA: packed.

Prior to RIH the Teleco. Tool failed a surface test and was laid down. Subsequently Bit #6 was RIH without a MWD. Circulation was broken at the shoe at 1151m. The bit then continued to wash and ream to bottom at 1352.0m. Prior to 1350m the mud system was opened, and consisted predominantly of seawater with frequent hi-vis sweeps. A decision was taken, and the mud system was closed in to allow the system to naturally weight up as hi-vis pills were continued to be pumped. The mud weight steadily increased from 1.04Sg at 1445m to 1.15SG at 1680m. Rotary drilling continued to 1740m without any notable drag on connections. Bit #6 was then prematurely POOH to allow a newly arrived mud motor to resume drilling. On the way out the entire 5"drill pipe was laid down.

Bit #5RR;

Type:Hughes HTC B9M+. Rot:0.6hrs. ROP: 0-10m/hr Nozzles: $5 \times 13,12$. Wear: 10%. In:1740m. BHA: packed. Out: 1742m.

Bit #5RR was RIH with a mud motor and MWD tool. Once on bottom a very slow drill rate associated with a 400psi drop in pump pressure made it necessary to POOH. The mud motor was subsequently blamed for the drop in pressure and laid down.

Bit #7;

Type:Reed HP43A. Rot:43.7hrs. Nozzles: $2 \times 14,13$. ROP:5.7m/hr. Wear:3/3/1:8 In:1742m. BHA:packed. Out:1992m.

Company : Petrofina Exploration Australia _____

Well : Angler # 1

-----PHASE SUMMARIES Country : Australia

12 1/4" PHASE REPORT cont'd

Bit #7 was RIH with a MWD tool. Circulation was broken at 1735.0m. Washing and reaming continued to 1742.0m. Rotary drilling recommenced from 1742m to 1779m, where a 400psi increase in pump pressure was detected. A blocked nozzle was suspected, nevertheless drilling continued with a reduced flow rate until 1992m. Prior to POOH the hole was displaced with a Gel/polymer mud system.

Bit #8;

Type:Reed HP 13GJ.

Rot:14.Ohrs. Nozzles:2 x 14,13. ROP:7.5m/hr. Wear:2/3/1:8

In:1992m. Out:2097m.

BHA: packed.

Bit #8 was RIH without either a mud motor or MWD tool. Circulation was again broken at the shoe prior to continuing to RIH. The hole was then washed and reamed from 1988m to 1992m. The junk basket was worked off bottom before drilling ahead. Rotary drilling recommenced from 2097m and continued to 2097m. The hole was then circulated out, a single shot survey dropped, and a slug was pumped. Bit #8 was prematurely POOH to allow a mud motor/PDC bit combination to drill the just newly penetrated Lakes Entrance Formation.

At 1997.0m a carbide test revealed the hole to be 18% overgauge,

or an open hole with an average diameter of 15 inches.

Bit #5RR2

Type:Hughes HTC B9M+. Nozzles:5 x 15,12.

In:2097m. Out:2918m. Rot:17.8hrs. ROP:46m/hr Wear:50% BHA: packed.

Bit #5RR2 was RIH with a mud motor and MWD tool. Circulation was broken at 2088m. Washing continued to 2092m. New 12.25" hole was then drilled from 2092m. A drill break at 2767m was circulated out in an attempt to locate the Gurnard Formation. Drilling resumed from 2767m without notable drag on connections. Good returns were continuously observed over the shakers. At 2918m the hole was circulated clean , and Bit #5RR2 was POOH. The first stand pulled recorded a maximum overpull of 50Klbs, thereafter minimal drag was observed.

Once out of the hole Schlumberger prepared for the intermediate logging runs. The first run could not pass 2330m in the Lakes Entrance Formation and was subsequently retrieved. A BHA was then made-up consisting of a near bit roller reamer and RIH. Hole fill was tagged at 2906m, 12m off bottom. Two 40bbl hi-vis sweeps were then circulated. Heavy returns were observed over the shakers as the 12m fill was circulated out of the hole. Electric logging recommenced, and two logging runs were completed before rigging to run the 9 5/8" casing.

Company : Petrofina Exploration Australia 3.7

Well : Angler # 1

Country : Australia PHASE SUMMARIES

12 1/4" PHASE REPORT cont'd

WOB/RPM/FLOW RATE PRACTICES.

This phase was drilled by employing maximum allowable drilling parameters. Originally this section was to be drilled entirely by a mud motor/PDC combination, however problems with the mud motors made it necessary to employ conventional insert bits. For the most part the insert bits drilled with 35-50Klbs with a rotary of 60 to 65rpm. The flow rates also varied little, and were between 600-550gpm. An exception to this was Bit #8 which drilled with an reduced flow rate of 500gpm due to a blocked nozzle.

The only PDC bit to be used was eventually reran on three occasions. Initially this bit drilled from 1170m to 1152m with 10-25Klbs on the bit, and 40-80rpm on rotary. These relatively low parameters were employed to allow straight hole to be drilled out of the 13 3/8" casing shoe. On the second occasion the bit was POOH after only 2m had be drilled due to a malfunctioning mud motor. On the last occasion the drill rate was restricted to 3.5 singles an hour through the Lakes Entrance Formation. In general this section of the phase was drilled with 40-50Klbs on the bit, and 140rpm on the rotary. The flow rate for all PDC runs was approximately 780gpm.

HYDRAULICS: (See table below).

The 12.25" phase hydraulics were optimized with power ratios of 0.60-0.74 for the Reed insert bit runs. Turbulent flow was also established in the immediate vicinity of bit, however in some instances turbulent flow was created higher in the annulus. A carbide test and a Schlumberger Caliper Log proved the hole was on average 15 inches in diameter.

The Hughes PDC bit was run with a positive displacement mud motor, hence the power ratios don't truly reflect the total power established at the bit.

Well : Angler # 1

PHASE SUMMARIES Country : Australia

12 1/4" PHASE REPORT cont'd

P)	nase	Н	draulics	Su	ummary Tab	16	e: 					==	-=====	===	=======	==	======
	Bit No.	:	Bit Type	:	Interval m	:	PDM		FR gpm				Power Ratio		Nozzles		SPP ;
I	===== 5	:	Hughes HTC B9M+	; ;	1170- 1352	:	YES	:	780		Turb	1 1	0.32	!	5 x 13, 1 x 12	!	3000 ;
-	6	! ! !	Reed HP 43A	:	1352- 1740		NO	t 1	630	!	Turb	1 1 1	0.68	!	2 x 13, 1 X 14	:	3100 ;
!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!	5rr		a/a	!	1740-42	!	YES	!	750	!	Turb	1	0.29	:	5 x 13, 1 x 12		3000 ;
-	7	!!!!	Reed HP 43A	:	1742- 1992	!	NO	•	510 /640	!					2 x 14, 1 x 13		2000 /3100
	8	!!!!!	Reed HP 13Gj		1992- 2097	!	NO	;	650	1	Turb /lam		0.63		2 x 14, 1 x13	!!!	3050
	5rr	2 ;	a/a		2097- 2918	:	YES	:	680	:	 Lam 		0.15	1	5 x 16, 1 x 12		3100

Note: PDM-Positive displacement mud motor.

Turb/lam:refers to type of flow around the drill collars.

Bit #7: Two flow rates due to blocked nozzle.

CASING AND CEMENTING

216 joints of N80 471b/ft BUTT Grade 3 9 5/8" casing were run to a depth of 2888.14m. Cementing was as follows:

SPACER: 10 bbl of freshwater followed by 20 bbls of a mix of freshwater and scavenger slurry.

LEAD :681 bbl total made up of Class G cement plus 2.5 %prehydrated gel and 108 gal/sac freshwater to give a 12.8 ppg.

TAIL: 102 bbl made up of Class 'G' cement plus 4 gal/10 bbl HR-6 and 5 gal/sac freshwater to give a weight of 15.8 ppg.

DISPLACEMENT: The cement was displaced first with 23.6 bbl of freshwater and 600 bbl of drilling mud.

Well : Angler # 1

Country : Australia _____

8 1/2" PHASE REPORT

to: 4330m From : 2918m

to: 13 - 05 - 89 From: 26 - 04 - 89

The 8 1/2" phase was drilled from 2918m to 4330m using 6 bits and and one 9m core barrel, and took 173.95 rotary hours to drill.

Rot: 1.25hrs ROP: 4 m/hr BIT #RR2 Type: REED HP11G

Nozzles: 3 x 13 Wear:7/3/1/8" In: 2918m Out: 2985m BHA: Pendulum

A rerun bit #RR2, a REED 11G with 3 x 13" nozzles was used to drill out the cement, float collar and shoe from 2822m to 2830 m, and the rat hole to 2923m. After circulating to condition the mud and flush the riser, the bit was pulled to the casing shoe for a L.O.T., which yielded a value of 1.60 sg. New formation was then drilled from 2923m to 2985m. After displacing hole with 1.10 sg mud and checking for flow the bit was pulled from the hole.

Type: Chr.R437 Rot.: 57.5 hrs BIT #9 Nozzles: 4 x 12 ROP : 9.1 m/hr Wear: 100%, In In: 2985m

BHA: Pendulum Out: 3507m

Bit #9 was run into the hole with the Teleco MWD tool and reamed and washed from 2967m to 2998m. New formation was then drilled from 2998m to 3227m. At 3227m a ten stand wiper trip to 2930m was performed . During the trip a max overpull of 20 Klbs was observed. New formation was then drilled from 3227m to 3507m.

Rot.: 44.75 hrs Type: Reed HP51A BIT #10 ROP: 7.2 m/hr Wear: 5/4/.125 out Nozzles: 3 x 13

In: 3507m

BHA: Pendulum Out: 3832m

Bit #10 was run into the hole with the Teleco MWD tool. After washing down from 3491m to 3507m, new formation was drilled from 3507m to 3833m.

Well : Angler # 1

PHASE SUMMARIES

The maximum drag experienced during connections was 5,000 lbs, with a maximum measured torque of 4,000 ft/lbs. At the TD of 3833m, a flow check was performed, but no flow was measured. A bottoms-up sample was circulated out and another flow check was performed with negative results. Bit #10 was pulled from the hole, with a final flow check made at the base of the 9-5/8" casing shoe. A Teleco survey made at 3827m indicated that the deviation drift had increased to 1.5 degrees at TD.

Type: Chr. 303HS Rot: 8.0 CORE BIT #1 Nozzles: --Rop: 1.125 Wear: 60% In: 3833m

BHA: Pendulum Out: 3842m

Core bit #1 was run into the hole with a 20m core barrel assembly. Difficulties were encountered while running in, with tight spots occurring because of an undergauge hole. After becoming stuck and working free, it was decided to pull the core bit assembly from the hole, having reached a depth of 3788m. Bit #12, a Reed S32G with 3 x 13 nozzles, junk sub and a near-bit roller reamer was run into the hole. The hole was washed and reamed from 3255m to 3717m, with tight hole conditions making it necessary to jar the string on nearly each single. Maximum overpull upwards was 480,000 lbs, and downward was 320,000. After reaching 3717m, the reaming assembly was pulled from the hole. Bit wear was rated at 2/1/1/16-under, the roller reamer at 1/4" under gauge, and the stabilizer 1/16" under gauge. Bit #13, a Reed S316 with 3 x 13 jets, was run into the hole to 3700m. The hole was washed and reamed from 3700m to 3833m. The maximum upwards overpull experienced during this run was 440,000 lbs and downwards overpull reached a maximum of 330,000 lbs. After reaming to the bottom of the hole at 3833m, the string was pulled to 3177m, experiencing only 20,000 of overpull. The reaming string was then pulled from the hole. Core bit #1 was refitted along with a 10m core barrel and run into the hole, experiencing little problem in reaching TD at 3833m. Core #1 was cut from 3833m-3842m in 8 hrs and retrieved from the hole with a recovery of 99%.

Rot. 34.7 hrs Bit #14 Type: HTC B35M Nozzles: 3 x 12 Rop: 6.8 m/hr In: 3842m Wear: 40%/I

BHA: Pendulum Out: 4079m

Bit #14 was run into the hole with the Teleco MWD tool. string encountered tight hole at 3976m and was washed and reamed down to 3842m. Drilling commenced and hole was made from 3842m to 4039m. High torque while drilling this section resulted in

Well : Angler # 1

PHASE SUMMARIES Country : Australia

poor functioning of the Teleco MWD tool. A wiper trip was made back to 3775m and six singles laid down. The string was run in hole to 3825m, and the hole was slowly reamed from 3825m to 3842m while the section was re-run with the MWD logging tool. Following the success of the logging run, the bit was run back to 4039m. Drilling was resumed from 4039m until reaching a depth of 4079m, where high torque was encountered and the bit could no longer drill formation. A slug was then circulated prior to tripping out of the hole.

Rot. 14.6 hrs Rop: 10.6m/hr Bit #15 Type: CDC R435S Nozzles: 4 x 12

In: 4079m Wear:50%/I BHA: Pendulum Out: 4234m

Bit #15 was RIH with a MWD tool. Circulation was then broken at 4043m. Reaming and washing continued to total depth at 4079m. The bit was gradually broken before drilling ahead. At the 4182m connection 50Klbs overpull was registered. Subsequently a 10std wiper trip was performed before drilling ahead. Thereafter 15Klbs overpull on average was observed on connections. Bit #15 was POOH due to lack of penetration at 4234m. Slight overpull was observed on the initial stands pulled, thereafter no drag was recorded during tripping.

Rot. 23.75hrs Type: REED HP53A Bit #16 Nozzles: 11/14/B Rop: 4.0 m/hr

Wear: 1/2/1/16" In: 4234m BHA: Pendulum Out: 4330m

Prior to RIH with Bit #16 a new MWD tool was picked up and surface tested. Drilling continued from 4234m with a maximum of 15Klbs overpull on connections. At total depth of 4330m bottoms up was circulated while working the string. A wiper to the 9 5/8" casing shoe was then performed with a maximum of 15Klbs overpull recorded while tripping. As the bit was returned to bottom no hole fill was tagged. The mud was circulated and conditioned before pumping a slug and POOHmaximum drag 15Klbs.

Well : Angler # 1

Country : Australia PHASE SUMMARIES

8 1/2" PHASE REPORT cont'd

WOB/RPM/FLOW RATE PRACTICES

To insure vertical hole was drilled out of the 9 5/8" casing shoe, a wob of 15Klbs with a rotary of 120rpm was initially employed. As new vertical hole was established the wob was gradually increased to 25Klbs with a rotary of 95rpm. An essentially sandstone formation persisted from 3000m to 3700m, however, at 3173 through to 3330m thin coal seams prompted a reduction of the wob to 20Klbs with a increased rotary of 100 rpm. From 3700m onward thin, though hard siltstone interbeds necessitated an increase in wob to 30-35Klbs with a rotary of 95rpm. This siltstone developed with depth and persisted as a 100% siltstone from 3930m to 4200m. As PDC bits were used to drill this section of the hole a wob of 15-25Klbs with a rotary of between 80-90rpm proved adequate. From 4200m to 4330m(T.D.) a moderately hard to hard pyritised sandstone was drilled with an insert bit with a wob of 35-40Klbs and a rotary of 70-80rpm.

The flow rates from 2900m to 3833m were generally held steady at between 450-480gpm, however, from 3833m onward the flow rate was reduced to 350-360gpm to avoid damaging turbulent flow higher in the annulus, while also keeping within pressure loss restrictions.

D. J. Circ. Franchisco Australia

Company: Petrofina Exploration Australia 3.13

Well : Angler # 1

Country : Australia PHASE SUMMARIES

8 1/2" PHASE REPORT cont'd

HYDRAULICS: (See Table below.)

The 8.5" phase hydraulics due to pressure loss restrictions weren't optimised with power ratios ranging from 0.36 to 0.57. Turbulent flow was in most cases generated in the immediate vicinity of the bit, while laminar flow was noted higher in the annulus.

Phase Hydraulics Summary Table:

			yuraulics					_			=====	====	=======
	Bit No.	•	Bit Type		Interval met	:	FR gpm	-		Power Ratio		es ¦	SPP ;
	2rr	:=:	Reed HP 11G		2918m - 2985m	!	450		Turb	0.45	3 x 1	3, ;	3000
:	9	!	Chris ECR 437		2985m - 3507m	1	480	1	Turb	0.36 	4 x 1	2 ;	3150
!	10	;	Reed HP 51A	!	3507m - 3833m	!	470		Turb	0.39	3 x 1	3 ;	3000 ;
1	11	;	CT 303	:	3833m -		Core	b	arrel u	unable to	reach	bot	tom :
	12 &13	!	Reed S31G	1 1 1	3833m -				ight ho	ole prior 13.	to co	ring	with
	11rr	· -	DB CT 303	!	3833m - 3842m 9m Core:99%Rec	•	290	1 1	_	-	, –	1	1340
!	14		Hughes HTC B35M+		3842m - 4079m	!	360	!!!!	Turb	0.45	3 x 1	2 ;	2200
1 1	15		CDC R435S		4079m - 4234m	1	374	1 1 1	Turb	0.44	4 x 1	.2	1900 ;
	16		Reed HP 53A		4234m - 4330m	:	350		Lam	0.57	11/14	/B :	3000

PE904714

This is an enclosure indicator page.

The enclosure PE904714 is enclosed within the container PE903251 at this location in this document.

```
The enclosure PE904714 has the following characteristics:
    ITEM_BARCODE = PE904714
CONTAINER_BARCODE = PE903251
            NAME = Angler-1 Bit Cost Charts
            BASIN = GIPPSLAND
        ONSHORE? = N
       DATA TYPE = WELL
   DATA_SUB_TYPE = DIAGRAM
     DESCRIPTION = Angler-1 Bit Cost Charts, VIC/P20,
                    W993. 12 charts. Charts within
                    "Angler-1 Final Well Report"
                    (PE903251).
          REMARKS =
    DATE_WRITTEN =
  DATE_PROCESSED =
   DATE_RECEIVED = 02-OCT-1989
   RECEIVED_FROM = Petrofina Exploration Australia S.A.
       WELL_NAME = Angler-1
       CONTRACTOR =
           AUTHOR =
       ORIGINATOR =
       TOP_DEPTH =
     BOTTOM_DEPTH =
   ROW_CREATED_BY = EC00_SW
```

(Inserted by DNRE - Vic Govt Mines Dept)

Company	 :	Petrofina Exploration Australia	 4.1
Well	:	Angler # 1	
Country	: 	Australia	 BIT REPORT

BIT REPORT

!	BIT	!	TYPE	} ;	SIZE	1	NOZZLES	;		!	RUN	1	ROT	1 1	WOB :	! !	FR	1 1	SPP	1	WEAR	!	ĦĦ	!	RENAF	KS
;	NO.	1		; ;		1		1	IN set	1	net		hrs	1	Klbs ;	(g p e	1	psi ·	1		;	Sg	1		
:	1		REED Y	11 ;	26"	;	4 x 11	!	303	;	60	;	5.5	;	0-3 ;		275	;	300	;	1/1/I	;	1.04	;		
;	1RR	;	REED Y	11 ;	26"	;	4 x 11	;	363	;	2		0.5	;	5 ;	;	350	;	2200	!	1/1/I	 ¦	1.04	;		
) <u>;</u>	2		REED HP	 11J ;	8.5	;	NONE		365	!	220	;	9.75	;	5 ;		500	;	1600	!	2/1/1	;	1.04	;	PILOT	HOLE
;	3	 !	REED HP	11J ;	12.25	• ;	3 x 12		585	;	28	:	1.25	;	10 ;		550	t 1	1660	;	2/2/1	;	1.05	;	OPEN H	10LE
;	4	;	HTC CX	34 ;	12.25	• :	4 x 14	;	613	;	552	:	29.5	;	10/25	(900	, ,	3400	;	3/3/I	;	1.06	,		
:	3RR	:	REED HP	11J!	12.25		3 x 15		1165	;	5	;	1.0	;	15/20;	. (600	!	1900	;	2/2/I	;	1.06	!		
;	5	:	HTC B9M	+ ;	12.25		5x13,1x1	2;	1170	;	182	;	11.5	;	10/15;		780	,	3000	:	107	:	1.06	;		
:	6		REED HP	 42A ¦	12.25	•;	2113,111	 4;	1352	;	388	;	27.0	;	25/40;	. (650	;	3100	;	1/1/I	:	1.08	;		
:	5RR	,- !	HTC B9H	+ ;	12.25	• ;	5113,111	4;	1740	;	2	;	0.6	;	30 ;		300	<u>. </u>	3100	;	102	1	1.08	;		
:	7	 ! !	REED HP	43A ;	12.25	• ;	2x14,1x1	3;	1742	;	251	;	43.7	;	40/45		550		3500	!	3/3/ 1/8	• ;	1.08	;		
1	6	;	REED HP:	 136J¦	12.25	•;	2X14,1X1	3;	1992	;	105	;	14	;	40/50;		30	· - ·	3150	;	2/3/ 1/8'	• ;	1.15	;		
 ;	5RR	!	HTC B9M	+ ;	12.25	• ;	12,5x16	1	2097	;	821	;	17.8	;	50/70;	7	780		3300	;	50% IN	;	1.1	:		
:	RR2	!	REED HPI	116J;	8.5	!	3113	:	2918	;	67	;	7.,5	′	30/45;	4	150		3000	!	7/3/1/8*	;	1.1	:	Drill	shoe
:	9	::0	CHRIS EC	R437:	8.5	;	4x12	 !	2985	;	522	;	41.5	!	15/25;		180		3150	;	1002,1	1	1.11	;	D\A.	
 !	10		REED HP:	51A ¦	8.5	;	3x13	;	3507	;	326	!	43.9	!	35/40;	4	70		3000	;	5/4/1/8"	i 1	1.12	 !	P00H,C	ore.
,	11	;	DB,CT 30)3 ;	8.5	!	+	;	2823	;	-	;	-	:	- ;		- ;		-		- ; PC	ЮH	due to		Tight	hole;
!	12		REED S31	lG ;	8.5 '	;	3x13	;	REAMING	1	IGHT	H(OLE FR	01	3507 a	t	o 38	33	S 6							
!	13	;	REED S31	16 ;	8.5	;	3x13	;	REAM TI	GH	IT HOL	Ε.	PRIOR	1	O CORI	NG	ì.									

С	omj	рa	ny	:	Pε	et:	rofin	na	Ex	pl	or	a	ti	O	n A	ust	cr	ali	a								4.
W	el.	1		:	Ar	ıg.	ler t	 ‡	1			_		-					_		_						
c	oui	nt	ry	 :	Αι	ıs	tral	ia				_							_				_			BIT	REPORT
_										BI	T	R	EP	O.	R T	cor	ıt		-		-		_				
,		;		1				1	IN			•		1		} !	;		1	•	1		!	REMARKS	1		
	11rr	. ;	DB,CT303	;	8.5	• ;		;	3833	; 1	9	 !	 8.0	; ;	5/20	; 290	; 1	1340	!	602	;	1.12	;	Core #1	;		
· - ·	14	;	HTC B35	+ ;	8.5		3112	į.	3842	!	237	!	34.7	!	15/25	; 360	;	2200	!	402/I	:	1.13	;	D/A	;	,	
)	15	;	CDC R4359	;	8.5	• ;	4x12	;	4079	! :	155	;	14.6	;	22	374	;	1900	;	502/I	;	1.14	1	POOK	!		
:	16	;	REED HP53	A ;	8.5	• ;	11/14/B	;	4234	;	96	:	 23.7	5;	30/35	; 350	;	3000	;	1/2/1/16	;	1.15	;	TD.	;		

______ Company : Petrofina Exploration Australia Well : Angler # 1 _____ MUD REPORT Country : Australia MUD RECORD ! Depth : MW ; FV ; PV ; YP ; Gel ; PH ; WL ; CL ; CA ; SOL ; H2O ; SND ; CAKE ; pf/mf ; REMARKS ; ; 303m-1386m Drilling with sea-water and Hi-vis sweeps in a open and system. : 1387m : 1.04 : 29 : 1 : 1 : 1/1 : 9.0 : - : 21K : 1320 : 2 : 98 : tr : - :.06/.11 : ------! 1445m ; 1.04 ; 28 ; 2 ; 1 ; 0/1 ; 9.9 ; - ; 21K ; 1320 ; 2 ; 98 ; tr ; ; ; 1538e ; 1.06 ; 28 ; 2 ; 2 ; 0/1 ; 9.1 ; - ; 21K ; 1680 ; 2 ; 98 ; tr ; ; ; ; ; _____ ; 1641m; 1.08; 30; 1; 4; 1/2; 9.6; -; 20K; 1520; 3; 97; tr; [.1/.18] ; 1757 ; 1.11; 29 ; 2 ; 3 ; 0/1 ; 9.3; -; 20K; 1360; 4 ; 96; tr; ; .06/.12; : 1836 | 1.11 | 29 | 2 | 3 | 0/1 | 9.7 | - | 20K | 1160 | 4 | 96 | tr | .07/.16 | ------! 1889 | 1.11 | 29 | 2 | 3 | 0/1 | 9.3 | - | 20K | 1160 | 4.2 | 95 | tr | [.07/.16 | : 1956 : 1.12 : 29 : 2 : 3 : 0/1 : 9.4 : - :19.5K: 1080 : 4.2 : 97 : tr : : .06/.13: : 1993 | 1.08 | 38 | 10 | 8 | 1/1 | 10.0 | 5.4 | 17K | 560 | 3.3 | 96 | tr | 1 | 1.07/.16 | : 2062 ; 1.09 ; 40 ; 10 ; 8 ; 1/2 ; 9.6; 5.6;16.5K; 600 ; 3.3 ; 96 ; tr ; 1 ; .07/.19; : 2534 : 1.15 : 46 : 15 : 15 : 2/10 : 9.5: 6.0:15.5K; 580 : 6.4 : 93 : 0.25: 1 : .10/.28: ______ ______ ; 3118 ; 1.12 ; 43 ; 13 ; 15 ; 3/5 ; 9.7 ; 4.8;18.5K; 140 ; 6.3 ; 93 ; 0.60; 1 ; .06/.9 ; -----: 3355 ; 1.12 ; 43 ; 14 ; 13 ; 3/5 ; 10.8; 4.9;18.5K; 60 ; 5.3 ; 94 ; 0.25 ; 1 ;.12/.9 ; ; 3508 ; 1.12 ; 45 ; 17 ; 15 ; 3/8 ; 10.9; 4.8;19.0K; 280 ; 5.2 ; 94 ; TR ; 1 ; .23/.9 ; Drill ahead ; ______ ; 3590 ; 1.12 ; 44 ; 15 ; 3/4 ; 10.0; 5.0;19.0K; 360 ; 5.2 ; 94 ; TR ; 1 ; .1/.8 ; POOH/RIH,D/A. ; _____ ; 3756 ; 1.12 ; 45 ; 16 ; 15 ; 3/6 ; 10.3; 5.0;19.0K; 280 ; 4.2 ; 95 ; TR ; 1 ; .15/.7 ; Drill ahead ; ______ ; 3832 ; 1.13 ; 46 ; 17 ; 17 ; 3/9 ; 10.6; 5.1;19.0K; 240 ; 5.2 ; 94 ; TR ; 1 ; .17/.8 ; Drill ahaed ;

Company : Petrofina Exploration Australia 4.4

Well : Angler # 1

Country : Australia MUD REPORT

MUD RECORD cont'd

======	===	===	===	==	===:	===	===	==	===	==	====	==:	====	==:	===	==	===	==:	====	==:	===	==	===:	==	===:	==	=====	==	::::::::	=		===
; Dept	h ;	1	16	;	F۷	1	PV	1	YP	!	Gel	;	PH	;	WL	;	CL	;	CA	;	SOL	;	H2() ;	SNI) ;	CAKE	!	pf/mf		REMARKS	:
; 3832	;	1.	.13	;	44	!	15	;	12	;	3/5	;	10.	5;	5.4	1;1	9.() K ;	160	;	5.2	;	94	:	TR	;	1	;	.19/.9		Test BOP.	;
; 3833	;	1.	.13	;	46	!	16	!	15	!	3/9	;	10.	7¦	4.8	3;1	9.0) K ;	360	!	5.2	;	94	;	TR	1	1	!	.29/.7	;	REANING	!
3842	.;	1.	.13	;	51	;	19	;	19	;	3/12	;	11.	0;	4.9	?;1	9.() K ;	480	;	5.2	;	94	!	TR	;	1	;	.45/1	;	CORING	!
; 3944	;	1.	.13	!	48	;	16	;	16	;	4/1	3;	9.9	;	5.4	 ¦1	9.0) K ;	480	;	5.2	;	94	;	TR	;	1	;	.25/.83	;	D/A.	;
4058	;	1.	.14	;	53	!	19	;	18	;	6/18	;	9.5	;	5.3	; 1	9.0) K ;	420	;	5.2	;	94	!	TR	;	1	;	.18/.42	;	D/A.	;
; 4079	;	1.	.14	;	51	; i	18	;	19	1	5/18	;	9.4	;	5.6	; 1	9.0	K!	420	;	5.2	;	94	!	TR	;	1	!	.18/.4	;	TRIP, TEST BO	OP;
4234	;	1.	.14	;	56	;	19	;	21	;	7/21	;	10.	1;	6.5	; 1	9.0	K;	440	;	5.2	;	94	;	TR	;	1	;	.26/.3	}	DRILL,POOH.	;
; 4302	;	1.	.15	;	56	;	19	;	22	;	6/20	;	9.6	;	6.8	};1	9.0) K ;	440	!	5.2	!	94	1	TR	;	1	;	.17/.3	?	RIH,DRILL.	;
; 4330	;	1.	.14	:	53	;	17	;	20	:	7/24	;	9.9	;	6.4	1;1	9.0) K ;	380	;	5.2	;	94	1	TR	!	1	;	.18/.3	j	DRILL TO TD.	. ;

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Company : Petrofina Exploration Australia 5.1
Well : Angler # 1

Country : Australia GEOLOGY SUMMARY

INTRODUCTION

Angler # 1 is located on a normal fault trap in the northern part of Permit VIC/P20 in the Bass Strait. The structure is situated along a NW-SE trending fault, with dip closure to the south and fault closure to the north. The Angler prospect lies within the central part of the NW-trending Gippsland Basin. Gippsland sedimentation occurred in three phases, each separated by periods of structural deformation marked by regional unconformities. Rifting and volcanism in the Late Jurassic/Early Cretaceous was followed by deposition of sediments of the Strezlecki Group. Continued wrench faulting and rifting related to the opening of the Tasman sea during the Late Cretaceous to Middle Eocene gave rise to the deposition of the Latrobe Group. Latrobe sediments are comprised of up to 2500m of shallow marine and continental shales, coals, and sandstones. represent a regressive sequence from upper delta/braided stream to back barrier/paludal swamp sediments, culminating in shallow marine sedimentation. The last phase of basin development involved the deposition of the Late Eocene to Recent Seaspray Group, formed during a widespread thermal sag phase. During this time, upper continental marls and claystones of the Lakes Entrance and calcarenites and calcilutites of the Gippsland Limestone were deposited. The sediments of the Seaspray Group form a seal for hydrocarbon-bearing strata of the Latrobe accumulations.

Potential reservoirs in the Angler prospect include Latrobe sandstones of deltaic and lower coastal plain origin. The predicted source interval was within thick coals and coaly shales of the Campanian lower coastal plain sequence. The primary objective is the Selene Sandstone, previously intercepted in the nearby Selene-1 and Hapuku-1 wells, where it reaches 100m+ in thickness. The presence of 200m of coaly shale above the Selene should provide a sufficient seal for hydrocarbons which have migrated up-dip and up-fault under the Angler prospect. The predicted hydrocarbon type was oil, with potential gas in over-mature Lower Campanian sequences.

Company : Petrofina Exploration Australia 5.2

Well : Angler # 1

Country : Australia GEOLOGY SUMMARY

LITHOLOGIC SUMMARY

303-613m Returns to sea floor.

CALCARENITE: white to off-white to grey, firm to 613-800m moderately cemented, sucrosic texture, fossiliferous, forams common, traces of glauconite, pyrite and mica.

800-880m CALCILUTITIC CALCARENITE: light to medium grey, fine to medium grained, chalky texture, moderately well cemented, calcilutite matrix, soft to firm, fossiliferous, common forams, glauconitic, trace

mica, poor visible porosity.

880-960m CALCARENITIC CALCILUTITE: light to medium grey, chalky texture, moderately well cemented, calcite cement, trace of argillaceous matrix, fossiliferous, abundant forams, traces of glauconite and

mica, trace of dolomite, poor visible porosity.

960-1070m CALCILUTITE: light to medium grey, chalky texture, moderately well cemented, calcite cement, fossiliferous, abundant forams, traces of glauconite and

mica, trace dolomite, nil-poor visible porosity.

1070-1210m MARL: light grey, soft, sticky, plastic, occasionally silty.

CALCARENITE: off white to tan, firm to moderately 1210-1720m hard, occasionally hard,, fine to very finely crystalline, rarely coarsely crystalline, common very fine to fine grained, moderately well cemented, common white calcite matrix, common forams, calcareous spicules, traces of glauconite, no vis

porosity, grading to lt gy, sft CALCILUTITE.

CALCARENITE: light grey-light brown-off white, mod 1720-2060m hard-hard, blocky-subfissile, very fine to fine grained, micro- to occasionally finely crystalline, moderately well to well cemented, calcareous/argilaceous matrix, trace forams, traces of glauconite

and dolomite, no visible cement

-----Company : Petrofina Exploration Australia ______

Well : Angler # 1

_____ GEOLOGY SUMMARY Country : Australia

LITHOLOGY SUMMARY

CALCILUTITE: light grey to off white, soft to firm, occasionally moderately hard, chalky to plastic in part, occasionally silty, calcareous/argillaceous matrix, no visible porosity.

MARL: light brown to light grey, predominantly 2060-2200m soft to hard in part, chalky-sticky, calcareous matrix, occasionally with argillaceous matrix, dispersive, slightly silty.

CALCAREOUS CLAYSTONE: light brown to grey, soft to 2200-2770m dispersive, firm in part, blocky, silty in part, minor aggregates of microxtalline pyrite, grading to shale, marl in part.

> SANDSTONE: brown to green to clear, dominantly unconsolidated, very fine to coarse grained, subangular to subround, poorly sorted, argillaceous matrix, common coarse glauconitic grains, poor to excellent inferred visible porosity, no shows

SANDSTONE: translucent-transparent, occasionally light grey to light brown, medium to coarse grained, poorly to moderately sorted, angular to subround, predominantly loose grains, weakly to moderately cemented with silica, common quartz over growths, locally common dissemenated pyrite, tr mica, tr glauconitic pellets, grading to siltstone in part.

SILTSTONE: light to medium grey, brownish-grey in part, firm to hard, trace calcareous cement, trace argillaceous matrix, pyritic in part

transparent-translucent, loose, coarse SANDSTONE: to medium grained, occasionally fine grained, poor to moderately sorted, subangular to subrounded, trace of dissemenated pyrite, poor to fair inferred porosity, grading to coal and siltstone in part, no shows.

SILTSTONE: light grey to light brownish-grey, firm, commonly carbonaceous, traces to common interlaminated coals, poor to no inferred porosity, tr cut fluorescence.

2770-2920m

2920-3023m

3023-3325m

Company: Petrofina Exploration Australia 5.4

Well : Angler # 1

Country: Australia GEOLOGY SUMMARY

LITHOLOGY SUMMARY

COAL: black-dark grey to brownish black, dominantly subvitreous to vitreous in part, firm to hard, blocky to subconchoidal in part, fractured.

3325-3490m

SANDSTONE: transparent to translucent, loose, medium to coarse grained, subangular to subrounded, poorly to moderately sorted, no visible cement or matrix, traces of dissemenated pyrite, fair to good inferred porosity, no shows, grading to siltstone in part, tr coal

SILTSTONE: medium to dark grey, subfissile to subblocky, soft to firm to brittle in part, carbonaceous in part, common argillaceous matrix.

COAL: black to dark grey, subvitreous to vitreous, brittle.

3490-3520m

CLAYSTONE: medium grey to dark grey, soft to firm, subblocky to subfissile, carbonaceous, silty in part, trace fluorescence, bright yellow cut, med yellow residual fluorescence.

SILTSTONE: light to dark grey, occasionally brown-brownish grey, soft to firm, subblocky, carbonaceous, common to abundant argillaceous matrix, grading in part to silty claystone

SANDSTONE: transparent-translucent, loose, coarse to fine grained, predominantly medium grained, subangular to subrounded, moderately to well sorted, no visible cement, tr dissemenated pyr, fair to good inferred porosity, poor to fair yellow direct cut fluorescence.

3520-3560m

SANDSTONE: transparent-translucent, coarse to fine grained, dominantly medium grained, moderately to well sorted, subangular to subrounded, no visible cement, trace of dissemenated pyrite, fair to good inferred porosity, trace direct fluorescence, cut fluorescence, grading to siltstone in part.

3560-3620m

SANDSTONE: 70% unconsolidated--transparent-translucent, coarse to fine grained, predominantly coarse to medium grained, moderately sorted, no

Company: Petrofina Exploration Australia 5.5

Well : Angler # 1

Country: Australia GEOLOGY SUMMARY

LITHOLOGIC SUMMARY

visible, trace dissemenated pyrite, fair to good inferred porosity. 30% consolidated—off white to translucent, fine grained, silty, well sorted, well cemented, silica cement, trace to common argillaceous cement, trace pyrite.

SILTSTONE: light to dark grey, occasionally brownish-grey, soft to firm, subblocky-subfissile, carbonaceous, common argillaceous matrix, grading to carbonaceous claystone.

CLAYSTONE: medium to dark grey, firm to dispersed in part, generally amorphous, carbonaceous in part.

3620-3690m

SANDSTONE: transparent-translucent, loose, medium to to coarse grained--occasionally fine grained, moderately to poorly sorted, subangular to subround, no visible cement, occasionally argillaceous matrix, trace pyrite, good inferred porosity, no shows.

3690-3825m

SANDSTONE: transparent-translucent-occasionally very light grey, loose, coarse to medium grained, dominantly coarse grained, occasionally fine grained, moderately sorted, subangular to subrounded, rare silica cement, no matrix, trace to minor pyrite micronodules, good inferred porosity, no shows, grading to siltstone.

SILTSTONE: medium reddish brown-light brown, firm to moderately hard, dominantly subfissile-occasionally fissile, commonly micromicaceous, very carbonaceous in part, grading to shale and coal in part.

3825-3835m

SANDSTONE: transparent-translucent to occasionally white, loose, coarse to fine grained, dominantly coarse, occasionally medium, fine grained, subangular to subrounded, trace silica cement, trace white calcareous matrix, tr mica, common to abundant pyrite, 50% fluoresence--moderate bright yellow direct, fast streaming yellow cut fluoresence, abundant brown oil staining.

Company : Petrofina Exploration Australia _____

Well : Angler # 1

______ Country : Australia GEOLOGY SUMMARY

SANDSTONE: transparent to milky white, very fine to 3835-3875m medium grained, occasionally very coarse, fractured grains, poorly sorted, trace of white matrix, occasional calcareous to dolomitic cement, common pyrite -occasionally as matrix, mineral flluorescence.

SILTSTONE: speckled brown-reddish-black, firm to 3875-4005m hard, occasionally very hard, subfissile subblocky, argillaceous matrix, micromicaceous in part, carbonaceous--grading to coal in part, pyritic in part; traces of COAL: black, vitreous, hard

> SANDSTONE: transparent to translucent, medium to coarse grained, subangular to subrounded, poorly sorted, trace of calcite cement, fair to poor visible porosity, common pyrite, occasionally showing 10% fluorescence--moderately bright greenish yellow, with slow streaming cut, very thin residual ring.

4005-4205m SILTSTONE: white-brown-lt brown, firm, cemented to earthy, common carbonaceous specks/grading to coal laminations in part, common feldspar grains, arenaceous in part, glauccontic in part, minor biotite with chlorite alteration, common coarse floating quartz grains, very fine mica and pyrite along fractures.

> SANDSTONE: transparent, unconsolidated, fine-med grained, moderately sorted, fractured grains, frosted in part, tr calcite cement, minor pyrite aggregates, poor inferred porosity.

4205-4330m SANDSTONE: translucent-white-very light grey, fine to coarse grained-fining with depth, moderately well sorted--becoming poorly sorted with depth, dominantly subangular to subround, traces of mica, (biotite altering to chlorite), trace of calcite cement, common pyrite, good inferred porosity--decreasing to poor at depth, no show to 20% fluorescence--pale yellow flourescence, slow weak greenish yellow cut, no stain or residual ring.

> SILTSTONE: light grey to medium brown, moderately hard to hard, blocky to subfissile, very arenaceous in part, grades to very fine grained sandstone,

Company : Petrofina Exploration Australia 5.7

Well : Angler # 1

Country : Australia HYDROCARBON SUMMARY

HYDROCARBON SUMMARY

; DEPTH ;	LITHOLGY ;	GAS ;	SHOWS
3490m- 3510m	SILTSTONE	NO GAS	No direct fluor, pr-fr yel cut, med yel residual rng.
3557m- 3579m	SANDSTONE	NO GAS	Tr-10% dul yel/grn,w/-dull ; yel/gold cut,lt brn res ; oil stn.
; 3825m- ; 3845m ;	SANDSTONE #	C1:0.4% C2:.025% C3:Trace.	Mod'bright yel, fast strmg bright yel cut, abdnt brn oil stn.
3985m- 4000m	SANDSTONE W/- THIN COAL SEAMS.	C1:0.1%	Tr-10% mod-bright grn/yel. W/-slow strmg yel cut,thin dull yel res' rng.
4125m- 4260m	SANDSTONE	C1:10.0% C2:0.5% C3:0.17% iC4:0.0072% nC4:0.0089%	
4260m- 4305m	SANDSTONE	C1:0.9% ¦	Tr-10% v. dull yel fluor, w/-wk cut,no residual rng.

[#] Core #1 was taken from 3833m to 3842m with 99.0% recovery. SEE PETROFINA CORE DESCRIPTION FOR HYDROCARBON SHOWS.

Company : Petrofina Exploration Australia										
Well	Angler	Angler # 1								
Country	: Austral	lia	ELECTRIC LOG RECORD							
			· 							
HOLE SIZE	FROM	TO met	ELECTRIC LOGS RUN	COMMENTS						
!		INTERME	DIATE LOGGING RUN -	-						
17.5"	1170	610	DIL-LSS-GR-CAL.							
12.25"	2887	2800	LSS-DLT-GR-CAL.							
	2887	1170	LDT-CNL-GR-CAL.	TOOL STUCK-UP AT 2330m.						
!		- FIN	NAL LOGGING RUN -	:						
8.5"	4333m	2888m	DLT-SLS-MSFL-GR-CAL-SP.							
; ; ;	4336m	2888m	LDL-CNL-NGL.							
i 1 1	3125m	4269m	RFT-HP-GR.							
	4336m	2888m	FMS-GR.							
	4336m	SURF1	VSP.							
t 4 1	4336m	3496m	CST. 60 SHOT	23 RECOVERED						
1 1 1	2888m	SURF'	CBL.							
1	3485m	2906m	CST. 30 SHOT	23 RECOVERED						

Company : Petrofina Exploration Australia 5.9

Well : Angler # 1

Country : Australia RFTs

RFT SUMMARY

Segregated fluid samples collected at 4226met with 2.75gal chamber.

CHAMBER CONTENTS:92.4cu ft of gas & 600cc Condensate.

GAS COMPOSITION; C1:88.24%, C2:5.0%, C3:1.63%, iC4:0.11%, nC4:0.13%.

CONDENSATE:Sg:0.77 @ 21.8 deg.C,52 degrees API.

1 gal pressure sample preserved for PVT ANALYSIS.

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Company : Petrofina Exploration Australia

: Angler # 1 Well

Country : Australia

FORMATION PRESSURE EVALUATION

OVERPRESSURE INTRODUCTION

The following is a brief summary of the methods used whilst drilling to indicate overpressure in geological formations.

"D" EXPONENT: This is a normalised rate of penetration which tries to adjust for variables such as weight on bit, rotation and mud weight. It can be used reliably in shales and clean claystones and as an indicator in siltstones, silty shales and calcareous claystones. A shift from the normal trend (representing a normal compaction) to the left (representing relative undercompaction) indicates overpressure or increased porosity due to lithology changes.

RESISTIVITY: As measured by sensors in the suction pit and flowline and the Teleco MWD tool while drilling. The mud resistivity is used to detect influxes to the mud system whereas the Teleco MWD tool measures formation resistivity which gives an indication of compaction in argillaceous formations. Decreasing formation resistivity results from undercompaction and indicates overpressure.

TEMPERATURE: As measured by the Teleco MWD tool while drilling or as a lagged parameter measured in the mud return system compared with a reference value measured in the active pits. (plotted against depth) shows overpressure by a positive change in the thermal gradient i.e. a shift to the right of a normal trend, due to lower conductivity in undercompacted formations. This is often preceded by a 'thermal shadow indicated by a left ward shift in the trend just above the abnormally pressured zone. Measurement while drilling (Teleco) is more reliable as there is no riser cooling effect with this method.

GAS: Increase in the background and trip gas readings as well as significant connection gas readings (a significant connection gas peak is twice the current background figure.) all indicate increasing pore pressures. Note that changes in porosity caused by changes in formation type can give increases in background and trip gas which are not related to overpressure.

CUTTINGS: Small splintery cuttings indicate overpressured formations. Long propeller shaped cavings are caused by overpressure or by hydration of reactive or swelling clays. This results in overpull and drag on the drill collars and stabilisers while making connections or while tripping.

ELECTRIC LOGS: Resistivity logs as described above. Sonic logs react to a function of rock density and as such react in a very similar way to the D exponent shifting to the left of a normal compaction trend. RFT logs measure the formation pressure at selected depths. These logs can be used only as a confirmation of overpressure after the well has been drilled.

O Detaction Franchism Australia

Company : Petrofina Exploration Australia 6.2

Well : Angler # 1

Country : Australia FORMATION PRESSURE EVALUATION

SUMMARY

Overpressure indicators were monitored throughout the drilling of Angler #1. In the top hole section before the setting of the 20" casing at 603m only the "d" exponent was available. Once the riser was run returns were maintained for the rest of the drilling, enabling gas levels, mud volumes, cuttings, temperature and resistivity to be monitored. A Teleco MWD tool was run from the 9 5/8" casing shoe at 2888m enabling the measurement of down hole tool temperature and formation resistivity. At TD, at 4330m, RFTs were run by Schlumberger and formation pressure measured at 36 depths in the 8 1/2" section.

The formations drilled, including the target zones, were expected to be normally pressured from correlations with other wells in the vicinity. This was found to be the case, the maximum pressure gradient calculated from the RFTs being 1.065 sg.

The "d" exponent was of little value in calculating formation pressure in this well as there was only one relatively thin claystone formation. In argillaceous formations with uniform composition and calcimetry the "d" exponent generally increased with a constant gradient. The only leftward trend of any significance was in the marks from 2100m to 2500m but this was attributed to decreasing calcite content over the interval. The major or sudden changes in "d" exponent were caused by formation changes and changes in bit type, from tricone to PDC. As such it was useful in picking formation and bedding tops and comparing drillability. At no stage did the "d" exponent indicate overpressure.

The mud resistivity, measured as conductivity, showed no influxes of formation fluids to the mud system and therefore a balanced or overbalanced system. The Teleco MWD formation resistivity was constrained by the same formation factors as the "d" exponent, but gave no indication of overpressure.

As temperature trends also depend on formation porosity, in that formation fluids are less conductive than rock, they gave no indication of overpressure in the interbedded formations of this well.

Gas readings were useful overpressure indicators while drilling as there was background gas for much of the well. Any formation pressures approaching the hydrostatic pressure of the mud would have been obvious from the presence of connection gas and high trip gas values. As these were not present we were confident of sufficiently overbalanced mud while drilling gas bearing formations.

There were no splintery cuttings observed in this well.

Mud pit levels showed some mud losses in porous formations but never any gains, once again indicating an overbalanced system.

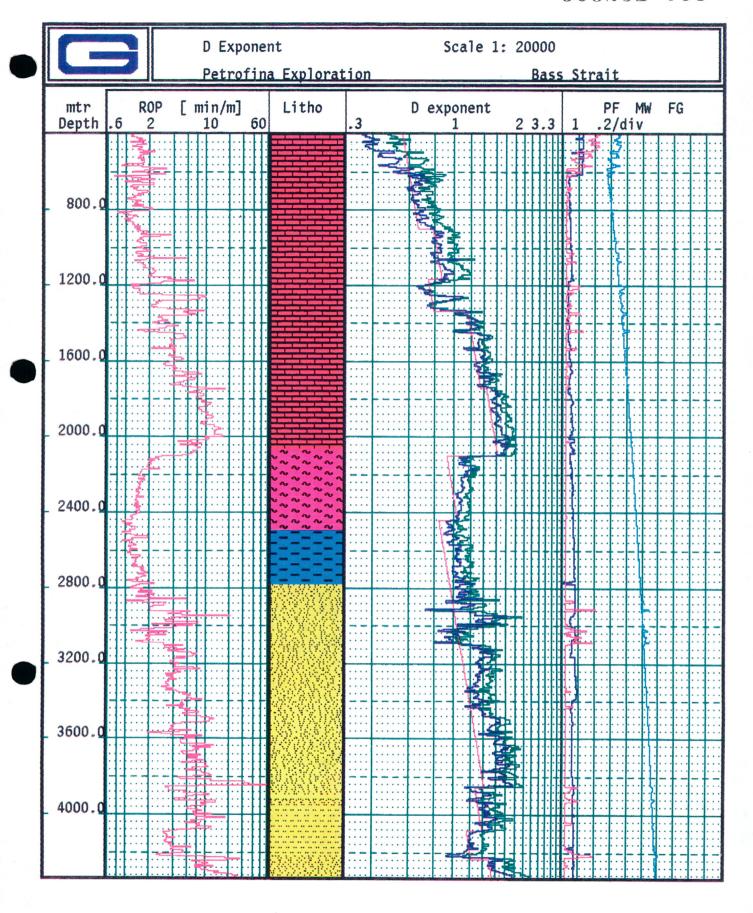
Electric logs, resistivity and sonic, are related to porosity and therefore were of limited use for overpressure detection. The RFT logs gave the actual formation pressure and, as a function of depth, the formation pressure gradient. This reached a maximum of 0.462 psi/ft or 1.065 sg EMW at 4220m RKB and was 0.439 psi/ft (1.014 sg EMW) in the Selene sandstones of the target formation.

Company: Petrofina Exploration Australia 6.3

Country: Australia FORMATION PRESSURE EVALUATION

CONCLUSIONS

There was no indication of overpressure in Angler #1 during the drilling and this was supported by electric logs run after reaching TD. The maximum pressure gradient encountered was 0.0462 psi/ft which equals an equivalent mud weight of 1.065 sg. In the interbedded non-argillaceous formations of varying porosity, and calcite and sand content, many of the calculated and sophisticated methods of overpressure detection were of less value than the classic ones such as gas readings, mud pit levels and mud resistivity changes.



Company : Petrofina Exploration Australia 7.1

Well : Angler # 1

Country : Australia GAS EVALUATION

SUMMARY

Background gas levels monitored during the drilling of Angler #1 were low, averaging between 0 and 1% for most of the well. Levels measured through the Gippsland Limestone section ranged between 0 and 1%, averaging about .7%, with a mud weight of 1.17 s.g. The background level declined somewhat after drilling the 13-3/8" casing shoe, to a depth of 1390m. At that point, the mud weight was reduced to 1.04 s.g. and the gas level resumed as before. No connection gasses or significant shows occurred through the Gippsland Limestone interval. The gas level through the Lakes Entrance Formation was essentially the same, ranging between 0 and 1%, averaging about .8%, with a mud weight of 1.08 s.g. No connection gasses or significant shows occurred during the drilling of the Lakes Entrance section. Upon entering the sandstones at the top of the Latrobe Group, the background level dropped, averaging about 0.4% to the bottom of the 12 1/4" hole at 2918m.

The mud weight was raised to 1.11 subsequent to the drilling out of the 9-5/8" casing shoe. As a result, no background gas level was measurable to a depth of 3173m. At 3173m and below, small gas shows emanated from an interbedded sandstone/siltstone/coal sequence. The most significant shows came from a carbonaceous siltstone interval from 3212m to 3245m. The maximum peak gas was 2.5% at 3235m, with 1.8% C1, 0.4% C2, 0.2% C3, 0.01% iC4, and 0.02% nC4. Below this zone, background gas dropped to zero with a mud weight of 1.12, and continued to be absent until a depth of 3810m. Background gas resumed at this depth from a sandstone/carbonaceous siltstone sequence and continued to T.D. Levels ranged between .06 and 1%, averaging about occasionally measured in this interval, with gas shows occurring from interbedded sandstones and siltstones from 4205m to 4233m. The maximum peak gas level of 11% was recorded at 4215m, with 10% C1, 0.71% C2, 0.27% C3, 0.012% iC4 and 0.018% nC4.

After a depth of 4235m was reached, the background gas returned to a level of about .8%, until 4290m, where it dropped to a level of 0.06% through a siltstone section to T.D. at 4330m.

Company: Petrofina Exploration Australia 7.2

Well : Angler # 1

Country : Australia GAS EVALUATION

GAS SUMMARY TABLE

DEPTH mt	GAS LEVELS %										
from: to	Background	Max peak	Trip gas Conn gas	!							
613 - 1150	.0011.0	1.2 @ 1020m		.							
1150 - 1390	.00102	.28 @ 1313m	1.1 @ 1335m	; ; ;							
1390 - 2010	.02 - 0.2	0.6 @ 1727m	0.7 @ 1792m	; ; ;							
	,		0.8 @ 1995m	† 							
2010 - 2812	.01 - 1.0	1.1 @ 2272m	0.8 @ 2100m	1 1 3							
2812 - 2930	.02 - 0.18	0.4 @ 2812m	.03 @ 2918m	1 1 1							
2930 - 3172	0 - 0		0 @ 2978m	! ! !							
3172 - 3253	0 - 2.2	2.2 @ 3235m	1.1 @ 3227m	1 4 5 1							
3253 - 3810	0 - 0	i i i	0 @ 3507m	1							
3810 - 4205	.04 - 1.0	1.0 @ 4165m	0.3 @ 4040m	1 1 1							
4205 - 4330	0.1 - 11.0	11.0 @ 4215m	0.7 @ 4238	;							

______ Company : Petrofina Exploration Australia ______

Angler # 1 ______

Country : Australia

GAS EVALUATION

GAS COMPOSITION DIAGRAMS

A brief explanation on the usage of gas composition diagrams;

The gas composition diagram allows the determination of two important points: 1) Whether the sample originates from a dry gas

reservoir, or from an oil accumulation.

2) Whether the composition of the sample is geochemically normal, or abnormal and hence originating from dissolved in water.

- 1.1) If the point of the triangle is:
 - i) UPWARD-then the sample originates from a gas reservoir.
 - ii) DOWNWARD-then the sample indicates an accumulation of oil.
- 2.1) The homothetic centre must fall within the delimited area, if not the composition of the sample is abnormal, as described above.

ANALYSIS OF GAS COMPOSITION DIAGRAMS: (Refer to gas composition

DEPTH: 3830m(Immediately before core point at 3833m).

- Sample originates from a non-productive oil 1) accumulation.
- Sample geochemically abnormal. 2)

DEPTH: 4215m(Lower Campanian Sandstone)

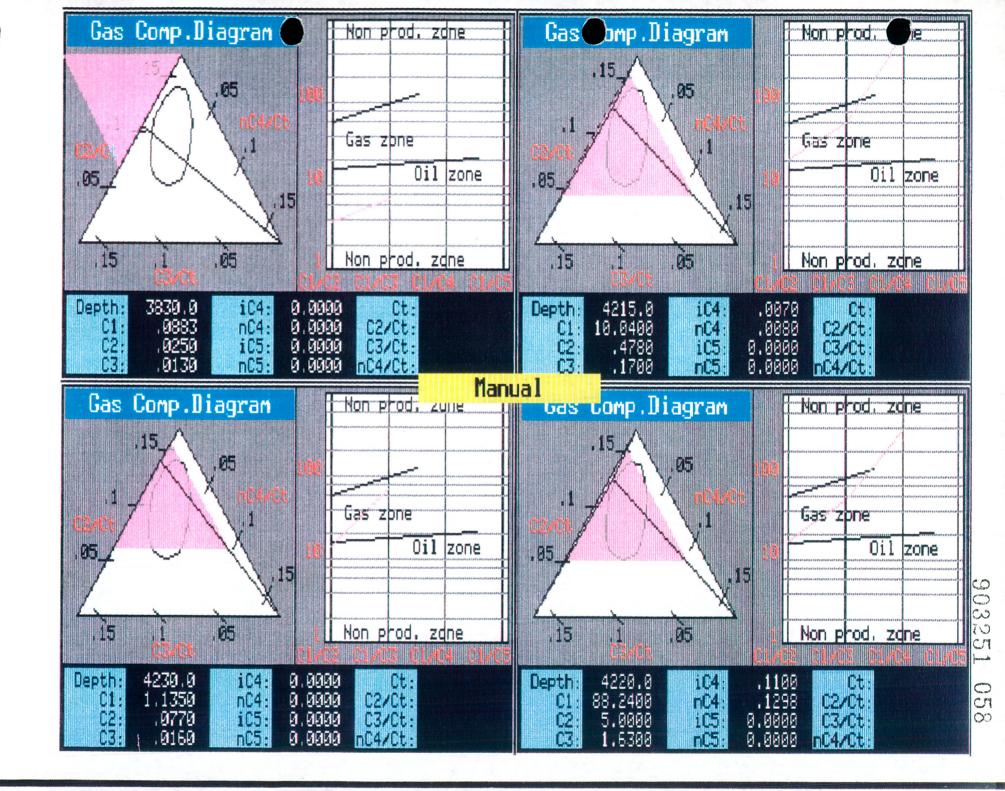
- Sample originates from a gas zone.
- Sample geochemically abnormal. 2)

DEPTH: 4220m(RFT gas chamber sample over Lower Campanian Sst).

- 1) Sample originates from a gas zone.
- Sample geochemically normal. 2)

DEPTH: 4230m(Lower Campanian Sandstone)

- Sample originates from a gas zone. 1)
- Sample geochemically normal. 2)



PE606683

This is an enclosure indicator page.

The enclosure PE606683 is enclosed within the container PE903251 at this location in this document.

```
The enclosure PE606683 has the following characteristics:
    ITEM_BARCODE = PE606683
CONTAINER_BARCODE = PE903251
            NAME = Angler-1 Chromatolog
            BASIN = GIPPSLAND
        ONSHORE? = N
        DATA_TYPE = WELL
   DATA_SUB_TYPE = WELL_LOG
     DESCRIPTION = Angler-1 Chromatolog, Scale 1:1000,
                    VIC/P20, W993. By Geoservices for
                    Petrofina Exploration Australia S.A.
                    (13 pages). Chromatolog to accompany
                    "Angler-1 Final Well Report"
                    (PE903251).
          REMARKS =
     DATE_WRITTEN =
   DATE_PROCESSED =
    DATE_RECEIVED =
    RECEIVED_FROM = Petrofina Exploration Australia S.A.
        WELL_NAME = Angler-1
       CONTRACTOR = Petrofina Exploration Australia S.A.
           AUTHOR =
       ORIGINATOR = Petrofina Exploration Australia S.A.
        TOP_DEPTH = 510
     BOTTOM_DEPTH = 4310
   ROW_CREATED_BY = EC00_SW
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(Inserted by DNRE - Vic Govt Mines Dept)

Company : Petrofina Exploration Australia 8.1
Well : Angler # 1
Country : Australia DEVIATION REPORT

SUMMARY

Angler # 1 was drilled as a vertical exploration well. The highest deviation recorded was at 2927m with a drift of 4.6 deg. However, in general insignificant deviations and doglegs were generated during drilling.

The bottom hole assemblies employed while drilling Angler #1 can be broadly categorised as rigid assemblies from 300m to 2900m, and bendulum assemblies from 2900m to total depth at 4330m.

From 304m to 2050m a persistent calcarenite formation drilled with a negligible drift range of 0.1 to 0.8 deg. Thereafter a marl/claystone formation initiated a systematic increase in drift from 0.9 deg at 2371m to 3.6 deg at 2896m; the last survey taken prior to setting the 9 5/8" casing shoe at 2888m. Once out of the shoe the angle continued to increase though precautions such as drilling with a reduced wob and quicker rotary were taken. At 2927m a dogleg of 7.29 deg/100m had been created. With the aid on a pendulum assembly the deviation was once again reduced gradually to 1.0deg at 3770m. Thereafter the deviation was restricted to 3.0deg without restricting the penetration rate.

The displacement of the hole from the vertical at TD was 29.0m to the north and 35.2m to the west or 47.5m at 333 deg from north.

The displacement of the hole from the vertical at the primary target (Selene Sandstone) was 4.2m to the north and 29.9m to the west or 32.7m at 278.9 deg from north at 3238.2m.

ANGLER #1					TELEC)			
			##	Vrtel	Coordinates		Dog lg		
	Depth	Drift	Bearing##	Depth	N / W	S / K	Departure	0/100m	No
	304.7	0.00	0.0 ##	304.7	0.0 N			0.00	1
		0.30					0.80	0.10	2
	638.6	0.50					0.96	1.40	3
	668.3	0.20					1.03	1.13	4
	698.4	0.30					1.12	0.90	5
	722.3	0.20					1.22	0.52	6
	768.6	0.30					1.31	0.75	7
	824.8	0.30			0.7 N		1.22	0.19	8
	868.0	0.30						1.29	9
	916.1	0.10					·	0.82	10
	961.2	0.30						0.86	11
	1009.0	0.10						0.79	12
	1064.6	0.20						0.51	13
	1099.6	0.20						0.63	14
	1136.3	0.10			0.7 N	1.5 B		0.35	15
	1185.5	0.30		1185.5	0.7 N		1.77	0.63	16
	1213.4	0.30		1213.4	0.8 N			0.19	17
	1241.9	0.40	44.1 ##	1241.9	0.9 N			0.44	18
	1270.4	0.50	45.9 ##	1270.4	1.1 N ·		2.29	0.34	19
	1298.0	0.30	44.5 ##	1298.0	1.2 N		2.48	0.72	20
	1502.6	0.60	50.8 ##	1502.6	2.3 ₦	3.4 E	4.05	0.15	21
	1712.5	0.50	45.9 ##	1712.5	3.6 N	4.9 B	6.06	0.05	22
	1743.4	0.50	43.1 ##	1743.4	3.8 N	5.1 E	6.32	0.00	23
	1787.6	0.40	33.6 ##	1787.6	4.1 N	5.3 E	6.66	0.28	24
	1825.5	0.50	35.0 ##	1825.5	4.3 N		6.94	0.26	25
	1873.5	0.30		1873.5	4.6 N	5.6 E	7.27	0.43	26
	2071.1	0.10		2071.1	4.3 N	6.3 E	7.58	0.20	27
	2101.7	0.30			4.2 N	6.2 E	7.49	0.69	28
	2138.1	0.40			4.0 N	6.1 E	7.31	0.38	29
	2193.5	0.50			3.6 N		6.92	0.47	30
		0.70				5.3 E	6.15	0.27	31
	2325.2	0.80			2.6 N		5.41	0.43	32
	2371.6	0.90			2.4 N	4.1 E	4.73	0.49	33
	2427.4	1.00			2.0 N	3.2 E	3.82	0.64	34
	2484.8	1.00			1.5 N	2.4 E	2.82	0.24	35
	2543.7	1.10			1.3 N	1.3 E	1.83	0.73	36
	2605.7	1.70			1.2 N	0.2 W	1.21	0.97	37
	2641.0	1.70			1.1 N	1.3 ₩	1.70	0.29	38
	2660.6	1.90			1.2 N	1.9 ₩	2.20	1.23	39
	2680.0	1.80			1.2 N	2.5 W	2.77	0.53	40
	2709.3	2.20			1.3 N	3.5 W	3.75	1.64	41
	2718.3	2.30			1.4 N	3.8 W	4.10	1.42	42
	2746.0	2.30			1.7 N	4.9 W	5.21	0.00	43
	2776.1	2.50			1.8 N	6.2 W	6.44	2.25	44
	2801.8	2.50			1.9 N	7.3 ₩	7.54	1.67	45
	2830.9	3.00			2.2 N	8.7 W	8.94	2.68	46
	2857.6	3.30			2.8 N	10.0 W	10.39	1.30	47
	2896.0	3.60			3.6 N	12.2 W	12.70	1.72	48
	2920.6	4.30	280.0 ##	2920.2	3.9 N	13.8 W	14.39	3.09	49

TELECO

		 ##	Vrtcl	Coordinates		Dog lg		
Depth	Drift	Bearing##	Depth	- N / W	S/K	Departure	o/100m	No
2927.8				4.0 N	14.4 W	14.94	7.59	50
2949.1	4.40	272.7 ##	2948.6	4.1 N	16.1 W	16.58	1.07	51
2958.3	4.20	272.7 ##		4.1 N	16.8 W	17.26	2.17	52
2976.4	4.30	275.1 ##	2975.8	4.2 N	18.1 W	18.58	1.12	53
2984.4	4.30	274.4 ##	2983.8	4.3 N	18.7 W	19.17	0.70	54
3002.0	4.00				20.0 W	20.43	2.34	55
3011.4	3.90	272.3 ##	3010.7	4.3 N	20.6 W	21.06	1.68	56
3030.6	3.50	270.9 ##	3029.9	4.4 N	21.9 W	22.28	2.14	57
3067.1	3.30	271.6 ##	3066.3	4.4 N	24.0 W	24.42	0.56	58
3095.8	2.60	271.2 ##	3095.0	4.4 N	25.5 ₩	25.88	2.44	59
3134.0	2.70	263.9 ##	3133.1	4.4 N	27.3 ₩	27.60	0.92	60
3152.6	1.80			4.3 N	28.0 W	28.31	4.86	61
3183.1	1.00	269.1 ##	3182.2	4.2 N	28.7 W	29.03	2.68	62
3209.6	1.50	267.7 ##	3208.7	4.2 N	29.3 W	29.60	1.89	63
3238.2	1.10	278.3 ##	3237.3	4.2 N	29.9 W	30.25	1.62	64
3266.5	1.00	285.0 ##	3265.6	4.3 N	30.5 W	30.77	0.55	65
3295.3	0.90	282.5 ##	3294.4	4.5 N	30.9 W		0.37	66
3323.7	1.20	284.3 ##	3322.8	4.6 N	31.4 W	31.76	1.06	67
3350.9	1.40	280.0	3350.0	4.7 N	32.0 W	32.38	0.82	68
3380.4	1.40	287.8 ##	3379.5	4.9 N	32.7 W	, 33.09	0.65	69
3409.1	1.60	282.5 ##	3408.2	5.1 N		33.84	0.85	70
3435.6	1.70	276.2	3434.6	5.2 N	34.2 W	34.60	0.78	71
3464.4	1.30	273.0 ##	3463.4	5.3 N	35.0 N	35.35	1.42	72
3491.8	1.10	274.4 ##	3490.8	5.3 N	35.5 W	35.93	0.73	73
3515.5	0.90	285.7	3514.5	5.4 N	35.9 W	36.34	1.18	74
3554.8	0.80				36.5 W	36.91	0.54	75
3600.7	1.10		3599.7	6.0 N	37.1 W	37.59	0.80	76
3638.9	0.70		3637.9	6.5 N	37.5 W	38.03	1.39	77
3677.9	0.80		3676.9	6.9 N	37.8 W	38.38	0.59	78
3720.4	0.80		3719.4	7.4 N	38.1 W	38.84	0.17	79
3770.5	1.00		3769.5	8.1 N	38.5 W	39.35	0.62	80
3826.0	1.50		3825.0	9.2 N	39.0 W	40.06	0.91	81
3860.6	1.60		3859.6	10.0 N	39.4 W	40.68	0.52	82
3897.5	1.70			11.0 N	39.9 W	41.37	. 0.81	
3974.7	1.90			13.4 N	40.4 W	42.51	0.84	84
4024.9	2.10		4023.8	15.1 N	40.3 W	43.07	0.47	85
4069.0	2.10		4067.9	16.7 N	40.3 W	43.59	0.10	86
4135.6	2.80		4134.4	19.5 N	39.7 W	44.26	1.38	87
4178.7	3.30		4177.4		38.9 W	44.53	1.37	88 eo
4204.3	3.40		4203.0	23.0 N	38.3 W	44.65	0.91	89 00
4223.6	3.20		4222.3	24.0 N	37.8 W	44.78	1.71	90 01
4232.0	3.10		4250.6	25.4 N	37.1 W	44.98	1.40	91
4281.3	3.10		4279.9	26.8 N	36.4 W	45.19	0.70	92 93
4308.1	2.80		4306.6	28.1 N	35.8 W	45.44	1.16	
4330.0	2.80	27.3	4 328.5	29.0 N	35.3 ₩	45.65	0.00	94

903251 065

PE606684

This is an enclosure indicator page.

The enclosure PE606684 is enclosed within the container PE903251 at this location in this document.

```
The enclosure PE606684 has the following characteristics:
    ITEM_BARCODE = PE606684
CONTAINER_BARCODE = PE903251
            NAME = Angler-1 Masterlog Geological
                   Evaluation
           BASIN = GIPPSLAND
        ONSHORE? = N
       DATA_TYPE = WELL
   DATA_SUB_TYPE = WELL_LOG
     DESCRIPTION = Angler-1 Masterlog Geological
                    Evaluation, VIC/P20, W933, Scale 1:500,
                    By Geoservices For Petrofina
                    Exploration Australia S.A. (29 pages).
                    To accompany "Angler-1 Final Well
                    Report" (PE903251).
          REMARKS =
    DATE_WRITTEN = 13-MAY-1989
  DATE_PROCESSED =
   DATE_RECEIVED =
   RECEIVED_FROM = Petrofina Exploration Australia S.A.
       WELL_NAME = Angler-1
       CONTRACTOR = Petrofina Exploration Australia S.A.
           AUTHOR =
       ORIGINATOR = Petrofina Exploration Australia S.A.
        TOP_DEPTH = 0
     BOTTOM_DEPTH = 4355
   ROW_CREATED_BY = EC00_SW
```

(Inserted by DNRE - Vic Govt Mines Dept)

PE606685

This is an enclosure indicator page.

The enclosure PE606685 is enclosed within the container PE903251 at this location in this document.

The enclosure PE606685 has the following characteristics: ITEM_BARCODE = PE606685 CONTAINER_BARCODE = PE903251 NAME = Angler-1 Computer Generated Log BASIN = GIPPSLAND ONSHORE? = NDATA_TYPE = WELL DATA_SUB_TYPE = WELL_LOG DESCRIPTION = Angler-1 Computer Generated Log, VIC/P20, W933, By Geoservices/Teleco for Petrofina Exploration Australia S.A., (9 pages). To accompany "Angler-1 Final Well Report" (PE903251). REMARKS = DATE_WRITTEN = 18-MAY-1989 DATE_PROCESSED = DATE_RECEIVED = RECEIVED_FROM = Petrofina Exploration Australia S.A. WELL_NAME = Angler-1 CONTRACTOR = Petrofina Exploration Australia S.A. AUTHOR = ORIGINATOR = Petrofina Exploration Australia S.A. $TOP_DEPTH = 2975$ $BOTTOM_DEPTH = 4325$ ROW_CREATED_BY = EC00_SW

(Inserted by DNRE - Vic Govt Mines Dept)