

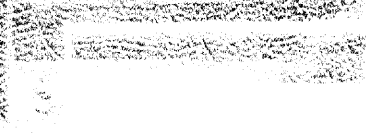
W 963. TARRICA-1. SENS CAL + SYD SENSING CENTER



ATTACHMENT TO W 963

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**SYDNEY LOG
INTERPRETATION
CENTER**



Schlumberger

17 AUG 1987

PETROLEUM DIVISION

LASMO ENERGY AUSTRALIA
WELL SEISMIC PROCESSING REPORT

PATRICIA - 1

FIELD : PATRICIA
STATE : VICTORIA
LOCATION : BASS STRAIT
COUNTRY : AUSTRALIA
COORDINATES : 038° 01' 53.23" S
148° 26' 46.82" E
DATE OF SURVEY : 03-JULY-1987
REFERENCE NO. : 570705/570706

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1.0 INTRODUCTION

A vertical seismic profile was shot in the Patricia - 1 well on 3 July 1987. Data was acquired using an airgun source. Thirty two levels were shot from 445 to 895 metres. The shot data has been used to calibrate the sonic log. A synthetic seismogram was computed.

The major aims of VSP processing are :

- to obtain a high resolution time-depth curve. As the levels are separated by an average of 7 milliseconds, accurate velocity analysis can be made.
- to obtain a better tie between the VSP and Seismic. The lateral depth of investigation of a VSP is intermediate between surface seismic and logs
- to determine the multiple content of the area by analysis of the downgoing wavetrains.
- Further analysis of the downgoing wavetrain provides information on the earth filtering of the seismic wave versus depth.

2.0 DATA ACQUISITION

Table 1 Field Equipment and Survey Parameters

| | |
|-----------------------------|---|
| Elevation SRD | 0.0 metres AMSL |
| Elevation KB | 22.0 metres AMSL |
| Elevation DF | 21.7 metres AMSL |
| Elevation GL | -51.0 metres AMSL |
| Total Depth | 900 metres below KB |
| | |
| No. of Levels | 32 |
| Energy Source | Airgun |
| Source Offset | 50 metres |
| Source Azimuth | 245° |
| Source Depth | 5.0 metres below MSL |
| Reference Sensor | Hydrophone |
| Sensor Offset | 50 metres |
| Sensor Azimuth | 245° |
| Sensor Depth | 10.0 metres below MSL |
| | |
| Downhole Triaxial Geophones | 3 orthogonally opposed, not gimballed Sensor SM-4 (one/axis) Temperature 350° F Low cut filter 2 Hz @6 db/oct High cut filter 330 Hz @30 db/oct Natural Freq. 10 hertz Sensitivity 0.83 V/cm/sec per axis |

Recording was made on the Schlumberger Cyber Service Unit (CSU) using LIS format. The survey was shot using a airgun source and hydrophone as the surface sensor.

3.0 SONIC CALIBRATION

A 'drift' curve is obtained using the sonic log and the vertical check level times. The term 'drift' is defined as the seismic time (from check shots) minus the sonic time (from integration of edited sonic). Commonly the word 'drift' is used to identify the above difference, or to identify the gradient of drift verses increasing depth, or to identify a difference of drift between two levels.

The gradient of drift, that is the slope of the drift curve, can be negative or positive.

For a negative drift $\frac{\Delta drift}{\Delta depth} < 0$, the sonic time is greater than the seismic time over a certain section of the log.

For a positive drift $\frac{\Delta drift}{\Delta depth} > 0$, the sonic time is less than the seismic time over a certain section of the log.

The drift curve, between two levels, is then an indication of the error on the integrated sonic or an indication of the amount of correction required on the sonic to have the TTI of the corrected sonic match the check shot times.

Two methods of correction to the sonic log are used.

1. **Uniform or block shift** This method applies a uniform correction to all the sonic values over the interval. This uniform correction is applied in the case of positive drift and is the average correction represented by the drift curve gradient expressed in $\mu\text{sec}/\text{m}$.
2. **ΔT Minimum** In the case of negative drift a second method is used, called Δt minimum. This applies a differential correction to the sonic log, where it is assumed that the greatest amount of transit time error is caused by the lower velocity sections of the log. Over a given interval the method will correct only Δt values which are higher than a threshold, the Δt_{min} . Values of Δt which are lower than the threshold are not corrected. The correction is a reduction of the excess of Δt over Δt_{min} , $\Delta t - \Delta t_{min}$.

$\Delta t - \Delta t_{min}$ is reduced through multiplication by a reduction coefficient which remains constant over the interval. This reduction coefficient, named G , can be defined as:

$$G = 1 + \frac{\text{drift}}{\int (\Delta t - \Delta t_{min}) dZ}$$

Where drift is the drift over the interval to be corrected and the value $\int (\Delta t - \Delta t_{min}) dZ$ is the time difference between the integrals of the two curves Δt and Δt_{min} , only over the intervals where $\Delta t > \Delta t_{min}$.

Hence the corrected sonic: $\Delta t = G(\Delta t - \Delta t_{min}) + \Delta t_{min}$.

4.0 SONIC CALIBRATION PROCESSING

4.1 Open Hole Logs

The sonic and density logs have been edited prior to input into the Well Seismic Calibration processing chain.

The sonic amplitude is very low in the gas zone (700 to 750 metres below KB) and ΔT is subject to cycle skip. The shortest transmitter-receiver pair (8 ft) is least affected by attenuation and the sonic log has been reconstructed over this interval by following the trend in the 8 ft transit time curve.

The density log has been patched across from 655 to 643 metres where the density is affected by poor hole conditions. A constant density of 2.1 gm/cc is assumed from the surface to the top of recording at 605 metres.

4.2 Correction to Datum and Velocity Modelling

A pseudo shot has been placed on the sea floor assuming a water velocity of 1480 metres/sec. Seismic datum is at mean sea level. All shots have been corrected to MSL.

4.3 Sonic Calibration Results

The top of the sonic log (220 metres below KB) is chosen as the origin for the calibration drift curve. The drift curve indicates a number of corrections to be made to the sonic log.

Table 3 Sonic Drift

| Depth Interval (metres below KB) | Block Shift $\mu\text{sec/m}$ | Δt_{min} $\mu\text{sec/m}$ | Equip Block Shift $\mu\text{sec/m}$ |
|--------------------------------------|----------------------------------|---------------------------------------|--|
| 220.0 - 509.5 | 13.82 | - | 13.82 |
| 509.5 - 643.5 | 37.31 | - | 37.31 |
| 643.5 - 702.0 | 17.09 | - | 17.09 |
| 702.0 - 750.5 | 6.19 | - | 6.19 |
| 750.5 - 900.0 | 10.03 | - | 10.03 |

The adjusted sonic curve is considered to be the best result using the available data.

5.0 GEOGRAM PROCESSING

GEOGRAM plots were generated using 40, 50 and 60 hertz zero phase ricker wavelets. The presentations include both normal and reverse polarity on a time scale of 20 cm/sec.

GEOGRAM processing produces synthetic seismic traces based on reflection coefficients generated from sonic and density measurements in the well-bore. The steps in the processing chain are the following:

- Depth to time conversion
- Reflection coefficients
- Attenuation coefficients
- Convolution
- Output.

5.1 Depth to Time Conversion

Open hole logs are recorded from the bottom to top with a depth index. This data is converted to a two-way time index and flipped to read from the top to bottom in order to match the seismic section.

5.2 Primary Reflection Coefficients

Sonic and density data are averaged over chosen time intervals (normally 2 or 4 milliseconds). Reflection coefficients are then computed using:

$$R = \frac{\rho_2 \cdot \nu_2 - \rho_1 \cdot \nu_1}{\rho_2 \cdot \nu_2 + \rho_1 \cdot \nu_1}$$

where

- ρ_1 = density of the layer above the reflection interface
- ρ_2 = density of the layer below the reflection interface
- ν_1 = compressional wave velocity of the layer above the reflection interface
- ν_2 = compressional wave velocity of the layer below the reflection interface

This computation is done for each time interval to generate a set of primary reflection coefficients without transmission losses.

5.3 Primaries with Transmission Loss

Transmission loss on two-way attenuation coefficients are computed using:

$$A_n = (1 - R_1^2).(1 - R_2^2).(1 - R_3^2)...(1 - R_n^2)$$

A set of primary reflection coefficients with transmission loss is generated using:

$$Primary_n = R_n.A_{n-1}$$

5.4 Primaries plus Multiples

Multiples are computed from these input reflection coefficients using the transform technique from the top of the well to obtain the impulse response of the earth. The transform outputs primaries plus multiples.

5.5 Multiples Only

By subtracting previously calculated primaries from the above result we obtain multiples only.

5.6 Wavelet

A theoretical wavelet is chosen to use for convolution with the reflection coefficients previously generated. Choices available include:

- Klauder wavelet
- Ricker zero phase wavelet
- Ricker minimum phase wavelet
- Butterworth wavelet
- User defined wavelet.

Time variant butterworth filtering can be applied after convolution.

5.7 Polarity Convention

An increase in acoustic impedance gives a positive reflection coefficient and is displayed as a white trough under normal polarity. Polarity conventions are displayed in Figure 1.

5.8 Convolution

Standard procedure of convolution of wavelet with reflection coefficients. The output is the synthetic seismogram.

6.0 VSP PROCESSING

6.1 PROCESSING SEQUENCE

1. STACKING

A median stack was performed on the vertical and horizontal component data (Plot 1) of all the good shots at each level using the surface sensor break times as the zero time for stacking. The transit time is computed after stacking, which is now the transit time from surface sensor to geophone.

2. SPHERICAL DIVERGANCE CORRECTION and BANDPASS FILTER

A bandpass filter of 5-125 hertz bandwidth was applied. A time varying gain function of the exponential form :

$$GAIN(T) = \left(\frac{T}{T_0}\right)^\alpha$$

where T is the recorded time and T_0 is the first break time and $\alpha = 1.2$

Trace equalisation was applied by normalising the RMS amplitude of the first break to correct for transmission losses of the direct wave. A normalisation window of 50 milliseconds was used. A static correction varying from +5.2 to +6.1 msec has been applied to reference the data to mean sea level, correct for gun to hydrophone distance and correct for source offset. Data after this stage is displayed at Plot 2.

3. VELOCITY FILTER

The downgoing coherent energy is estimated using a seven level median velocity filter. The filter array is moved down one level after each computation and the process is repeated level by level over the entire dataset. As a result, the deepest and shallowest levels are lost because of edge effects.

The residual wavefield is obtained by subtracting the downgoing coherent energy from the total wavefield. Finally, a five level median filter is applied on the residual wavefield to enhance the upgoing compressional wavefield. The downgoing and residual wavefields are displayed at Plot 3.

4. PREDICTIVE DECONVOLUTION

At this stage, the assumption is made that the downgoing energy at a given level is convolved with the earth reflectivity sequence below that level. The deconvolution operator is designed on the downgoing trace, the operator is applied to both the downgoing and upgoing traces at the same level.

The result of predictive deconvolution on the residual wavefield is shown in plot 4. An operator of 1000 msec length and prediction distance equal to the 2nd zero crossing was computed. The deconvolution is applied before any coherency enhancement in order to collapse the multiple sequence of shear arrivals, diffractions or out of plane reflections. A five level median filter is applied to the residual wavefield after predictive deconvolution to enhance the reflected compressional events.

5. WAVESHAPING DECONVOLUTION

Plot 6 shows the data after the application of waveshaping deconvolution. The deconvolution operator is a two sided operator and is designed trace by trace by opening a 520 msec window starting 20 msec before the first break on the downgoing wave train. The desired output wavelet was chosen to be zero phase with a band width of 10-80 hertz. The operator is applied to the downgoing and subtracted wavefield at the same level. The upgoing compressional wavefield are enhanced as before.

6. CORRIDOR STACK

A corridor stack is computed on the data after deconvolution by summing the data in a 100 millisecc window from the first break. All the data from the bottom four levels have been included to provide continuity of the corridor stack data down to 3.0 seconds.

The enhanced upgoing and corridor stack after predictive deconvolution are displayed at plot 5, the enhanced upgoing and corridor stack after waveshaping deconvolution are displayed at plot 7.

7. ACOUSTIC IMPEDANCE INVERSION

The zero phase waveshaping should permit a better interpretation of acoustic contrast, hence the data used for the inversion has been taken from the VSP after zero phase waveshaping deconvolution. The traces chosen for the inversion were the corridor stack.

The inversion technique is one which produces a limited number of reflection coefficients and varies these to minimise the error energy between the observed seismogram and the synthetic seismogram, whilst satisfying any constraints that may be imposed. This approach yields a blocky impedance profile.

An initial impedance of 15509 taken from the logged impedance was used. No constraints are applied to the inverted impedance.

The quality of the inversion procedure on the data can be assessed by the similarity in the observed trace and synthetic trace (the synthetic trace is obtained by convolving the zero phase downgoing wavelet with reflectivity series derived from the inversion procedure).

The inversion is displayed alongside the VSP data after zero phase waveshaping deconvolution at plot 8. The similarity between the corridor stack and the synthetic seismogram from the inversion process is very good. Equally the comparison between the inverted impedance and the logged impedance is good, with the inverted impedance reflecting acoustic boundaries from rather subtle lithological changes. This is especially evident within the reservoir zone where the small increases in impedance probably reflect tighter sands.

8. VELOCITY ANALYSIS

The shear and compressional interval velocities were computed with respect to their transmitted arrivals on both the vertical component and horizontal component (see plot 9). A log like response of the V_P/V_S ratios and poissons ratio was computed from these components. There is a very good correlation between the V_P and the the sonic log. The gas zone can be identified as the low section in the poisson's ratio curve. The shear velocities can be used to compute the rock properties of the sand reservoir.

9. HORIZONTAL COMPONENT PROCESSING

The maximum horizontal energy was obtained by opening a narrow time window about the first arrival and applying a rotation in the direction of maximum energy. This is computed for each geophone position.

Plot 10 displays the horizontal components projected on the downgoing shear wavefield. Plot 11 displays the horizontal components projected on the downgoing compressional wavefield.

A bandpass filter of 5-50 hertz bandwidth was applied and the result is displayed on the two upper panels.

10. SHEAR WAVE PROCESSING

The maximum horizontal energy projected on the downgoing shear wavefield is processed to yeild the upgoing shear wavefield (see plot 12). The processing sequence is similar to the Z-axis processing.

- Amplitude recovery 1.22, Bandpass filter 5-50 hertz and normalisation in 400 millisecc window from compressional first break.
- Seven level median estimate of downgoing shear
- Residual wavefield
- Five level enhancement of upgoing shear
- Convert to shear two way time

The impedance change at the base of the sandstone can be identified the black peak at 1550 msec on the lower panel of Plot 12. No deconvolution has been applied to the horizontal component processing.

An inspection of the residual wavefield reveals several alignments of upgoing data. These can be enhanced as upgoing shear and upgoing compressional (see Plot 13). The compressional events on the horizontal components would suggest significant dip on these events. This is also consistent with the strong mode converted compressional to shear energy. Significant time moveout is evident on the shear aligned data.

The polarity convention for displaying horizontal component data is not consistent with the Z - axis, and will change if the upgoing wavefield arrives at the geophone from the opposite side of the borehole from that of the downgoing wavefield. Tectonic stresses can also effect phase rotations in the shear components. In the case of a vertical well we can expect the apparent polarity of the horizontal components to vary with time.

APPENDIX - 1 SUMMARY OF GEOPHYSICAL LISTINGS

Six geophysical data listings are appended to this report. Following is a brief description of the format of each listing.

Geophysical Airgun Report

1. Level number : the level number starting from the top level (includes any imposed shots).
2. Vertical depth from KB : dkb , the depth in metres from kelly bushing .
3. Vertical depth from SRD : $dsrd$, the depth in metres from seismic reference datum.
4. Vertical depth from GL : dgl , the depth in metres from ground level.
5. Observed travel time HYD to GEO : $tim0$, the transit time picked from the stacked data by subtracting the surface sensor first break time from the downhole sensor first break time.
6. Vertical travel time SRC to GEO : $timv$, is corrected for source to hydrophone distance and for source offset.
7. Vertical travel time SRD to GEO : $shtm$, is $timv$ corrected for the vertical distance between source and datum.
8. Average velocity SRD to GEO : the average seismic velocity from datum to the corresponding checkshot level, $\frac{dsrd}{shtm}$.
9. Delta depth between shots : $\Delta depth$, the vertical distance between each level.
10. Delta time between shots : $\Delta time$, the difference in vertical travel time ($shtm$) between each level.
11. Interval velocity between shots : the average seismic velocity between each level, $\frac{\Delta depth}{\Delta time}$.

Drift Computation Report

1. Level number : the level number starting from the top level (includes any imposed shots).
2. Vertical depth from KB : the depth in metres from kelly bushing .
3. Vertical depth from SRD : the depth in metres from seismic reference datum.
4. Vertical depth from GL : the depth in metres from ground level.
5. Vertical travel time SRD to GEO : the calculated vertical travel time from datum to downhole geophone (see column 7, Geophysical Airgun Report).
6. Integrated raw sonic time : the raw sonic log is integrated from top to bottom and listed at each level. An initial value at the top of the sonic log is set equal to the checkshot time at that level. This may be an imposed shot if a shot was not taken at the top of the sonic.
7. Computed drift at level : the checkshot time minus the integrated raw sonic time.
8. Computed blk-shft correction : the drift gradient between any two checkshot levels ($\frac{\Delta drift}{\Delta depth}$).

Sonic Adjustment Parameter Report

1. Knee number : the knee number starting from the highest knee. (The first knees listed will generally be at SRD and the top of sonic. The drift imposed at these knees will normally be zero.)
2. Vertical depth from KB : the depth in metres from kelly bushing .
3. Vertical depth from SRD : the depth in metres from seismic reference datum.
4. Vertical depth from GL : the depth in metres from ground level.
5. Drift at knee : the value of drift imposed at each knee.
6. Blockshift used : the change in drift divided by the change in depth between any two levels.
7. Delta-T minimum used : see section 4 of report for an explanation of Δt_{min} .
8. Reduction factor : see section 4 of report.
9. Equivalent blockshift : the gradient of the imposed drift curve.

Velocity Report

1. Level number : the level number starting from the top level (includes any imposed shots).
2. Vertical depth from KB : the depth in metres from kelly bushing .
3. Vertical depth from SRD : the depth in metres from seismic reference datum
4. Vertical depth from GL : the depth in metres from ground level
5. Vertical travel time SRD to GEOPH : the vertical travel time from SRD to downhole geophone (see column 7, Geophysical Airgun Report)
6. Integrated adjusted sonic time : the adjusted sonic log is integrated from top to bottom. An initial value at the the top of the sonic is set equal the checkshot time at that level. (The adjusted sonic log is the drift corrected sonic log.)
7. Drift=shot time-raw son : the check shot time minus the raw integrated sonic time.
8. Residual=shot time-adj son : the check shot time minus the adjusted integrated sonic time. This is the difference between calculated drift and the imposed drift.
9. Adjusted interval velocity : the interval velocity calculated from the integrated adjusted sonic time at each level.

Time Converted Velocity Report

The data in this listing has been resampled in time.

1. Two way travel time from SRD : This is the index for the data in this listing. The first value is at SRD (0 milliseconds) and the sampling rate is 2 milliseconds.
2. Measured depth from KB : the depth from KB at each corresponding value of two way time.
3. Vertical depth from SRD : the vertical depth from SRD at each corresponding value of two way time.
4. Average velocity SRD to GEO : the vertical depth from SRD divided by half the two way time.
5. RMS velocity : the root mean square velocity from datum to the corresponding value of two way time.

$$v_{rms} = \sqrt{\sum_1^n v_i^2 t_i / \sum_1^n t_i}$$

where v_i is the velocity between each 2 milliseconds interval.

6. First normal moveout : the correction time in milliseconds to be applied to the two way travel time for a specified moveout distance (default = 3000 feet).
7. Second normal moveout : the correction time in milliseconds to be applied to the two way travel time for a specified moveout distance (default = 4500 feet).
8. Third normal moveout : the correction time in milliseconds to be applied to the two way travel time for a specified moveout distance (default = 6000 feet).
9. Interval velocity : the velocity between each sampled depth. Typically, the sampling rate is 2 milliseconds two way time, (1 millisecond one way time) therefore the interval velocity will be equal to the depth increment divided by 0.001. It is equivalent to column 9 from the the Velocity Report.

Synthetic Seismogram Table

1. Two way travel time from SRD : This is the index for the data in this listing. The first value is at the top of the sonic. The default sampling rate is 2 milliseconds.
2. Vertical depth from SRD : the vertical depth from SRD at each corresponding value of two way time.
3. Interval velocity : the velocity between each sampled depth. Typically, the sampling rate is 2 milliseconds two way time, (1 millisecond one way time) therefore the interval velocity will be equal to the depth increment divided by 0.001. It is equivalent to column 9 from the the Velocity Report.
4. Interval density : the average density between two successive values of two way time.
5. Reflect. coeff. : the difference in acoustic impedance divided by the sum of the acoustic impedance between any two levels. The acoustic impedance is the product of the interval density and the interval velocity.
6. Two way atten. coeff. : is computed from the series

$$A_n = (1 - R_1^2).(1 - R_2^2).(1 - R_3^2)...(1 - R_n^2)$$

7. Synthetic seismo. primary : the product of the reflection coefficient at each depth and the two way attenuation coefficient up to that depth.

$$Primary_n = R_n \cdot A_{n-1}$$

8. Primary + multiple : a transform technique is used to calculate multiples from the input reflection coefficients.
9. Multiples only : (Primary + multiple) - (Synthetic seismo. primary)

GEOGRAM PLOTS

Seismic Calibration Log

40 hertz Geogram

50 hertz Geogram

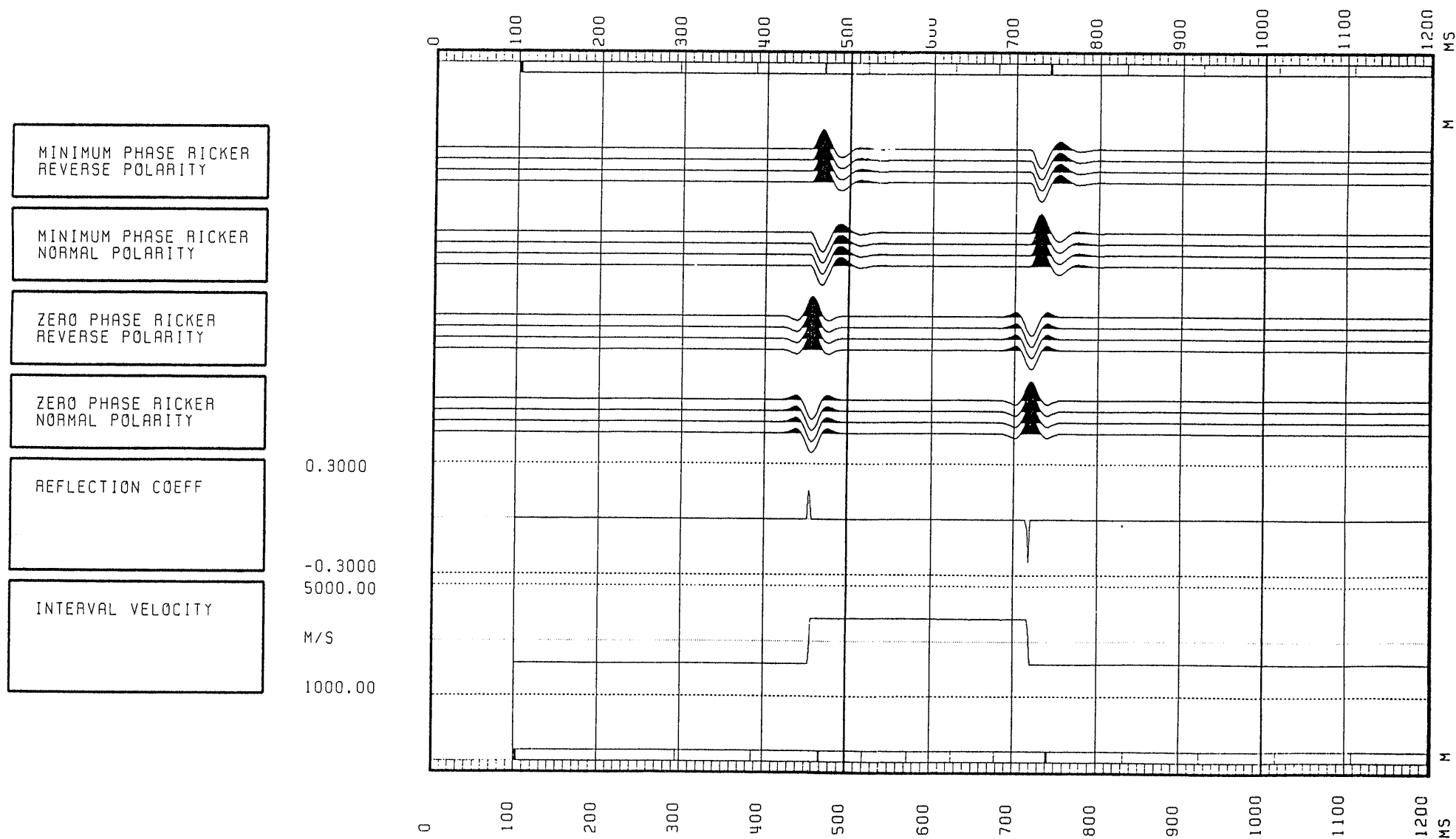
60 hertz Geogram

VSP PLOTS

- Plot 1 X, Y & Z axis : Stacked data
- Plot 2 Amplitude Recovery
- Plot 3 Velocity Filter
- Plot 4 Predictive Deconvolution
- Plot 5 Predictive Deconvolution & Corridor Stack
- Plot 6 Waveshaping Deconvolution
- Plot 7 Waveshaping Deconvolution & Corridor Stack
- Plot 8 VSP Inversion
- Plot 9 Compressional/Shear Velocity Analysis
- Plot 10 Horizontal Projection on Shear Arrival
- Plot 11 Horizontal Projection on Compressional Arrival
- Plot 12 Shear Wave Processing
- Plot 13 Comp & Shear VSP from Horizontal Components

SCHLUMBERGER (SEG-1976) WAVELET POLARITY CONVENTION

Figure 1



Shot

LONG DEFINITIONS

GLOBAL

KB - ELEVATION OF THE KELLY-BUSHING ABOVE MSL OR MWL
 SRD - ELEVATION OF THE SEISMIC REFERENCE DATUM ABOVE MSL OR MWL
 EKB - ELEVATION OF KELLY BUSHING
 GL - ELEVATION OF USER'S REFERENCE (GENERALLY GROUND LEVEL) ABOVE SRD
 VELHYD - VELOCITY OF THE MEDIUM BETWEEN THE SOURCE AND THE HYDROPHONE
 VELSUR - VELOCITY OF THE MEDIUM BETWEEN THE SOURCE AND THE SRD

MATRIX

GUNELZ - SOURCE ELEVATION ABOVE SRD (ONE FOR THE WHOLE JOB; OR ONE PER SHOT)
 GUNEWZ - SOURCE DISTANCE FROM THE BOREHOLE AXIS IN EW DIRECTION (CF. GUNELZ)
 GUNNSZ - SOURCE DISTANCE FROM THE BOREHOLE AXIS IN NS DIRECTION (CF. GUNELZ)
 HYDELZ - HYDROPHONE ELEVATION ABOVE SRD (CF. GUNELZ)
 HYDEWZ - HYDROPHONE DISTANCE FROM THE BOREH AXIS IN EW DIRECTION (CF GUNELZ)
 HYDNSZ - HYDROPHONE DISTANCE FROM THE BOREH AXIS IN NS DIRECTION (CF GUNELZ)
 TRTHYD - TRAVEL TIME FROM THE HYDROPHONE TO THE SOURCE
 TRTSRD - TRAVEL TIME FROM THE SOURCE TO THE SRD
 DEWVEL - DEVIATED WELL DATA PER SHOT : MEAS. DEPTH, VERT. DEPTH, EW, NS

SAMPLED

SHOT.GSH - SHOT NUMBER
 DKB.GSH - MEASURED DEPTH FROM KELLY-BUSHING
 DSRD.GSH - DEPTH FROM SRD
 DGL.GSH - VERTICAL DEPTH RELATIVE TO GROUND LEVEL (USER'S REFERENCE)
 TIMO.GSH - MEASURED TRAVEL TIME FROM HYDROPHONE TO GEOPHONE
 TIMV.GSH - VERTICAL TRAVEL TIME FROM THE SOURCE TO THE GEOPHONE
 SHTM.GSH - SHOT TIME (WST)
 AVGV.GSH - AVERAGE SEISMIC VELOCITY
 DELZ.GSH - DEPTH INTERVAL BETWEEN SUCCESSIVE SHOTS
 DELT.GSH - TRAVEL TIME INTERVAL BETWEEN SUCCESSIVE SHOTS
 INTV.GSH - INTERNAL VELOCITY, AVERAGE

(GLOBAL PARAMETERS)

(VALUE)

| | | | | |
|---------------------------|--------|---|----------|-----|
| ELEV OF KB AB. MSL (WST) | KB | : | 22.0000 | M |
| ELEV OF SRD AB. MSL (WST) | SRD | : | 0 | M |
| ELEVATION OF KELLY BUSHI | EKB | : | 22.0000 | M |
| ELEV OF GL AB. SRD (WST) | GL | : | -51.0000 | M |
| VEL SOURCE-HYDRO (WST) | VELHYD | : | 1480.00 | M/S |
| VEL SOURCE-SRD (WST) | VELSUR | : | 1480.00 | M/S |

(MATRIX PARAMETERS)

| | SOURCE ELV M | SOURCE EW M | SOURCE NS M | HYDRO ELEV M | HYDRO EW M | HYDRO NS M |
|---|-----------------|----------------|----------------|-----------------|---------------|---------------|
| 1 | -5.00 | -45.32 | -21.13 | -10.00 | -45.32 | -21.13 |

| | TRT HYD-SC MS | TRT SC-SRD MS |
|---|------------------|------------------|
| 1 | 3.38 | 3.38 |

| | MD @ KB M | VD @ KB M | VD @ SRD M | E-W COORD M | N-S COORD M |
|----|--------------|--------------|---------------|----------------|----------------|
| 1 | 73.00 | 73.00 | 51.00 | 0 | 0 |
| 2 | 220.00 | 220.00 | 198.00 | 0 | 0 |
| 3 | 445.00 | 445.00 | 423.00 | 0 | 0 |
| 4 | 460.00 | 460.00 | 438.00 | 0 | 0 |
| 5 | 475.00 | 475.00 | 453.00 | 0 | 0 |
| 6 | 490.00 | 490.00 | 468.00 | 0 | 0 |
| 7 | 505.00 | 505.00 | 483.00 | 0 | 0 |
| 8 | 520.00 | 520.00 | 498.00 | 0 | 0 |
| 9 | 535.00 | 535.00 | 513.00 | 0 | 0 |
| 10 | 550.00 | 550.00 | 528.00 | 0 | 0 |
| 11 | 565.00 | 565.00 | 543.00 | 0 | 0 |
| 12 | 580.00 | 580.00 | 558.00 | 0 | 0 |
| 13 | 595.00 | 595.00 | 573.00 | 0 | 0 |
| 14 | 610.00 | 610.00 | 588.00 | 0 | 0 |
| 15 | 625.00 | 625.00 | 603.00 | 0 | 0 |
| 16 | 640.00 | 640.00 | 618.00 | 0 | 0 |
| 17 | 656.00 | 656.00 | 634.00 | 0 | 0 |
| 18 | 670.00 | 670.00 | 648.00 | 0 | 0 |
| 19 | 685.00 | 685.00 | 663.00 | 0 | 0 |
| 20 | 700.00 | 700.00 | 678.00 | 0 | 0 |
| 21 | 715.00 | 715.00 | 693.00 | 0 | 0 |
| 22 | 730.00 | 730.00 | 708.00 | 0 | 0 |
| 23 | 745.00 | 745.00 | 723.00 | 0 | 0 |
| 24 | 760.00 | 760.00 | 738.00 | 0 | 0 |
| 25 | 774.00 | 774.00 | 752.00 | 0 | 0 |
| 26 | 790.00 | 790.00 | 768.00 | 0 | 0 |
| 27 | 805.00 | 805.00 | 783.00 | 0 | 0 |
| 28 | 820.00 | 820.00 | 798.00 | 0 | 0 |
| 29 | 835.00 | 835.00 | 813.00 | 0 | 0 |
| 30 | 850.00 | 850.00 | 828.00 | 0 | 0 |
| 31 | 865.00 | 865.00 | 843.00 | 0 | 0 |
| 32 | 880.00 | 880.00 | 858.00 | 0 | 0 |
| 33 | 895.00 | 895.00 | 873.00 | 0 | 0 |

| LEVEL NUMBER | MEASUR DEPTH FROM KB M | VERTIC DEPTH FROM SRD M | VERTIC DEPTH FROM GL M | OBSERV TRAVEL TIME HYD/GEO MS | VERTIC TRAVEL TIME SRC/GEO MS | VERTIC TRAVEL TIME SRD/GEO MS | AVERAGE VELOC SRD/GEO M/S | DELTA DEPTH BETWEEN SHOTS M | DELTA TIME BETWEEN SHOTS MS | INTERV VELOC BETWEEN SHOTS M/S |
|-----------------|------------------------------------|-------------------------------------|------------------------------------|---|---|---|------------------------------------|---|---|--|
| 1 | 73.00 | 51.00 | 0 | 42.53 | 31.08 | 34.46 | 1480 | | | |
| 2 | 220.00 | 198.00 | 147.00 | 113.00 | 112.66 | 116.04 | 1706 | 147.00 | 81.58 | 1802 |
| 3 | 445.00 | 423.00 | 372.00 | 213.00 | 214.85 | 218.23 | 1938 | 225.00 | 102.19 | 2202 |
| 4 | 460.00 | 438.00 | 387.00 | 220.00 | 221.90 | 225.28 | 1944 | 15.00 | 7.06 | 2126 |
| 5 | 475.00 | 453.00 | 402.00 | 226.00 | 227.96 | 231.34 | 1958 | 15.00 | 6.06 | 2476 |
| 6 | 490.00 | 468.00 | 417.00 | 233.00 | 235.01 | 238.39 | 1963 | 15.00 | 7.05 | 2128 |
| 7 | 505.00 | 483.00 | 432.00 | 240.00 | 242.06 | 245.44 | 1968 | 15.00 | 7.05 | 2129 |
| 8 | 520.00 | 498.00 | 447.00 | 247.00 | 249.10 | 252.48 | 1972 | 15.00 | 7.04 | 2130 |
| 9 | 535.00 | 513.00 | 462.00 | 253.00 | 255.15 | 258.52 | 1984 | 15.00 | 6.04 | 2481 |
| 10 | 550.00 | 528.00 | 477.00 | 259.00 | 261.19 | 264.57 | 1996 | 15.00 | 6.04 | 2483 |
| 11 | 565.00 | 543.00 | 492.00 | 265.00 | 267.23 | 270.61 | 2007 | 15.00 | 6.04 | 2484 |
| 12 | 580.00 | 558.00 | 507.00 | 272.00 | 274.26 | 277.64 | 2010 | 15.00 | 7.03 | 2133 |
| 13 | 595.00 | 573.00 | 522.00 | 278.00 | 280.29 | 283.67 | 2020 | 15.00 | 6.03 | 2486 |
| 14 | 610.00 | 588.00 | 537.00 | 285.00 | 287.32 | 290.70 | 2023 | 15.00 | 7.03 | 2134 |
| 15 | 625.00 | 603.00 | 552.00 | 292.00 | 294.35 | 297.73 | 2025 | 15.00 | 7.03 | 2134 |
| 16 | 640.00 | 618.00 | 567.00 | 299.00 | 301.38 | 304.76 | 2028 | 15.00 | 7.03 | 2135 |
| 17 | 656.00 | 634.00 | 583.00 | 307.00 | 309.40 | 312.78 | 2027 | 16.00 | 8.02 | 1994 |
| 18 | 670.00 | 648.00 | 597.00 | 314.00 | 316.42 | 319.80 | 2026 | 14.00 | 7.02 | 1994 |
| 19 | 685.00 | 663.00 | 612.00 | 321.00 | 323.45 | 326.82 | 2029 | 15.00 | 7.02 | 2136 |
| 20 | 700.00 | 678.00 | 627.00 | 329.00 | 331.46 | 334.84 | 2025 | 15.00 | 8.02 | 1871 |
| 21 | 715.00 | 693.00 | 642.00 | 336.00 | 338.49 | 341.86 | 2027 | 15.00 | 7.02 | 2137 |
| 22 | 730.00 | 708.00 | 657.00 | 343.00 | 345.51 | 348.88 | 2029 | 15.00 | 7.02 | 2137 |
| 23 | 745.00 | 723.00 | 672.00 | 350.00 | 352.52 | 355.90 | 2031 | 15.00 | 7.02 | 2137 |
| 24 | 760.00 | 738.00 | 687.00 | 356.00 | 358.55 | 361.92 | 2039 | 15.00 | 6.02 | 2491 |

| LEVEL NUMBER | MEASUR DEPTH FROM KB M | VERTIC DEPTH FROM SRD M | VERTIC DEPTH FROM GL M | OBSERV TRAVEL TIME HYD/GEO MS | VERTIC TRAVEL TIME SRC/GEO MS | VERTIC TRAVEL TIME SRD/GEO MS | AVERAGE VELOC SRD/GEO M/S | DELTA DEPTH BETWEEN SHOTS M | DELTA TIME BETWEEN SHOTS MS | INTERV VELOC BETWEEN SHOTS M/S |
|-----------------|------------------------------------|-------------------------------------|------------------------------------|---|---|---|------------------------------------|---|---|--|
| 25 | 774.00 | 752.00 | 701.00 | 361.00 | 363.56 | 366.94 | 2049 | 14.00 | 5.02 | 2789 |
| 26 | 790.00 | 768.00 | 717.00 | 366.00 | 368.59 | 371.97 | 2065 | 16.00 | 5.02 | 3185 |
| 27 | 805.00 | 783.00 | 732.00 | 371.00 | 373.61 | 376.99 | 2077 | 15.00 | 5.02 | 2988 |
| 28 | 820.00 | 798.00 | 747.00 | 377.00 | 379.62 | 383.00 | 2084 | 15.00 | 6.02 | 2493 |
| 29 | 835.00 | 813.00 | 762.00 | 384.00 | 386.64 | 390.02 | 2085 | 15.00 | 7.01 | 2138 |
| 30 | 850.00 | 828.00 | 777.00 | 389.00 | 391.66 | 395.03 | 2096 | 15.00 | 5.02 | 2990 |
| 31 | 865.00 | 843.00 | 792.00 | 395.00 | 397.67 | 401.05 | 2102 | 15.00 | 6.01 | 2494 |
| 32 | 880.00 | 858.00 | 807.00 | 401.00 | 403.69 | 407.06 | 2108 | 15.00 | 6.01 | 2494 |
| 33 | 895.00 | 873.00 | 822.00 | 408.00 | 410.70 | 414.08 | 2108 | 15.00 | 7.01 | 2139 |

Drift

ANALYST: M. SANDERS

14-JUL-87 13:29:35

PROGRAM: GDRIFT 007.E09

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*          SCHLUMBERGER              *  
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DRIFT COMPUTATION REPORT

COMPANY : LASMO ENERGY
WELL : PATRICIA - 1
FIELD : WILDCAT
COUNTRY : AUSTRALIA
REFERENCE: 570705

LONG DEFINITIONS

GLOBAL

- KB - ELEVATION OF THE KELLY-BUSHING ABOVE MSL OR MWL
- SRD - ELEVATION OF THE SEISMIC REFERENCE DATUM ABOVE MSL OR MWL
- EKB - ELEVATION OF KELLY BUSHING
- GL - ELEVATION OF USER'S REFERENCE (GENERALLY GROUND LEVEL) ABOVE SRD
- XSTART - TOP OF ZONE PROCESSED BY WST
- XSTOP - BOTTOM OF ZONE PROCESSED BY WST
- GAD001 - RAW SONIC CHANNEL NAME USED FOR WST SONIC ADJUSTMENT
- UNFDEN - UNIFORM DENSITY VALUE

ZONE

- LOFDEN - LAYER OPTION FLAG FOR DENSITY : -1=NONE; 0=UNIFORM; 1=UNIFORM+LAYER
- LAYDEN - USER SUPPLIED DENSITY DATA

SAMPLED

- SHOT - SHOT NUMBER
- DKE - MEASURED DEPTH FROM KELLY-BUSHING
- DSRD - DEPTH FROM SRD
- DGL - VERTICAL DEPTH RELATIVE TO GROUND LEVEL (USER'S REFERENCE)
- SHTM - SHOT TIME (WST)
- RAWS - RAW SONIC (WST)
- SHDR - DRIFT AT SHOT OR KNEE
- BLSH - BLOCK SHIFT BETWEEN SHOTS OR KNEE

(GLOBAL PARAMETERS)

(VALUE)

| | | | | |
|---------------------------|--------|---|----------------------|------|
| ELEV OF KB AB. MSL (WST) | KB | : | 22.0000 | M |
| ELEV OF SRD AB. MSL (WST) | SRD | : | 0 | M |
| ELEVATION OF KELLY BUSHI | EKB | : | 22.0000 | M |
| ELEV OF GL AB. SRD (WST) | GL | : | -51.0000 | M |
| TOP OF ZONE PROCD (WST) | XSTART | : | 0 | M |
| BOT OF ZONE PROCD (WST) | XSTOP | : | 0 | M |
| RAW SONIC CH NAME (WST) | GAD001 | : | DT.ATT.004.IPA.FLP.* | |
| UNIFCRM DENSITY VALUE | UNFDEN | : | 2.30000 | G/C3 |

(ZONED PARAMETERS)

(VALUE)

(LIMITS)

| | | | | | | |
|--------------------------|--------|---|-----------|---------|---------|-----|
| LAYER OPTION FLAG DENS | LOFDEN | : | 1.000000 | 30479.7 | - | 0 |
| USER SUPPLIED DENSITY DA | LAYDEN | : | -999.2500 | G/C3 | 30479.7 | - 0 |

| LEVEL NUMBER | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | VERTICAL DEPTH FROM GL M | VERTICAL TRAVEL TIME SRD/GEO MS | INTEGRATED RAW SONIC TIME MS | COMPUTED DRIFT AT LEVEL MS | COMPUTED BLK-SHFT CORRECTION US/M |
|-----------------|--------------------------------------|---------------------------------------|--------------------------------------|---|---------------------------------------|-------------------------------------|--|
| 1 | 73.00 | 51.00 | 0 | 34.46 | 34.46 | 0 | 0 |
| 2 | 220.00 | 198.00 | 147.00 | 116.04 | 116.04 | 0 | 0 |
| 3 | 445.00 | 423.00 | 372.00 | 218.23 | 215.58 | 2.64 | 11.74 |
| 4 | 460.00 | 438.00 | 387.00 | 225.28 | 222.20 | 3.08 | 29.23 |
| 5 | 475.00 | 453.00 | 402.00 | 231.34 | 228.52 | 2.82 | -17.33 |
| 6 | 490.00 | 468.00 | 417.00 | 238.39 | 235.09 | 3.30 | 32.12 |
| 7 | 505.00 | 483.00 | 432.00 | 245.44 | 241.68 | 3.75 | 29.98 |
| 8 | 520.00 | 498.00 | 447.00 | 252.48 | 247.96 | 4.52 | 51.10 |
| 9 | 535.00 | 513.00 | 462.00 | 258.52 | 253.73 | 4.80 | 18.56 |
| 10 | 550.00 | 528.00 | 477.00 | 264.57 | 259.28 | 5.29 | 32.79 |
| 11 | 565.00 | 543.00 | 492.00 | 270.61 | 265.13 | 5.48 | 12.52 |
| 12 | 580.00 | 558.00 | 507.00 | 277.64 | 271.01 | 6.62 | 76.51 |
| 13 | 595.00 | 573.00 | 522.00 | 283.67 | 276.98 | 6.69 | 4.27 |
| 14 | 610.00 | 588.00 | 537.00 | 290.70 | 283.69 | 7.01 | 21.65 |
| 15 | 625.00 | 603.00 | 552.00 | 297.73 | 289.73 | 8.00 | 65.83 |
| 16 | 640.00 | 618.00 | 567.00 | 304.76 | 295.90 | 8.86 | 57.21 |
| 17 | 656.00 | 634.00 | 583.00 | 312.78 | 303.36 | 9.42 | 35.01 |
| 18 | 670.00 | 648.00 | 597.00 | 319.80 | 309.95 | 9.85 | 31.04 |
| 19 | 685.00 | 663.00 | 612.00 | 326.82 | 316.73 | 10.09 | 16.01 |
| 20 | 700.00 | 678.00 | 627.00 | 334.84 | 323.47 | 11.38 | 85.46 |
| 21 | 715.00 | 693.00 | 642.00 | 341.86 | 330.79 | 11.08 | -19.76 |
| 22 | 730.00 | 708.00 | 657.00 | 348.88 | 338.26 | 10.62 | -30.63 |
| 23 | 745.00 | 723.00 | 672.00 | 355.90 | 345.50 | 10.41 | -14.15 |
| 24 | 760.00 | 738.00 | 687.00 | 361.92 | 351.49 | 10.43 | 1.85 |

| LEVEL NUMBER | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | VERTICAL DEPTH FROM GL M | VERTICAL TRAVEL TIME SRD/GEO MS | INTEGRATED RAW SONIC TIME MS | COMPUTED DRIFT AT LEVEL MS | COMPUTED BLK-SHFT CORRECTION US/M |
|-----------------|--------------------------------------|---------------------------------------|--------------------------------------|---|---------------------------------------|-------------------------------------|--|
| 25 | 774.00 | 752.00 | 701.00 | 366.94 | 355.93 | 11.01 | 41.05 |
| 26 | 790.00 | 768.00 | 717.00 | 371.97 | 361.18 | 10.79 | -14.00 |
| 27 | 805.00 | 783.00 | 732.00 | 376.99 | 366.46 | 10.53 | -17.20 |
| 28 | 820.00 | 798.00 | 747.00 | 383.00 | 372.52 | 10.49 | -2.72 |
| 29 | 835.00 | 813.00 | 762.00 | 390.02 | 378.48 | 11.53 | 69.85 |
| 30 | 850.00 | 828.00 | 777.00 | 395.03 | 384.01 | 11.02 | -34.26 |
| 31 | 865.00 | 843.00 | 792.00 | 401.05 | 389.81 | 11.24 | 14.88 |
| 32 | 880.00 | 858.00 | 807.00 | 407.06 | 395.89 | 11.17 | -4.80 |
| 33 | 895.00 | 873.00 | 822.00 | 414.08 | 401.71 | 12.36 | 79.52 |
| 34 | 899.92 | 877.92 | 826.92 | 415.96 | 403.59 | 12.36 | 0 |

ANALYST: M. SANDERS

14-JUL-87 13:42:37

PROGRAM: GADJST 008.E08

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*                                     *  
*          SCHLUMBERGER              *  
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SONIC ADJUSTMENT PARAMETER REPORT

COMPANY : LASMO ENERGY
WELL : PATRICIA - 1
FIELD : WILDCAT
CCOUNTRY : AUSTRALIA
REFERENCE: 570705

LONG DEFINITIONS

GLOBAL

SRCDRF - ORIGIN OF ADJUSTMENT DATA
 CONADJ - CONSTANT ADJUSTMENT TO AUTOMATIC DELTA-T MINIMUM = 7.5 US/F
 UNERTH - UNIFORM EARTH VELOCITY (GTRFRM)

ZONE

ZDRIFT - USER DRIFT AT BOTTOM OF THE ZONE
 ADJOPZ - TYPE OF ADJUSTMENT IN THE DRIFT ZONE : 0=DELTA-T MIN, 1=BLOCKSHIFT
 ADJUSZ - DELTA-T MINIMUM USED FOR ADJUSTMENT IN THE DRIFT ZONE
 LOFVEL - LAYER OPTION FLAG FOR VELOCITY: -1=NONE; 0=UNIFORM; 1=UNIFORM+LAYER
 LAYVEL - USER SUPPLIED VELOCITY DATA

SAMPLED

SHOT - SHOT NUMBER
 VDKB - VERTICAL DEPTH RELATIVE TO KB
 DSRD - DEPTH FROM SRD
 DGL - VERTICAL DEPTH RELATIVE TO GRUND LEVEL (USER'S REFERENCE)
 KNEE - KNEE
 BLSH - BLOCK SHIFT BETWEEN SHOTS OR KNEE
 DTMI - VALUE OF DELTA-T MINIMUM USED
 COEF - DELTA-T MIN COEFFICIENT USED IN THE DRIFT ZONE
 DRGR - GRADIENT OF DRIFT CURVE

(GLOBAL PARAMETERS)

(VALUE)

| | | | | |
|------------------------|--------|---|---------|------|
| ORIG OF ADJ DATA (WST) | SRCDRF | : | 2.00000 | |
| CONS SONIC ADJST (WST) | CONADJ | : | 24.6063 | US/M |
| UNIFORM EARTH VELOCITY | UNERTH | : | 2133.60 | M/S |

(ZONED PARAMETERS)

(VALUE)

(LIMITS)

| | | | | | | | |
|-------------------------|--------|----|-----------|------|---------|---|---------|
| USER DRIFT ZONE (WST) | ZDRIFT | : | 11.80000 | MS | 900.000 | - | 750.500 |
| | | | 10.30000 | | 750.500 | | 702.000 |
| | | | 10.00000 | | 702.000 | | 643.500 |
| | | | 9.000000 | | 643.500 | | 509.500 |
| | | | 4.000000 | | 509.500 | | 220.000 |
| | | | 0 | | 220.000 | | 0 |
| ADJUSMNT MODE (WST) | ADJOPZ | :: | -999.2500 | | 30479.7 | - | 0 |
| USER DELTA-T MIN (WST) | ADJUSZ | :: | -999.2500 | US/M | 30479.7 | - | 0 |
| LAYER OPTION FLAG VELOC | LOFVEL | :: | 1.000000 | | 30479.7 | - | 0 |
| USER VELOC (WST) | LAYVEL | : | 1802.000 | M/S | 220.000 | - | 73.0000 |
| | | | 1480.000 | | 73.0000 | | 0 |

COMPANY : LASMO ENERGY

WELL : PATRICIA - 1

PAGE 2

| KNEE NUMBER | VERTICAL DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | VERTICAL DEPTH FROM GL M | DRIFT AT KNEE MS | BLOCKSHIFT USED US/M | DELTA-T MINIMUM USED US/M | REDUCTION FACTOR G | EQUIVALENT BLOCKSHIFT US/M |
|----------------|--------------------------------------|---------------------------------------|--------------------------------------|---------------------------|----------------------------|------------------------------------|--------------------------|----------------------------------|
| 2 | 220.00 | 198.00 | 147.00 | 0 | 0 | | | 0 |
| 3 | 509.50 | 487.50 | 436.50 | 4.00 | 13.82 | | | 13.82 |
| 4 | 643.50 | 621.50 | 570.50 | 9.00 | 37.31 | | | 37.31 |
| 5 | 702.00 | 680.00 | 629.00 | 10.00 | 17.09 | | | 17.09 |
| 6 | 750.50 | 728.50 | 677.50 | 10.30 | 6.19 | | | 6.19 |
| 7 | 900.00 | 878.00 | 827.00 | 11.80 | 10.03 | | | 10.03 |

ANALYST: M. SANDERS

14-JUL-87 13:43:31

PROGRAM: GADJST 008.E08

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*          SCHLUMBERGER              *  
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VELOCITY REPORT

COMPANY : LASMO ENERGY
WELL : PATRICIA - 1
FIELD : WILDCAT
COUNTRY : AUSTRALIA
REFERENCE: 570705

ANALYST: M. SANDERS

14-JUL-87 13:43:31

PROGRAM: GADJST 008.E08

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*                                     *  
*          SCHLUMBERGER              *  
*                                     *  
*                                     *  
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VELOCITY REPORT

COMPANY : LASMO ENERGY
WELL : PATRICIA - 1
FIELD : WILDCAT
COUNTRY : AUSTRALIA
REFERENCE: 570705

LONG DEFINITIONS

GLOBAL

KB - ELEVATION OF THE KELLY-BUSHING ABOVE MSL OR MWL
 SRD - ELEVATION OF THE SEISMIC REFERENCE DATUM ABOVE MSL OR MWL
 EKB - ELEVATION OF KELLY BUSHING
 GL - ELEVATION OF USER'S REFERENCE (GENERALLY GROUND LEVEL) ABOVE SRD
 UNERTH - UNIFORM EARTH VELOCITY (GTRFRM)

ZONE

LOFVEL - LAYER OPTION FLAG FOR VELOCITY: -1=NONE; 0=UNIFORM; 1=UNIFORM+LAYER
 LAYVEL - USER SUPPLIED VELOCITY DATA

SAMPLED

SHOT - SHOT NUMBER
 DKE - MEASURED DEPTH FROM KELLY-BUSHING
 DSRD - DEPTH FROM SRD
 DGL - VERTICAL DEPTH RELATIVE TO GROUND LEVEL (USER'S REFERENCE)
 SHTM - SHOT TIME (WST)
 ADJS - ADJUSTED SONIC TRAVEL TIME
 SHDR - DRIFT AT SHOT OR KNEE
 REST - RESIDUAL TRAVEL TIME AT KNEE
 INTV - INTERNAL VELOCITY, AVERAGE

(GLOBAL PARAMETERS)

(VALUE)

| | | | | |
|--------------------------|--------|---|----------|-----|
| ELEV OF KB AB. MSL (WST) | KB | : | 22.0000 | M |
| ELEV OF SRD AB. MSL(WST) | SRD | : | 0 | M |
| ELEVATION OF KELLY BUSHI | EKB | : | 22.0000 | M |
| ELEV OF GL AB. SRD(WST) | GL | : | -51.0000 | M |
| UNIFORM EARTH VELOCITY | UNERTH | : | 2133.60 | M/S |

(ZONED PARAMETERS)

(VALUE)

(LIMITS)

| | | | | | | |
|-------------------------|--------|---|----------|---------|---------|-----------|
| LAYER OPTION FLAG VELOC | LOFVEL | : | 1.000000 | 30479.7 | - | 0 |
| USER VELOC (WST) | LAYVEL | : | 1802.000 | M/S | 220.000 | - 73.0000 |
| | | | 1480.000 | | 73.0000 | 0 |

| LEVEL NUMBER | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | VERTICAL DEPTH FROM GL M | VERTICAL TRAVEL TIME SRD/GEOPH MS | INTEGRATED ADJUSTED SONIC TIME MS | DRIFT = SHOT TIME - RAW SON MS | RESIDUAL = SHOT TIME - ADJ SON MS | ADJUSTED INTERVAL VELOCITY M/S |
|-----------------|--------------------------------------|---------------------------------------|--------------------------------------|---|---|--|---|---|
| 1 | 73.00 | 51.00 | 0 | 34.46 | 34.46 | 0 | 0 | 1480 |
| 2 | 220.00 | 198.00 | 147.00 | 116.04 | 116.03 | 0 | 0 | 1802 |
| 3 | 445.00 | 423.00 | 372.00 | 218.23 | 218.69 | 2.64 | -.47 | 2192 |
| 4 | 460.00 | 438.00 | 387.00 | 225.28 | 225.52 | 3.08 | -.23 | 2198 |
| 5 | 475.00 | 453.00 | 402.00 | 231.34 | 232.04 | 2.82 | -.70 | 2298 |
| 6 | 490.00 | 468.00 | 417.00 | 238.39 | 238.82 | 3.30 | -.43 | 2214 |
| 7 | 505.00 | 483.00 | 432.00 | 245.44 | 245.62 | 3.75 | -.18 | 2206 |
| 8 | 520.00 | 498.00 | 447.00 | 252.48 | 252.35 | 4.52 | .13 | 2230 |
| 9 | 535.00 | 513.00 | 462.00 | 258.52 | 258.66 | 4.80 | -.14 | 2374 |
| 10 | 550.00 | 528.00 | 477.00 | 264.57 | 264.77 | 5.29 | -.21 | 2455 |
| 11 | 565.00 | 543.00 | 492.00 | 270.61 | 271.20 | 5.48 | -.59 | 2336 |
| 12 | 580.00 | 558.00 | 507.00 | 277.64 | 277.64 | 6.62 | 0 | 2328 |
| 13 | 595.00 | 573.00 | 522.00 | 283.67 | 284.18 | 6.69 | -.50 | 2295 |
| 14 | 610.00 | 588.00 | 537.00 | 290.70 | 291.44 | 7.01 | -.74 | 2066 |
| 15 | 625.00 | 603.00 | 552.00 | 297.73 | 298.03 | 8.00 | -.30 | 2275 |
| 16 | 640.00 | 618.00 | 567.00 | 304.76 | 304.76 | 8.86 | -.01 | 2228 |
| 17 | 656.00 | 634.00 | 583.00 | 312.78 | 312.57 | 9.42 | .21 | 2048 |
| 18 | 670.00 | 648.00 | 597.00 | 319.80 | 319.39 | 9.85 | .41 | 2052 |
| 19 | 685.00 | 663.00 | 612.00 | 326.82 | 326.44 | 10.09 | .39 | 2131 |
| 20 | 700.00 | 678.00 | 627.00 | 334.84 | 333.43 | 11.38 | 1.41 | 2145 |
| 21 | 715.00 | 693.00 | 642.00 | 341.86 | 340.86 | 11.08 | 1.00 | 2018 |
| 22 | 730.00 | 708.00 | 657.00 | 348.88 | 348.44 | 10.62 | .45 | 1980 |
| 23 | 745.00 | 723.00 | 672.00 | 355.90 | 355.76 | 10.41 | .14 | 2048 |
| 24 | 760.00 | 738.00 | 687.00 | 361.92 | 361.87 | 10.43 | .06 | 2458 |

| LEVEL NUMBER | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | VERTICAL DEPTH FROM GL M | VERTICAL TRAVEL TIME SRD/GEOPH MS | INTEGRATED ADJUSTED SONIC TIME MS | DRIFT = SHOT TIME - RAW SON MS | RESIDUAL = SHOT TIME - ADJ SON MS | ADJUSTED INTERVAL VELOCITY M/S |
|-----------------|--------------------------------------|---------------------------------------|--------------------------------------|---|---|--|---|---|
| 25 | 774.00 | 752.00 | 701.00 | 366.94 | 366.45 | 11.01 | .49 | 3051 |
| 26 | 790.00 | 768.00 | 717.00 | 371.97 | 371.86 | 10.79 | .11 | 2960 |
| 27 | 805.00 | 783.00 | 732.00 | 376.99 | 377.30 | 10.53 | -.31 | 2760 |
| 28 | 820.00 | 798.00 | 747.00 | 383.00 | 383.50 | 10.49 | -.50 | 2416 |
| 29 | 835.00 | 813.00 | 762.00 | 390.02 | 389.62 | 11.53 | .39 | 2452 |
| 30 | 850.00 | 828.00 | 777.00 | 395.03 | 395.30 | 11.02 | -.27 | 2641 |
| 31 | 865.00 | 843.00 | 792.00 | 401.05 | 401.25 | 11.24 | -.20 | 2524 |
| 32 | 880.00 | 858.00 | 807.00 | 407.06 | 407.48 | 11.17 | -.42 | 2405 |
| 33 | 895.00 | 873.00 | 822.00 | 414.08 | 413.45 | 12.36 | .62 | 2512 |
| 34 | 899.92 | 877.92 | 826.92 | 415.96 | 415.38 | 12.36 | .58 | 2552 |

Time / Depth

TIME/DEPTH

ANALYST: M. SANDERS

14-JUL-87 13:49:18

PROGRAM: GTRFRM 001.E12

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*   SCHLUMBERGER                     *  
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TIME CONVERTED VELOCITY REPORT

COMPANY : LASMO ENERGY
WELL : PATRICIA - 1
FIELD : WILDCAT
COUNTRY : AUSTRALIA
REFERENCE: 570705

LONG DEFINITIONS

GLOBAL

- KB - ELEVATION OF THE KELLY-BUSHING ABOVE MSL OR MWL
- SRD - ELEVATION OF THE SEISMIC REFERENCE DATUM ABOVE MSL OR MWL
- GL - ELEVATION OF USER'S REFERENCE (GENERALLY GROUND LEVEL) ABOVE SRD
- UNERTH - UNIFORM EARTH VELOCITY (GTRFRM)
- UNFDEN - UNIFORM DENSITY VALUE

MATRIX

- MVODIS - MOVE-OUT DISTANCE FROM BOREHOLE

ZONE

- LOFVEL - LAYER OPTION FLAG FOR VELOCITY: -1=NONE; 0=UNIFORM; 1=UNIFORM+LAYER
- LAYVEL - USER SUPPLIED VELOCITY DATA
- LOFDEN - LAYER OPTION FLAG FOR DENSITY : -1=NONE; 0=UNIFORM; 1=UNIFORM+LAYER
- LAYDEN - USER SUPPLIED DENSITY DATA

SAMPLED

- TWOT - TWO WAY TRAVEL TIME (RELATIVE TO THE SEISMIC REFERENCE)
- DKE - MEASURED DEPTH FROM KELLY-BUSHING
- DSRD - DEPTH FROM SRD
- AVGV - AVERAGE SEISMIC VELOCITY
- RMSV - ROOT MEAN SQUARE VELOCITY (SEISMIC)
- MVOT - NORMAL MOVE-OUT
- MVOT - NORMAL MOVE-OUT
- MVOT - NORMAL MOVE-OUT
- INTV - INTERNAL VELOCITY, AVERAGE

(GLOBAL PARAMETERS)

(VALUE)

| | | | | |
|--------------------------|--------|---|----------|------|
| ELEV OF KB AB. MSL (WST) | KB | : | 22.0000 | M |
| ELEV OF SRD AB. MSL(WST) | SRD | : | 0 | M |
| ELEV OF GL AB. SRD(WST) | GL | : | -51.0000 | M |
| UNIFORM EARTH VELOCITY | UNERTH | : | 2133.60 | M/S |
| UNIFORM DENSITY VALUE | UNFDEN | : | 2.30000 | G/C3 |

(MATRIX PARAMETERS)

MVOUT DIST

M

| | |
|---|--------|
| 1 | 1000.0 |
| 2 | 1500.0 |
| 3 | 2000.0 |

(ZONED PARAMETERS)

| | | (VALUE) | (LIMITS) | |
|--------------------------|--------|-------------|--------------|-----------|
| LAYER OPTION FLAG VELOC | LOFVEL | : 1.000000 | 30479.7 | - 0 |
| USER VELOC (WST) | LAYVEL | : 1802.000 | M/S 220.000 | - 73.0000 |
| | | 1480.000 | 73.0000 | 0 |
| LAYER OPTION FLAG DENS | LOFDEN | : -1.000000 | 30479.7 | - 0 |
| USER SUPPLIED DENSITY DA | LAYDEN | : -999.2500 | G/C3 30479.7 | - 0 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 0 | 22.00 | 0 | | | | | | 1480 |
| 2.00 | 23.48 | 1.48 | 1480 | 1480 | 673.68 | 1011.52 | 1349.35 | 1480 |
| 4.00 | 24.96 | 2.96 | 1480 | 1480 | 671.69 | 1009.52 | 1347.36 | 1480 |
| 6.00 | 26.44 | 4.44 | 1480 | 1480 | 669.70 | 1007.53 | 1345.36 | 1480 |
| 8.00 | 27.92 | 5.92 | 1480 | 1480 | 667.72 | 1005.55 | 1343.38 | 1480 |
| 10.00 | 29.40 | 7.40 | 1480 | 1480 | 665.75 | 1003.56 | 1341.39 | 1480 |
| 12.00 | 30.88 | 8.88 | 1480 | 1480 | 663.78 | 1001.58 | 1339.40 | 1480 |
| 14.00 | 32.36 | 10.36 | 1480 | 1480 | 661.82 | 999.61 | 1337.42 | 1480 |
| 16.00 | 33.84 | 11.84 | 1480 | 1480 | 659.87 | 997.64 | 1335.45 | 1480 |
| 18.00 | 35.32 | 13.32 | 1480 | 1480 | 657.92 | 995.67 | 1333.47 | 1480 |
| 20.00 | 36.80 | 14.80 | 1480 | 1480 | 655.97 | 993.71 | 1331.50 | 1480 |
| 22.00 | 38.28 | 16.28 | 1480 | 1480 | 654.03 | 991.75 | 1329.53 | 1480 |
| 24.00 | 39.76 | 17.76 | 1480 | 1480 | 652.10 | 989.80 | 1327.56 | 1480 |
| 26.00 | 41.24 | 19.24 | 1480 | 1480 | 650.18 | 987.85 | 1325.60 | 1480 |
| 28.00 | 42.72 | 20.72 | 1480 | 1480 | 648.26 | 985.90 | 1323.64 | 1480 |
| 30.00 | 44.20 | 22.20 | 1480 | 1480 | 646.34 | 983.96 | 1321.68 | 1480 |
| 32.00 | 45.68 | 23.68 | 1480 | 1480 | 644.43 | 982.02 | 1319.73 | 1480 |
| 34.00 | 47.16 | 25.16 | 1480 | 1480 | 642.53 | 980.08 | 1317.78 | 1480 |
| 36.00 | 48.64 | 26.64 | 1480 | 1480 | 640.63 | 978.15 | 1315.83 | 1480 |
| 38.00 | 50.12 | 28.12 | 1480 | 1480 | 638.74 | 976.23 | 1313.89 | 1480 |
| 40.00 | 51.60 | 29.60 | 1480 | 1480 | 636.86 | 974.30 | 1311.94 | 1480 |
| 42.00 | 53.08 | 31.08 | 1480 | 1480 | 634.98 | 972.38 | 1310.00 | 1480 |
| 44.00 | 54.56 | 32.56 | 1480 | 1480 | 633.11 | 970.47 | 1308.07 | 1480 |
| 46.00 | 56.04 | 34.04 | 1480 | 1480 | 631.24 | 968.56 | 1306.13 | 1480 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 48.00 | 57.52 | 35.52 | 1480 | 1480 | 629.38 | 966.65 | 1304.20 | 1480 |
| 50.00 | 59.00 | 37.00 | 1480 | 1480 | 627.52 | 964.75 | 1302.28 | 1480 |
| 52.00 | 60.48 | 38.48 | 1480 | 1480 | 625.67 | 962.85 | 1300.35 | 1480 |
| 54.00 | 61.96 | 39.96 | 1480 | 1480 | 623.83 | 960.95 | 1298.43 | 1480 |
| 56.00 | 63.44 | 41.44 | 1480 | 1480 | 621.99 | 959.06 | 1296.51 | 1480 |
| 58.00 | 64.92 | 42.92 | 1480 | 1480 | 620.16 | 957.17 | 1294.60 | 1480 |
| 60.00 | 66.40 | 44.40 | 1480 | 1480 | 618.33 | 955.29 | 1292.68 | 1480 |
| 62.00 | 67.88 | 45.88 | 1480 | 1480 | 616.51 | 953.41 | 1290.77 | 1480 |
| 64.00 | 69.36 | 47.36 | 1480 | 1480 | 614.70 | 951.53 | 1288.87 | 1480 |
| 66.00 | 70.84 | 48.84 | 1480 | 1480 | 612.89 | 949.66 | 1286.96 | 1480 |
| 68.00 | 72.32 | 50.32 | 1480 | 1480 | 611.09 | 947.79 | 1285.06 | 1480 |
| 70.00 | 74.00 | 52.00 | 1486 | 1486 | 606.61 | 941.89 | 1277.77 | 1675 |
| 72.00 | 75.80 | 53.80 | 1494 | 1496 | 600.48 | 933.51 | 1267.17 | 1802 |
| 74.00 | 77.60 | 55.60 | 1503 | 1505 | 594.68 | 925.61 | 1257.21 | 1802 |
| 76.00 | 79.40 | 57.40 | 1511 | 1513 | 589.17 | 918.13 | 1247.81 | 1802 |
| 78.00 | 81.20 | 59.20 | 1518 | 1521 | 583.91 | 911.03 | 1238.91 | 1802 |
| 80.00 | 83.01 | 61.01 | 1525 | 1529 | 578.89 | 904.28 | 1230.47 | 1802 |
| 82.00 | 84.81 | 62.81 | 1532 | 1536 | 574.08 | 897.84 | 1222.45 | 1802 |
| 84.00 | 86.61 | 64.61 | 1538 | 1543 | 569.46 | 891.68 | 1214.80 | 1802 |
| 86.00 | 88.41 | 66.41 | 1544 | 1550 | 565.02 | 885.79 | 1207.50 | 1802 |
| 88.00 | 90.21 | 68.21 | 1550 | 1556 | 560.75 | 880.13 | 1200.51 | 1802 |
| 90.00 | 92.02 | 70.02 | 1556 | 1562 | 556.62 | 874.70 | 1193.81 | 1802 |
| 92.00 | 93.82 | 71.82 | 1561 | 1567 | 552.63 | 869.46 | 1187.38 | 1802 |
| 94.00 | 95.62 | 73.62 | 1566 | 1573 | 548.77 | 864.41 | 1181.19 | 1802 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 96.00 | 97.42 | 75.42 | 1571 | 1578 | 545.03 | 859.53 | 1175.23 | 1802 |
| 98.00 | 99.22 | 77.22 | 1576 | 1583 | 541.39 | 854.81 | 1169.47 | 1802 |
| 100.00 | 101.02 | 79.02 | 1580 | 1587 | 537.86 | 850.24 | 1163.91 | 1802 |
| 102.00 | 102.83 | 80.83 | 1585 | 1592 | 534.43 | 845.80 | 1158.53 | 1802 |
| 104.00 | 104.63 | 82.63 | 1589 | 1596 | 531.08 | 841.50 | 1153.32 | 1802 |
| 106.00 | 106.43 | 84.43 | 1593 | 1600 | 527.82 | 837.31 | 1148.27 | 1802 |
| 108.00 | 108.23 | 86.23 | 1597 | 1604 | 524.63 | 833.24 | 1143.36 | 1802 |
| 110.00 | 110.03 | 88.03 | 1601 | 1608 | 521.52 | 829.27 | 1138.59 | 1802 |
| 112.00 | 111.84 | 89.84 | 1604 | 1612 | 518.48 | 825.39 | 1133.95 | 1802 |
| 114.00 | 113.64 | 91.64 | 1608 | 1615 | 515.51 | 821.62 | 1129.43 | 1802 |
| 116.00 | 115.44 | 93.44 | 1611 | 1619 | 512.59 | 817.93 | 1125.03 | 1802 |
| 118.00 | 117.24 | 95.24 | 1614 | 1622 | 509.74 | 814.32 | 1120.73 | 1802 |
| 120.00 | 119.04 | 97.04 | 1617 | 1625 | 506.94 | 810.79 | 1116.53 | 1802 |
| 122.00 | 120.85 | 98.85 | 1620 | 1628 | 504.19 | 807.33 | 1112.43 | 1802 |
| 124.00 | 122.65 | 100.65 | 1623 | 1631 | 501.50 | 803.94 | 1108.42 | 1802 |
| 126.00 | 124.45 | 102.45 | 1626 | 1634 | 498.85 | 800.62 | 1104.49 | 1802 |
| 128.00 | 126.25 | 104.25 | 1629 | 1637 | 496.24 | 797.37 | 1100.65 | 1802 |
| 130.00 | 128.05 | 106.05 | 1632 | 1639 | 493.68 | 794.17 | 1096.88 | 1802 |
| 132.00 | 129.86 | 107.86 | 1634 | 1642 | 491.17 | 791.03 | 1093.18 | 1802 |
| 134.00 | 131.66 | 109.66 | 1637 | 1644 | 488.69 | 787.94 | 1089.56 | 1802 |
| 136.00 | 133.46 | 111.46 | 1639 | 1647 | 486.25 | 784.90 | 1086.00 | 1802 |
| 138.00 | 135.26 | 113.26 | 1641 | 1649 | 483.84 | 781.92 | 1082.50 | 1802 |
| 140.00 | 137.06 | 115.06 | 1644 | 1652 | 481.48 | 778.98 | 1079.07 | 1802 |
| 142.00 | 138.87 | 116.87 | 1646 | 1654 | 479.14 | 776.08 | 1075.69 | 1802 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 144.00 | 140.67 | 118.67 | 1648 | 1656 | 476.84 | 773.23 | 1072.36 | 1802 |
| 146.00 | 142.47 | 120.47 | 1650 | 1658 | 474.56 | 770.42 | 1069.09 | 1802 |
| 148.00 | 144.27 | 122.27 | 1652 | 1660 | 472.32 | 767.65 | 1065.87 | 1802 |
| 150.00 | 146.07 | 124.07 | 1654 | 1662 | 470.11 | 764.92 | 1062.70 | 1802 |
| 152.00 | 147.88 | 125.88 | 1656 | 1664 | 467.92 | 762.22 | 1059.57 | 1802 |
| 154.00 | 149.68 | 127.68 | 1658 | 1666 | 465.76 | 759.56 | 1056.49 | 1802 |
| 156.00 | 151.48 | 129.48 | 1660 | 1668 | 463.63 | 756.93 | 1053.45 | 1802 |
| 158.00 | 153.28 | 131.28 | 1662 | 1669 | 461.52 | 754.34 | 1050.45 | 1802 |
| 160.00 | 155.08 | 133.08 | 1664 | 1671 | 459.44 | 751.78 | 1047.49 | 1802 |
| 162.00 | 156.89 | 134.89 | 1665 | 1673 | 457.38 | 749.24 | 1044.56 | 1802 |
| 164.00 | 158.69 | 136.69 | 1667 | 1674 | 455.34 | 746.74 | 1041.67 | 1802 |
| 166.00 | 160.49 | 138.49 | 1669 | 1676 | 453.33 | 744.26 | 1038.82 | 1802 |
| 168.00 | 162.29 | 140.29 | 1670 | 1678 | 451.33 | 741.81 | 1036.00 | 1802 |
| 170.00 | 164.09 | 142.09 | 1672 | 1679 | 449.36 | 739.39 | 1033.22 | 1802 |
| 172.00 | 165.90 | 143.90 | 1673 | 1681 | 447.41 | 737.00 | 1030.46 | 1802 |
| 174.00 | 167.70 | 145.70 | 1675 | 1682 | 445.48 | 734.62 | 1027.74 | 1802 |
| 176.00 | 169.50 | 147.50 | 1676 | 1683 | 443.56 | 732.27 | 1025.04 | 1802 |
| 178.00 | 171.30 | 149.30 | 1678 | 1685 | 441.67 | 729.95 | 1022.38 | 1802 |
| 180.00 | 173.10 | 151.10 | 1679 | 1686 | 439.79 | 727.65 | 1019.74 | 1802 |
| 182.00 | 174.91 | 152.91 | 1680 | 1687 | 437.93 | 725.37 | 1017.13 | 1802 |
| 184.00 | 176.71 | 154.71 | 1682 | 1689 | 436.09 | 723.11 | 1014.54 | 1802 |
| 186.00 | 178.51 | 156.51 | 1683 | 1690 | 434.27 | 720.87 | 1011.98 | 1802 |
| 188.00 | 180.31 | 158.31 | 1684 | 1691 | 432.46 | 718.65 | 1009.44 | 1802 |
| 190.00 | 182.11 | 160.11 | 1685 | 1692 | 430.67 | 716.45 | 1006.92 | 1802 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---------------------------------|--------------------------|---------------------------|------------------------------|------------------|-------------------------|--------------------------|-------------------------|-----------------------|
| 192.00 | 183.91 | 161.91 | 1687 | 1694 | 428.89 | 714.27 | 1004.43 | 1802 |
| 194.00 | 185.72 | 163.72 | 1688 | 1695 | 427.13 | 712.10 | 1001.96 | 1802 |
| 196.00 | 187.52 | 165.52 | 1689 | 1696 | 425.39 | 709.96 | 999.51 | 1802 |
| 198.00 | 189.32 | 167.32 | 1690 | 1697 | 423.66 | 707.83 | 997.09 | 1802 |
| 200.00 | 191.12 | 169.12 | 1691 | 1698 | 421.94 | 705.72 | 994.68 | 1802 |
| 202.00 | 192.92 | 170.92 | 1692 | 1699 | 420.24 | 703.63 | 992.29 | 1802 |
| 204.00 | 194.73 | 172.73 | 1693 | 1700 | 418.55 | 701.55 | 989.92 | 1802 |
| 206.00 | 196.53 | 174.53 | 1694 | 1701 | 416.88 | 699.49 | 987.57 | 1802 |
| 208.00 | 198.33 | 176.33 | 1695 | 1702 | 415.22 | 697.44 | 985.24 | 1802 |
| 210.00 | 200.13 | 178.13 | 1696 | 1703 | 413.57 | 695.41 | 982.93 | 1802 |
| 212.00 | 201.93 | 179.93 | 1697 | 1704 | 411.94 | 693.40 | 980.63 | 1802 |
| 214.00 | 203.74 | 181.74 | 1698 | 1705 | 410.32 | 691.40 | 978.35 | 1802 |
| 216.00 | 205.54 | 183.54 | 1699 | 1706 | 408.71 | 689.41 | 976.09 | 1802 |
| 218.00 | 207.34 | 185.34 | 1700 | 1707 | 407.11 | 687.44 | 973.84 | 1802 |
| 220.00 | 209.14 | 187.14 | 1701 | 1708 | 405.53 | 685.48 | 971.61 | 1802 |
| 222.00 | 210.94 | 188.94 | 1702 | 1709 | 403.95 | 683.53 | 969.39 | 1802 |
| 224.00 | 212.75 | 190.75 | 1703 | 1709 | 402.39 | 681.60 | 967.19 | 1802 |
| 226.00 | 214.55 | 192.55 | 1704 | 1710 | 400.84 | 679.67 | 965.00 | 1802 |
| 228.00 | 216.35 | 194.35 | 1705 | 1711 | 399.30 | 677.77 | 962.83 | 1802 |
| 230.00 | 218.15 | 196.15 | 1706 | 1712 | 397.77 | 675.87 | 960.67 | 1802 |
| 232.00 | 219.95 | 197.95 | 1707 | 1713 | 396.26 | 673.99 | 958.53 | 1802 |
| 234.00 | 222.18 | 200.18 | 1711 | 1718 | 393.42 | 670.04 | 953.59 | 2222 |
| 236.00 | 224.30 | 202.30 | 1714 | 1722 | 390.98 | 666.70 | 949.47 | 2120 |
| 238.00 | 226.54 | 204.54 | 1719 | 1727 | 388.15 | 662.75 | 944.52 | 2247 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 240.00 | 228.58 | 206.58 | 1722 | 1729 | 386.04 | 659.90 | 941.05 | 2040 |
| 242.00 | 230.80 | 208.80 | 1726 | 1734 | 383.40 | 656.24 | 936.48 | 2215 |
| 244.00 | 232.81 | 210.81 | 1728 | 1737 | 381.41 | 653.58 | 933.27 | 2016 |
| 246.00 | 234.91 | 212.91 | 1731 | 1740 | 379.21 | 650.57 | 929.58 | 2099 |
| 248.00 | 237.06 | 215.06 | 1734 | 1743 | 376.90 | 647.41 | 925.67 | 2142 |
| 250.00 | 239.13 | 217.13 | 1737 | 1746 | 374.83 | 644.60 | 922.24 | 2073 |
| 252.00 | 241.27 | 219.27 | 1740 | 1750 | 372.60 | 641.53 | 918.46 | 2139 |
| 254.00 | 243.50 | 221.50 | 1744 | 1754 | 370.13 | 638.09 | 914.17 | 2229 |
| 256.00 | 245.63 | 223.63 | 1747 | 1757 | 367.97 | 635.12 | 910.51 | 2136 |
| 258.00 | 247.68 | 225.68 | 1749 | 1760 | 366.06 | 632.54 | 907.39 | 2053 |
| 260.00 | 249.90 | 227.90 | 1753 | 1764 | 363.73 | 629.29 | 903.34 | 2217 |
| 262.00 | 252.05 | 230.05 | 1756 | 1767 | 361.62 | 626.38 | 899.75 | 2148 |
| 264.00 | 254.22 | 232.22 | 1759 | 1770 | 359.47 | 623.41 | 896.08 | 2172 |
| 266.00 | 256.49 | 234.49 | 1763 | 1775 | 357.09 | 620.06 | 891.89 | 2270 |
| 268.00 | 258.74 | 236.74 | 1767 | 1779 | 354.81 | 616.86 | 887.89 | 2246 |
| 270.00 | 261.02 | 239.02 | 1771 | 1783 | 352.47 | 613.56 | 883.76 | 2281 |
| 272.00 | 263.32 | 241.32 | 1774 | 1787 | 350.12 | 610.24 | 879.60 | 2297 |
| 274.00 | 265.67 | 243.67 | 1779 | 1792 | 347.64 | 606.71 | 875.15 | 2358 |
| 276.00 | 268.09 | 246.09 | 1783 | 1797 | 345.05 | 602.99 | 870.43 | 2416 |
| 278.00 | 270.55 | 248.55 | 1788 | 1803 | 342.40 | 599.16 | 865.55 | 2457 |
| 280.00 | 272.92 | 250.92 | 1792 | 1808 | 340.00 | 595.73 | 861.23 | 2375 |
| 282.00 | 275.23 | 253.23 | 1796 | 1812 | 337.82 | 592.63 | 857.35 | 2305 |
| 284.00 | 277.70 | 255.70 | 1801 | 1817 | 335.25 | 588.91 | 852.61 | 2473 |
| 286.00 | 279.98 | 257.98 | 1804 | 1821 | 333.18 | 586.00 | 848.97 | 2282 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 288.00 | 282.21 | 260.21 | 1807 | 1824 | 331.27 | 583.31 | 845.64 | 2230 |
| 290.00 | 284.57 | 262.57 | 1811 | 1828 | 329.09 | 580.20 | 841.73 | 2353 |
| 292.00 | 286.80 | 264.80 | 1814 | 1831 | 327.21 | 577.55 | 838.44 | 2239 |
| 294.00 | 289.07 | 267.07 | 1817 | 1835 | 325.29 | 574.84 | 835.07 | 2264 |
| 296.00 | 291.23 | 269.23 | 1819 | 1837 | 323.62 | 572.52 | 832.23 | 2159 |
| 298.00 | 293.51 | 271.51 | 1822 | 1840 | 321.71 | 569.81 | 828.83 | 2284 |
| 300.00 | 295.60 | 273.60 | 1824 | 1842 | 320.21 | 567.75 | 826.35 | 2091 |
| 302.00 | 297.76 | 275.76 | 1826 | 1844 | 318.61 | 565.52 | 823.61 | 2155 |
| 304.00 | 299.87 | 277.87 | 1828 | 1846 | 317.10 | 563.45 | 821.09 | 2109 |
| 306.00 | 301.94 | 279.94 | 1830 | 1848 | 315.69 | 561.51 | 818.76 | 2071 |
| 308.00 | 304.09 | 282.09 | 1832 | 1850 | 314.13 | 559.33 | 816.09 | 2154 |
| 310.00 | 306.12 | 284.12 | 1833 | 1851 | 312.82 | 557.55 | 813.96 | 2028 |
| 312.00 | 308.21 | 286.21 | 1835 | 1853 | 311.40 | 555.60 | 811.60 | 2091 |
| 314.00 | 310.32 | 288.32 | 1836 | 1855 | 309.97 | 553.62 | 809.20 | 2106 |
| 316.00 | 312.48 | 290.48 | 1839 | 1857 | 308.44 | 551.48 | 806.57 | 2166 |
| 318.00 | 314.64 | 292.64 | 1840 | 1859 | 306.95 | 549.39 | 804.00 | 2155 |
| 320.00 | 316.76 | 294.76 | 1842 | 1861 | 305.53 | 547.41 | 801.58 | 2126 |
| 322.00 | 318.91 | 296.91 | 1844 | 1862 | 304.08 | 545.38 | 799.09 | 2148 |
| 324.00 | 321.01 | 299.01 | 1846 | 1864 | 302.73 | 543.50 | 796.81 | 2099 |
| 326.00 | 323.15 | 301.15 | 1848 | 1866 | 301.31 | 541.52 | 794.39 | 2142 |
| 328.00 | 325.33 | 303.33 | 1850 | 1868 | 299.85 | 539.45 | 791.85 | 2176 |
| 330.00 | 327.46 | 305.46 | 1851 | 1870 | 298.49 | 537.54 | 789.51 | 2128 |
| 332.00 | 329.62 | 307.62 | 1853 | 1871 | 297.08 | 535.54 | 787.05 | 2166 |
| 334.00 | 331.73 | 309.73 | 1855 | 1873 | 295.78 | 533.73 | 784.84 | 2103 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| | | | | | | | | 2093 |
| 336.00 | 333.82 | 311.82 | 1856 | 1874 | 294.51 | 531.95 | 782.69 | 2123 |
| 338.00 | 335.94 | 313.94 | 1858 | 1876 | 293.20 | 530.11 | 780.44 | 2108 |
| 340.00 | 338.05 | 316.05 | 1859 | 1877 | 291.92 | 528.33 | 778.26 | 2088 |
| 342.00 | 340.14 | 318.14 | 1860 | 1879 | 290.69 | 526.60 | 776.17 | 2008 |
| 344.00 | 342.15 | 320.15 | 1861 | 1879 | 289.59 | 525.09 | 774.36 | 2138 |
| 346.00 | 344.28 | 322.28 | 1863 | 1881 | 288.30 | 523.26 | 772.12 | 2303 |
| 348.00 | 346.59 | 324.59 | 1865 | 1884 | 286.76 | 521.01 | 769.30 | 2282 |
| 350.00 | 348.87 | 326.87 | 1868 | 1886 | 285.27 | 518.84 | 766.58 | 2567 |
| 352.00 | 351.44 | 329.44 | 1872 | 1891 | 283.30 | 515.90 | 762.78 | 2333 |
| 354.00 | 353.77 | 331.77 | 1874 | 1894 | 281.77 | 513.64 | 759.94 | 2406 |
| 356.00 | 356.17 | 334.17 | 1877 | 1897 | 280.13 | 511.22 | 756.85 | 2332 |
| 358.00 | 358.51 | 336.51 | 1880 | 1900 | 278.63 | 509.02 | 754.07 | 2531 |
| 360.00 | 361.04 | 339.04 | 1884 | 1904 | 276.83 | 506.30 | 750.58 | 2230 |
| 362.00 | 363.27 | 341.27 | 1885 | 1906 | 275.52 | 504.40 | 748.21 | 2289 |
| 364.00 | 365.55 | 343.55 | 1888 | 1908 | 274.13 | 502.37 | 745.66 | 2668 |
| 366.00 | 368.22 | 346.22 | 1892 | 1913 | 272.15 | 499.36 | 741.74 | 2239 |
| 368.00 | 370.46 | 348.46 | 1894 | 1915 | 270.87 | 497.50 | 739.42 | 2308 |
| 370.00 | 372.77 | 350.77 | 1896 | 1917 | 269.51 | 495.48 | 736.88 | 2163 |
| 372.00 | 374.93 | 352.93 | 1897 | 1919 | 268.36 | 493.82 | 734.83 | 2217 |
| 374.00 | 377.15 | 355.15 | 1899 | 1920 | 267.14 | 492.05 | 732.63 | 2273 |
| 376.00 | 379.42 | 357.42 | 1901 | 1922 | 265.86 | 490.17 | 730.26 | 2156 |
| 378.00 | 381.58 | 359.58 | 1903 | 1924 | 264.75 | 488.56 | 728.28 | 2151 |
| 380.00 | 383.73 | 361.73 | 1904 | 1925 | 263.65 | 486.97 | 726.32 | 2101 |
| 382.00 | 385.83 | 363.83 | 1905 | 1926 | 262.62 | 485.50 | 724.52 | |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 384.00 | 387.93 | 365.93 | 1906 | 1927 | 261.61 | 484.05 | 722.75 | 2094 |
| 386.00 | 390.08 | 368.08 | 1907 | 1928 | 260.53 | 482.49 | 720.82 | 2154 |
| 388.00 | 392.19 | 370.19 | 1908 | 1929 | 259.51 | 481.01 | 719.00 | 2116 |
| 390.00 | 394.44 | 372.44 | 1910 | 1931 | 258.34 | 479.29 | 716.84 | 2241 |
| 392.00 | 396.52 | 374.52 | 1911 | 1932 | 257.38 | 477.90 | 715.14 | 2081 |
| 394.00 | 398.65 | 376.65 | 1912 | 1933 | 256.35 | 476.41 | 713.30 | 2138 |
| 396.00 | 400.77 | 378.77 | 1913 | 1934 | 255.36 | 474.96 | 711.52 | 2119 |
| 398.00 | 402.77 | 380.77 | 1913 | 1934 | 254.50 | 473.75 | 710.07 | 1999 |
| 400.00 | 404.93 | 382.93 | 1915 | 1935 | 253.47 | 472.24 | 708.19 | 2162 |
| 402.00 | 407.30 | 385.30 | 1917 | 1938 | 252.19 | 470.31 | 705.73 | 2366 |
| 404.00 | 409.79 | 387.79 | 1920 | 1941 | 250.77 | 468.13 | 702.91 | 2490 |
| 406.00 | 411.79 | 389.79 | 1920 | 1941 | 249.94 | 466.95 | 701.49 | 2003 |
| 408.00 | 413.86 | 391.86 | 1921 | 1942 | 249.05 | 465.66 | 699.92 | 2063 |
| 410.00 | 415.98 | 393.98 | 1922 | 1943 | 248.11 | 464.27 | 698.20 | 2122 |
| 412.00 | 418.06 | 396.06 | 1923 | 1943 | 247.21 | 462.97 | 696.60 | 2083 |
| 414.00 | 420.11 | 398.11 | 1923 | 1944 | 246.35 | 461.73 | 695.09 | 2046 |
| 416.00 | 422.26 | 400.26 | 1924 | 1945 | 245.39 | 460.31 | 693.32 | 2153 |
| 418.00 | 424.50 | 402.50 | 1926 | 1946 | 244.35 | 458.74 | 691.34 | 2233 |
| 420.00 | 426.63 | 404.63 | 1927 | 1947 | 243.42 | 457.37 | 689.64 | 2134 |
| 422.00 | 428.57 | 406.57 | 1927 | 1947 | 242.69 | 456.34 | 688.41 | 1941 |
| 424.00 | 430.76 | 408.76 | 1928 | 1948 | 241.71 | 454.88 | 686.57 | 2194 |
| 426.00 | 433.30 | 411.30 | 1931 | 1952 | 240.35 | 452.75 | 683.80 | 2535 |
| 428.00 | 435.48 | 413.48 | 1932 | 1953 | 239.40 | 451.33 | 682.01 | 2184 |
| 430.00 | 437.50 | 415.50 | 1933 | 1953 | 238.62 | 450.20 | 680.64 | 2016 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 432.00 | 439.55 | 417.55 | 1933 | 1954 | 237.82 | 449.02 | 679.19 | 2053 |
| 434.00 | 441.62 | 419.62 | 1934 | 1954 | 237.00 | 447.82 | 677.71 | 2066 |
| 436.00 | 443.63 | 421.63 | 1934 | 1954 | 236.24 | 446.71 | 676.36 | 2012 |
| 438.00 | 445.66 | 423.66 | 1935 | 1955 | 235.47 | 445.59 | 674.99 | 2027 |
| 440.00 | 447.71 | 425.71 | 1935 | 1955 | 234.68 | 444.42 | 673.55 | 2057 |
| 442.00 | 449.93 | 427.93 | 1936 | 1956 | 233.74 | 442.98 | 671.73 | 2219 |
| 444.00 | 452.15 | 430.15 | 1938 | 1958 | 232.80 | 441.55 | 669.91 | 2221 |
| 446.00 | 454.44 | 432.44 | 1939 | 1959 | 231.80 | 440.02 | 667.96 | 2283 |
| 448.00 | 456.68 | 434.68 | 1941 | 1961 | 230.85 | 438.56 | 666.10 | 2247 |
| 450.00 | 458.91 | 436.91 | 1942 | 1962 | 229.92 | 437.15 | 664.31 | 2225 |
| 452.00 | 461.08 | 439.08 | 1943 | 1963 | 229.06 | 435.84 | 662.65 | 2172 |
| 454.00 | 463.25 | 441.25 | 1944 | 1964 | 228.21 | 434.55 | 661.03 | 2163 |
| 456.00 | 465.81 | 443.81 | 1947 | 1967 | 226.95 | 432.56 | 658.40 | 2566 |
| 458.00 | 468.10 | 446.10 | 1948 | 1968 | 226.00 | 431.09 | 656.51 | 2288 |
| 460.00 | 470.46 | 448.46 | 1950 | 1970 | 224.99 | 429.50 | 654.46 | 2358 |
| 462.00 | 472.73 | 450.73 | 1951 | 1972 | 224.06 | 428.06 | 652.62 | 2277 |
| 464.00 | 474.94 | 452.94 | 1952 | 1973 | 223.21 | 426.76 | 650.96 | 2202 |
| 466.00 | 477.02 | 455.02 | 1953 | 1973 | 222.46 | 425.64 | 649.55 | 2088 |
| 468.00 | 479.17 | 457.17 | 1954 | 1974 | 221.67 | 424.43 | 648.03 | 2148 |
| 470.00 | 481.30 | 459.30 | 1954 | 1975 | 220.90 | 423.26 | 646.56 | 2125 |
| 472.00 | 483.63 | 461.63 | 1956 | 1976 | 219.96 | 421.78 | 644.64 | 2331 |
| 474.00 | 485.80 | 463.80 | 1957 | 1977 | 219.16 | 420.55 | 643.08 | 2171 |
| 476.00 | 488.09 | 466.09 | 1958 | 1979 | 218.27 | 419.15 | 641.28 | 2290 |
| 478.00 | 490.39 | 468.39 | 1960 | 1980 | 217.37 | 417.74 | 639.45 | 2303 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 480.00 | 492.74 | 470.74 | 1961 | 1982 | 216.43 | 416.27 | 637.53 | 2350 |
| 482.00 | 494.94 | 472.94 | 1962 | 1983 | 215.64 | 415.04 | 635.96 | 2199 |
| 484.00 | 497.10 | 475.10 | 1963 | 1983 | 214.88 | 413.86 | 634.47 | 2161 |
| 486.00 | 499.28 | 477.28 | 1964 | 1984 | 214.11 | 412.67 | 632.95 | 2181 |
| 488.00 | 501.52 | 479.52 | 1965 | 1985 | 213.30 | 411.40 | 631.32 | 2235 |
| 490.00 | 503.69 | 481.69 | 1966 | 1986 | 212.55 | 410.24 | 629.84 | 2168 |
| 492.00 | 505.81 | 483.81 | 1967 | 1987 | 211.84 | 409.14 | 628.44 | 2129 |
| 494.00 | 507.92 | 485.92 | 1967 | 1987 | 211.15 | 408.08 | 627.09 | 2105 |
| 496.00 | 510.13 | 488.13 | 1968 | 1988 | 210.39 | 406.88 | 625.55 | 2207 |
| 498.00 | 512.50 | 490.50 | 1970 | 1990 | 209.49 | 405.45 | 623.68 | 2371 |
| 500.00 | 514.75 | 492.75 | 1971 | 1991 | 208.70 | 404.20 | 622.06 | 2253 |
| 502.00 | 516.91 | 494.91 | 1972 | 1992 | 207.99 | 403.09 | 620.64 | 2155 |
| 504.00 | 519.26 | 497.26 | 1973 | 1993 | 207.13 | 401.71 | 618.84 | 2351 |
| 506.00 | 521.65 | 499.65 | 1975 | 1995 | 206.24 | 400.28 | 616.96 | 2394 |
| 508.00 | 523.94 | 501.94 | 1976 | 1996 | 205.44 | 399.01 | 615.30 | 2293 |
| 510.00 | 526.16 | 504.16 | 1977 | 1997 | 204.71 | 397.85 | 613.80 | 2212 |
| 512.00 | 528.49 | 506.49 | 1978 | 1999 | 203.89 | 396.54 | 612.08 | 2330 |
| 514.00 | 530.83 | 508.83 | 1980 | 2000 | 203.07 | 395.21 | 610.34 | 2345 |
| 516.00 | 533.23 | 511.23 | 1982 | 2002 | 202.21 | 393.82 | 608.50 | 2399 |
| 518.00 | 535.95 | 513.95 | 1984 | 2005 | 201.07 | 391.94 | 605.97 | 2725 |
| 520.00 | 538.36 | 516.36 | 1986 | 2007 | 200.22 | 390.56 | 604.14 | 2407 |
| 522.00 | 540.64 | 518.64 | 1987 | 2008 | 199.48 | 389.37 | 602.58 | 2279 |
| 524.00 | 542.91 | 520.91 | 1988 | 2009 | 198.75 | 388.19 | 601.04 | 2268 |
| 526.00 | 545.46 | 523.46 | 1990 | 2011 | 197.80 | 386.64 | 598.96 | 2548 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 528.00 | 547.85 | 525.85 | 1992 | 2013 | 196.99 | 385.32 | 597.21 | 2390 |
| 530.00 | 550.71 | 528.71 | 1995 | 2017 | 195.79 | 383.30 | 594.46 | 2865 |
| 532.00 | 553.36 | 531.36 | 1998 | 2019 | 194.80 | 381.65 | 592.23 | 2644 |
| 534.00 | 555.57 | 533.57 | 1998 | 2020 | 194.14 | 380.59 | 590.85 | 2213 |
| 536.00 | 557.96 | 535.96 | 2000 | 2022 | 193.35 | 379.30 | 589.14 | 2395 |
| 538.00 | 560.32 | 538.32 | 2001 | 2023 | 192.60 | 378.07 | 587.51 | 2361 |
| 540.00 | 562.51 | 540.51 | 2002 | 2024 | 191.97 | 377.06 | 586.19 | 2189 |
| 542.00 | 564.61 | 542.61 | 2002 | 2024 | 191.40 | 376.16 | 585.03 | 2096 |
| 544.00 | 566.79 | 544.79 | 2003 | 2025 | 190.78 | 375.16 | 583.74 | 2179 |
| 546.00 | 569.09 | 547.09 | 2004 | 2026 | 190.08 | 374.03 | 582.24 | 2304 |
| 548.00 | 571.57 | 549.57 | 2006 | 2027 | 189.27 | 372.68 | 580.43 | 2476 |
| 550.00 | 573.73 | 551.73 | 2006 | 2028 | 188.68 | 371.72 | 579.19 | 2163 |
| 552.00 | 576.34 | 554.34 | 2008 | 2030 | 187.78 | 370.21 | 577.14 | 2611 |
| 554.00 | 578.58 | 556.58 | 2009 | 2031 | 187.14 | 369.18 | 575.78 | 2242 |
| 556.00 | 580.83 | 558.83 | 2010 | 2032 | 186.51 | 368.14 | 574.42 | 2246 |
| 558.00 | 582.99 | 560.99 | 2011 | 2033 | 185.93 | 367.21 | 573.20 | 2164 |
| 560.00 | 585.26 | 563.26 | 2012 | 2033 | 185.29 | 366.16 | 571.82 | 2265 |
| 562.00 | 587.50 | 565.50 | 2012 | 2034 | 184.67 | 365.14 | 570.48 | 2246 |
| 564.00 | 589.80 | 567.80 | 2013 | 2035 | 184.01 | 364.07 | 569.06 | 2298 |
| 566.00 | 592.57 | 570.57 | 2016 | 2038 | 183.04 | 362.41 | 566.78 | 2768 |
| 568.00 | 594.69 | 572.69 | 2017 | 2039 | 182.51 | 361.55 | 565.66 | 2119 |
| 570.00 | 596.60 | 574.60 | 2016 | 2038 | 182.09 | 360.89 | 564.84 | 1913 |
| 572.00 | 598.59 | 576.59 | 2016 | 2038 | 181.63 | 360.17 | 563.91 | 1991 |
| 574.00 | 600.71 | 578.71 | 2016 | 2038 | 181.11 | 359.32 | 562.81 | 2112 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 576.00 | 602.77 | 580.77 | 2017 | 2038 | 180.62 | 358.52 | 561.78 | 2067 |
| 578.00 | 604.69 | 582.69 | 2016 | 2038 | 180.20 | 357.87 | 560.97 | 1915 |
| 580.00 | 606.79 | 584.79 | 2017 | 2038 | 179.69 | 357.05 | 559.89 | 2102 |
| 582.00 | 609.20 | 587.20 | 2018 | 2039 | 179.01 | 355.90 | 558.34 | 2407 |
| 584.00 | 611.17 | 589.17 | 2018 | 2039 | 178.57 | 355.20 | 557.45 | 1977 |
| 586.00 | 613.48 | 591.48 | 2019 | 2040 | 177.95 | 354.17 | 556.07 | 2308 |
| 588.00 | 615.78 | 593.78 | 2020 | 2041 | 177.35 | 353.16 | 554.72 | 2295 |
| 590.00 | 618.09 | 596.09 | 2021 | 2042 | 176.73 | 352.12 | 553.33 | 2319 |
| 592.00 | 620.54 | 598.54 | 2022 | 2044 | 176.04 | 350.96 | 551.75 | 2446 |
| 594.00 | 622.70 | 600.70 | 2023 | 2044 | 175.52 | 350.10 | 550.62 | 2159 |
| 596.00 | 624.96 | 602.96 | 2023 | 2045 | 174.96 | 349.15 | 549.36 | 2257 |
| 598.00 | 627.21 | 605.21 | 2024 | 2046 | 174.39 | 348.21 | 548.09 | 2258 |
| 600.00 | 629.61 | 607.61 | 2025 | 2047 | 173.75 | 347.12 | 546.62 | 2396 |
| 602.00 | 631.88 | 609.88 | 2026 | 2048 | 173.18 | 346.18 | 545.36 | 2266 |
| 604.00 | 634.15 | 612.15 | 2027 | 2048 | 172.62 | 345.23 | 544.08 | 2277 |
| 606.00 | 636.28 | 614.28 | 2027 | 2049 | 172.14 | 344.43 | 543.03 | 2126 |
| 608.00 | 638.41 | 616.41 | 2028 | 2049 | 171.66 | 343.64 | 541.98 | 2126 |
| 610.00 | 640.53 | 618.53 | 2028 | 2049 | 171.18 | 342.84 | 540.94 | 2126 |
| 612.00 | 642.66 | 620.66 | 2028 | 2049 | 170.70 | 342.06 | 539.90 | 2126 |
| 614.00 | 644.73 | 622.73 | 2028 | 2050 | 170.26 | 341.32 | 538.93 | 2074 |
| 616.00 | 646.82 | 624.82 | 2029 | 2050 | 169.80 | 340.57 | 537.94 | 2090 |
| 618.00 | 648.80 | 626.80 | 2028 | 2049 | 169.40 | 339.92 | 537.09 | 1982 |
| 620.00 | 650.80 | 628.80 | 2028 | 2049 | 169.00 | 339.25 | 536.23 | 2000 |
| 622.00 | 652.82 | 630.82 | 2028 | 2049 | 168.59 | 338.57 | 535.35 | 2015 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 624.00 | 654.84 | 632.84 | 2028 | 2049 | 168.17 | 337.90 | 534.46 | 2020 |
| 626.00 | 656.90 | 634.90 | 2028 | 2049 | 167.74 | 337.18 | 533.52 | 2066 |
| 628.00 | 658.94 | 636.94 | 2028 | 2049 | 167.33 | 336.49 | 532.61 | 2039 |
| 630.00 | 660.96 | 638.96 | 2028 | 2049 | 166.92 | 335.82 | 531.73 | 2020 |
| 632.00 | 662.93 | 640.93 | 2028 | 2049 | 166.54 | 335.19 | 530.92 | 1964 |
| 634.00 | 665.02 | 643.02 | 2028 | 2049 | 166.10 | 334.47 | 529.96 | 2092 |
| 636.00 | 667.10 | 645.10 | 2029 | 2049 | 165.68 | 333.75 | 529.01 | 2076 |
| 638.00 | 669.15 | 647.15 | 2029 | 2049 | 165.26 | 333.06 | 528.09 | 2059 |
| 640.00 | 671.34 | 649.34 | 2029 | 2049 | 164.78 | 332.25 | 527.01 | 2188 |
| 642.00 | 673.55 | 651.55 | 2030 | 2050 | 164.30 | 331.43 | 525.90 | 2210 |
| 644.00 | 675.64 | 653.64 | 2030 | 2050 | 163.88 | 330.72 | 524.96 | 2084 |
| 646.00 | 677.67 | 655.67 | 2030 | 2050 | 163.48 | 330.06 | 524.08 | 2032 |
| 648.00 | 679.67 | 657.67 | 2030 | 2050 | 163.10 | 329.42 | 523.25 | 2002 |
| 650.00 | 681.76 | 659.76 | 2030 | 2050 | 162.68 | 328.71 | 522.30 | 2094 |
| 652.00 | 684.08 | 662.08 | 2031 | 2051 | 162.16 | 327.81 | 521.07 | 2317 |
| 654.00 | 686.28 | 664.28 | 2031 | 2051 | 161.69 | 327.02 | 520.00 | 2194 |
| 656.00 | 688.42 | 666.42 | 2032 | 2052 | 161.26 | 326.28 | 519.00 | 2146 |
| 658.00 | 690.54 | 668.54 | 2032 | 2052 | 160.83 | 325.56 | 518.04 | 2117 |
| 660.00 | 692.67 | 670.67 | 2032 | 2052 | 160.41 | 324.83 | 517.06 | 2135 |
| 662.00 | 694.81 | 672.81 | 2033 | 2052 | 159.98 | 324.11 | 516.08 | 2137 |
| 664.00 | 696.88 | 674.88 | 2033 | 2052 | 159.58 | 323.44 | 515.18 | 2070 |
| 666.00 | 699.07 | 677.07 | 2033 | 2053 | 159.14 | 322.67 | 514.14 | 2189 |
| 668.00 | 701.35 | 679.35 | 2034 | 2054 | 158.65 | 321.83 | 512.99 | 2279 |
| 670.00 | 703.29 | 681.29 | 2034 | 2053 | 158.32 | 321.27 | 512.25 | 1940 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 672.00 | 705.27 | 683.27 | 2034 | 2053 | 157.96 | 320.67 | 511.47 | 1984 |
| 674.00 | 707.27 | 685.27 | 2033 | 2053 | 157.61 | 320.07 | 510.67 | 1994 |
| 676.00 | 709.23 | 687.23 | 2033 | 2053 | 157.26 | 319.50 | 509.91 | 1967 |
| 678.00 | 711.20 | 689.20 | 2033 | 2052 | 156.92 | 318.92 | 509.14 | 1969 |
| 680.00 | 713.20 | 691.20 | 2033 | 2052 | 156.57 | 318.32 | 508.35 | 1993 |
| 682.00 | 715.31 | 693.31 | 2033 | 2052 | 156.17 | 317.64 | 507.42 | 2117 |
| 684.00 | 717.27 | 695.27 | 2033 | 2052 | 155.83 | 317.07 | 506.68 | 1958 |
| 686.00 | 719.26 | 697.26 | 2033 | 2052 | 155.49 | 316.49 | 505.90 | 1988 |
| 688.00 | 721.37 | 699.37 | 2033 | 2052 | 155.10 | 315.82 | 504.99 | 2108 |
| 690.00 | 723.39 | 701.39 | 2033 | 2052 | 154.74 | 315.21 | 504.17 | 2024 |
| 692.00 | 725.29 | 703.29 | 2033 | 2052 | 154.43 | 314.69 | 503.49 | 1903 |
| 694.00 | 727.19 | 705.19 | 2032 | 2051 | 154.13 | 314.18 | 502.81 | 1901 |
| 696.00 | 729.15 | 707.15 | 2032 | 2051 | 153.80 | 313.62 | 502.07 | 1960 |
| 698.00 | 731.15 | 709.15 | 2032 | 2051 | 153.46 | 313.04 | 501.29 | 2001 |
| 700.00 | 733.09 | 711.09 | 2032 | 2050 | 153.14 | 312.50 | 500.58 | 1936 |
| 702.00 | 735.07 | 713.07 | 2032 | 2050 | 152.81 | 311.93 | 499.82 | 1981 |
| 704.00 | 737.04 | 715.04 | 2031 | 2050 | 152.48 | 311.38 | 499.08 | 1966 |
| 706.00 | 739.11 | 717.11 | 2031 | 2050 | 152.12 | 310.75 | 498.23 | 2073 |
| 708.00 | 741.40 | 719.40 | 2032 | 2051 | 151.67 | 309.95 | 497.12 | 2292 |
| 710.00 | 743.46 | 721.46 | 2032 | 2051 | 151.31 | 309.34 | 496.29 | 2060 |
| 712.00 | 745.51 | 723.51 | 2032 | 2051 | 150.96 | 308.73 | 495.47 | 2051 |
| 714.00 | 747.57 | 725.57 | 2032 | 2051 | 150.61 | 308.12 | 494.63 | 2061 |
| 716.00 | 749.63 | 727.63 | 2032 | 2051 | 150.26 | 307.52 | 493.81 | 2057 |
| 718.00 | 752.10 | 730.10 | 2034 | 2052 | 149.74 | 306.59 | 492.50 | 2469 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 720.00 | 754.58 | 732.58 | 2035 | 2053 | 149.22 | 305.66 | 491.19 | 2478 |
| 722.00 | 757.30 | 735.30 | 2037 | 2056 | 148.59 | 304.52 | 489.56 | 2726 |
| 724.00 | 760.50 | 738.50 | 2040 | 2060 | 147.72 | 302.92 | 487.23 | 3194 |
| 726.00 | 763.77 | 741.77 | 2043 | 2064 | 146.82 | 301.25 | 484.79 | 3277 |
| 728.00 | 766.84 | 744.84 | 2046 | 2067 | 146.04 | 299.81 | 482.72 | 3064 |
| 730.00 | 769.83 | 747.83 | 2049 | 2071 | 145.31 | 298.46 | 480.76 | 2995 |
| 732.00 | 772.74 | 750.74 | 2051 | 2073 | 144.62 | 297.21 | 478.95 | 2909 |
| 734.00 | 775.66 | 753.66 | 2054 | 2076 | 143.94 | 295.96 | 477.14 | 2915 |
| 736.00 | 778.67 | 756.67 | 2056 | 2079 | 143.22 | 294.62 | 475.20 | 3016 |
| 738.00 | 781.52 | 759.52 | 2058 | 2082 | 142.58 | 293.45 | 473.51 | 2846 |
| 740.00 | 784.53 | 762.53 | 2061 | 2085 | 141.87 | 292.15 | 471.61 | 3009 |
| 742.00 | 787.42 | 765.42 | 2063 | 2087 | 141.23 | 290.96 | 469.89 | 2894 |
| 744.00 | 790.47 | 768.47 | 2066 | 2090 | 140.52 | 289.64 | 467.97 | 3045 |
| 746.00 | 793.45 | 771.45 | 2068 | 2093 | 139.84 | 288.40 | 466.16 | 2979 |
| 748.00 | 796.53 | 774.53 | 2071 | 2097 | 139.13 | 287.07 | 464.22 | 3083 |
| 750.00 | 799.59 | 777.59 | 2074 | 2100 | 138.43 | 285.77 | 462.32 | 3064 |
| 752.00 | 801.94 | 779.94 | 2074 | 2100 | 138.03 | 285.06 | 461.32 | 2344 |
| 754.00 | 804.28 | 782.28 | 2075 | 2101 | 137.64 | 284.35 | 460.31 | 2343 |
| 756.00 | 806.81 | 784.81 | 2076 | 2102 | 137.19 | 283.51 | 459.12 | 2526 |
| 758.00 | 809.34 | 787.34 | 2077 | 2104 | 136.73 | 282.68 | 457.92 | 2534 |
| 760.00 | 811.87 | 789.87 | 2079 | 2105 | 136.27 | 281.84 | 456.73 | 2534 |
| 762.00 | 814.21 | 792.21 | 2079 | 2106 | 135.89 | 281.16 | 455.75 | 2335 |
| 764.00 | 816.52 | 794.52 | 2080 | 2106 | 135.52 | 280.49 | 454.81 | 2312 |
| 766.00 | 818.78 | 796.78 | 2080 | 2106 | 135.18 | 279.86 | 453.92 | 2253 |

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 768.00 | 821.23 | 799.23 | 2081 | 2107 | 134.76 | 279.10 | 452.83 | 2459 |
| 770.00 | 823.51 | 801.51 | 2082 | 2108 | 134.41 | 278.46 | 451.93 | 2275 |
| 772.00 | 825.95 | 803.95 | 2083 | 2109 | 134.00 | 277.72 | 450.87 | 2441 |
| 774.00 | 828.53 | 806.53 | 2084 | 2110 | 133.55 | 276.88 | 449.66 | 2580 |
| 776.00 | 831.04 | 809.04 | 2085 | 2111 | 133.12 | 276.10 | 448.53 | 2511 |
| 778.00 | 833.48 | 811.48 | 2086 | 2112 | 132.72 | 275.37 | 447.48 | 2444 |
| 780.00 | 835.94 | 813.94 | 2087 | 2113 | 132.32 | 274.63 | 446.42 | 2457 |
| 782.00 | 838.36 | 816.36 | 2088 | 2114 | 131.93 | 273.92 | 445.41 | 2416 |
| 784.00 | 841.06 | 819.06 | 2089 | 2116 | 131.45 | 273.02 | 444.10 | 2703 |
| 786.00 | 843.77 | 821.77 | 2091 | 2117 | 130.96 | 272.11 | 442.78 | 2710 |
| 788.00 | 846.58 | 824.58 | 2093 | 2120 | 130.45 | 271.15 | 441.37 | 2807 |
| 790.00 | 849.23 | 827.23 | 2094 | 2121 | 129.99 | 270.30 | 440.13 | 2655 |
| 792.00 | 851.83 | 829.83 | 2096 | 2122 | 129.56 | 269.49 | 438.96 | 2594 |
| 794.00 | 854.38 | 832.38 | 2097 | 2124 | 129.14 | 268.72 | 437.84 | 2556 |
| 796.00 | 856.92 | 834.92 | 2098 | 2125 | 128.73 | 267.96 | 436.74 | 2540 |
| 798.00 | 859.37 | 837.37 | 2099 | 2126 | 128.35 | 267.27 | 435.74 | 2450 |
| 800.00 | 861.89 | 839.89 | 2100 | 2127 | 127.96 | 266.53 | 434.67 | 2517 |
| 802.00 | 864.41 | 842.41 | 2101 | 2128 | 127.56 | 265.79 | 433.61 | 2526 |
| 804.00 | 866.89 | 844.89 | 2102 | 2129 | 127.18 | 265.09 | 432.59 | 2479 |
| 806.00 | 869.28 | 847.28 | 2102 | 2129 | 126.83 | 264.45 | 431.66 | 2383 |
| 808.00 | 871.82 | 849.82 | 2104 | 2130 | 126.44 | 263.71 | 430.59 | 2541 |
| 810.00 | 874.39 | 852.39 | 2105 | 2132 | 126.04 | 262.96 | 429.50 | 2574 |
| 812.00 | 876.53 | 854.53 | 2105 | 2132 | 125.77 | 262.47 | 428.80 | 2137 |
| 814.00 | 878.82 | 856.82 | 2105 | 2132 | 125.45 | 261.89 | 427.98 | 2290 |

COMPANY : LASMO ENERGY

WELL : PATRICIA - 1

PAGE 20

| TWO-WAY TRAVEL TIME FROM SRD MS | MEASURED DEPTH FROM KB M | VERTICAL DEPTH FROM SRD M | AVERAGE VELOCITY SRD/GEO M/S | RMS VELOCITY M/S | FIRST NORMAL MOVEOUT MS | SECOND NORMAL MOVEOUT MS | THIRD NORMAL MOVEOUT MS | INTERVAL VELOCITY M/S |
|---|--------------------------------------|---------------------------------------|---------------------------------------|------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------|
| 816.00 | 881.36 | 859.36 | 2106 | 2133 | 125.07 | 261.17 | 426.93 | 2537 |
| 818.00 | 883.90 | 861.90 | 2107 | 2134 | 124.68 | 260.45 | 425.88 | 2545 |
| 820.00 | 886.31 | 864.31 | 2108 | 2135 | 124.34 | 259.81 | 424.95 | 2412 |
| 822.00 | 888.90 | 866.90 | 2109 | 2136 | 123.95 | 259.08 | 423.87 | 2584 |
| 824.00 | 891.47 | 869.47 | 2110 | 2137 | 123.56 | 258.35 | 422.82 | 2568 |
| 826.00 | 893.87 | 871.87 | 2111 | 2138 | 123.22 | 257.73 | 421.91 | 2406 |
| 828.00 | 896.41 | 874.41 | 2112 | 2139 | 122.85 | 257.03 | 420.89 | 2542 |
| 830.00 | 898.98 | 876.98 | 2113 | 2140 | 122.47 | 256.31 | 419.84 | 2571 |

Synthetic

ANALYST: M. SANDERS

14-JUL-87 15:17:00

PROGRAM: GMULTP 006.E06

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*****  
*                                     *  
*                                     *  
*                                     *  
*                                     *  
*                                     *  
*          SCHLUMBERGER              *  
*                                     *  
*                                     *  
*****
```

SYNTHETIC SEISMOGRAM TABLE

COMPANY : LASMO ENERGY
WELL : PATRICIA - 1
FIELD : WILDCAT
COUNTRY : AUSTRALIA
REFERENCE: 570705

ANALYST: M. SANDERS

14-JUL-87 15:17:00

PROGRAM: GMULTP 006.E06

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*****  
*                                     *  
*                                     *  
*                                     *  
* *****                           *  
* *                                     *  
* * SCHLUMBERGER                       *  
* *                                     *  
* *****                           *  
*****
```

SYNTHETIC SEISMOGRAM TABLE

COMPANY : LASMO ENERGY
WELL : PATRICIA - 1
FIELD : WILDCAT
COUNTRY : AUSTRALIA
REFERENCE: 57C705

THE HEADINGS AND FLAGS SHOWN IN THE DATA LIST ARE DEFINED AS FOLLOWS:

IGEOF1- FLAG INDICATING MODE OF PROCESSING
IGEOF1 = 0 WST DATA AVAILABLE AND PROCESSED
IGEOF1 = 1 WST DATA NOT AVAILABLE

LOG INPUT DATA :
GRFOO1- CHANNEL NAME FOR INPUT DENSITY LOG DATA
GTROC1- CHANNEL NAME FOR INPUT SONIC LOG DATA
GCURVE- CORRELATION LOG NAMES

USER DEFINED MODELING

LOFVEL- LAYER OPTION FLAG FOR VELOCITY
LOFDEN- LAYER OPTION FLAG FOR DENSITY
LAYVEL- LAYERED VELOCITY VALUES FOR USER SUPPLIED ZONE LIMIT
WITH RESPECT TO SONIC LOG DATA
LAYDEN- LAYERED DENSITY VALUES FOR USER SUPPLIED ZONE LIMITS
WITH RESPECT TO SONIC LOG DATA
UNERTH- UNIFORM EARTH VELOCITY
UNFDEN- UNIFORM EARTH DENSITY
SRATE SAMPLING RATE IN MS
INIDEP START DEPTH FOR COMPUTING SYNTHETIC SEISMOGRAM
WITH RESPECT TO SONIC LOG DATA
IGESTP STOP DEPTH FOR COMPUTING SYNTHETIC SEISMOGRAM
WITH RESPECT TO SONIC LOG DATA
INITAU TWO WAY TRAVEL TIME FROM TOP SONIC TO SRD
EKB ELEVATION OF KELLY BUSHING WITH RESPECT TO
MEAN SEA LEVEL
SRDGEO SEISMIC REFERENCE DEPTH WITH RESPECT TO
MEAN SEA LEVEL
ICDP FLAG FOR COMPUTING RESIDUAL MULTIPLES
CDPTIM TWO WAY TIME INTERVAL FOR COMPUTATION OF
RESIDUAL MULTIPLES
SCRTIM SURFACE REFLECTOR TWO WAY TIME ABOVE INITAU
SCREFL SURFACE REFLECTION COEFFICIENT
RCMAX REFLECTION COEFFICIENTS THAT ARE EQUAL TO OR
GREATER THAN THIS VALUE SHALL BE FLAGGED

NOTE IN CASE OF MODELING A SYNTHETIC SEISMOGRAM WITHOUT
SONIC LOG DATA ,THE DEPTH REFERENCES SHALL BE USER
DEFINED

OUTPUT DATA

RMSVWE ROOT MEAN SQUARE VELOCITY FOUND FOR THE WELL
SRDTIM TWO WAY TRANSIT TIME BETWEEN INIDEP AND SRDGEO

CHANNEL NAMES

TWOT- TWO WAY TRAVEL TIME
 DSRD- DEPTH OF COMPUTED DATA WITH RESPECT TO SRD
 INTV- INTERVAL VELOCITY ON A TIME SCALE
 RHOT- INTERVAL DENSITY ON A TIME SCALE
 REFL- REFLECTION COEFFICIENT AT GIVEN TWO WAY TRAVEL TIMES
 ATTE- ATTENUATION COEFFICIENT AT GIVEN TWO WAY TRAVEL TIMES
 PRIM- SYNTHETIC SEISMOGRAM - PRIMARIES
 MULT- SYNTHETIC SEISMOGRAM - PRIMARIES + MULTIPLES
 MUON- MULTIPLES ONLY

CHANNEL NAMES

CHAN 1 - TWOT.GMU.002.*
 CHAN 2 - DSRD.GRF.006.*
 CHAN 3 - INTV.GRF.007.*
 CHAN 4 - RHOT.GRF.001.*
 CHAN 5 - REFL.GRF.001.*
 CHAN 6 - ATTE.GRF.001.*
 CHAN 7 - PRIM.GRF.001.*
 CHAN 8 - MULT.GMU.001.*
 CHAN 9 - MUON.GMU.001.*

(GLOBAL PARAMETERS)

(VALUE)

| | | | | |
|----------------------------|--------|---|----------|------|
| MODE OF PROC (GEOGRAM) | IGEOF | : | 0 | |
| INITIALIZE CDP LOGIC | ICDP | : | 0 | |
| CDP TIME | CDPTIM | : | 200000 | S |
| TIME SAMPLING (WST) | SRATE | : | 2.000000 | MS |
| TOP DEPTH OF PROCESSING | INIDEP | : | 198.000 | M |
| BOTTOM DEPTH OF PROCESSING | IGESTP | : | 872.000 | M |
| INITIAL TWO WAY TRAVEL T | INITAU | : | 232C80 | S |
| SRD FOR GEOGRAM | SRDGEO | : | -30479.7 | M |
| ELEVATION OF KELLY BUSHI | EKB | : | 0 | M |
| SRD TIME | SRDTIM | : | 0 | MS |
| SURFACE COEFFICIENT OF R | SCRTIM | : | 0 | MS |
| SURFACE COEFFICIENT OF R | SCREFL | : | -1.00000 | |
| REFLECTION COEFF MAXIMUM | RCMAX | : | 300000 | |
| RMS VELOCITY IN WELL | RMSVWE | : | 2288.01 | M/S |
| UNIFORM EARTH VELOCITY | UNERTH | : | 2133.60 | M/S |
| UNIFORM DENSITY VALUE | UNFDEN | : | 2.30000 | G/C3 |

(MATRIX PARAMETERS)

- 1 GR*
- 2 CALI*

(ZONED PARAMETERS)

| | | (VALUE) | (LIMITS) | |
|--------------------------|--------|-------------|----------|-----------|
| LAYER OPTION FLAG DENS | LOFDEN | : -1.000000 | 30479.7 | - 0 |
| LAYER OPTION FLAG VELOC | LOFVEL | : 1.000000 | 30479.7 | - 0 |
| USER SUPPLIED DENSITY DA | LAYDEN | : -999.2500 | 30479.7 | - 0 |
| USER VELOC (WST) | LAYVEL | : 1802.000 | 220.000 | - 73.0000 |
| | | 1480.000 | 73.0000 | 0 |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 234.1 | 200.22 | 2218 | 2.100 | -.023 | .99949 | -.02264 | -.02264 | 0 |
| 236.1 | 202.34 | 2120 | 2.100 | .028 | .99869 | .02830 | .02779 | -.00051 |
| 238.1 | 204.58 | 2243 | 2.100 | -.046 | .99656 | -.04611 | -.04482 | .00129 |
| 240.1 | 206.63 | 2045 | 2.100 | .038 | .99513 | .03777 | .03480 | -.00296 |
| 242.1 | 208.83 | 2206 | 2.100 | -.043 | .99326 | -.04315 | -.03870 | .00445 |
| 244.1 | 210.86 | 2023 | 2.100 | .018 | .99292 | .01819 | .01173 | -.00645 |
| 246.1 | 212.95 | 2098 | 2.100 | .011 | .99281 | .01050 | .01725 | .00675 |
| 248.1 | 215.10 | 2143 | 2.100 | -.017 | .99252 | -.01689 | -.02225 | -.00536 |
| 250.1 | 217.17 | 2072 | 2.100 | .015 | .99229 | .01522 | .01765 | .00243 |
| 252.1 | 219.30 | 2136 | 2.100 | .022 | .99182 | .02153 | .02229 | .00076 |
| 254.1 | 221.54 | 2231 | 2.100 | -.021 | .99139 | -.02078 | -.02228 | -.00150 |
| 256.1 | 223.68 | 2139 | 2.100 | -.021 | .99094 | -.02119 | -.01988 | .00131 |
| 258.1 | 225.72 | 2050 | 2.100 | .039 | .98940 | .03897 | .03797 | -.00100 |
| 260.1 | 227.94 | 2218 | 2.100 | -.017 | .98912 | -.01668 | -.01503 | .00165 |
| 262.1 | 230.09 | 2144 | 2.100 | .008 | .98906 | .00760 | .00578 | -.00182 |
| 264.1 | 232.26 | 2177 | 2.100 | .020 | .98865 | .02027 | .02347 | .00320 |
| 266.1 | 234.53 | 2268 | 2.100 | -.005 | .98862 | -.00523 | -.00963 | -.00440 |
| 268.1 | 236.78 | 2245 | 2.100 | .007 | .98857 | .00735 | .01230 | .00495 |
| 270.1 | 239.06 | 2278 | 2.100 | .004 | .98855 | .00424 | .00337 | -.00088 |
| 272.1 | 241.35 | 2298 | 2.100 | .013 | .98839 | .01247 | .00916 | -.00332 |
| 274.1 | 243.71 | 2356 | 2.100 | .013 | .98823 | .01252 | .01966 | .00714 |
| 276.1 | 246.13 | 2417 | 2.100 | .008 | .98817 | .00775 | .00461 | -.00314 |
| 278.1 | 248.58 | 2455 | 2.100 | -.016 | .98792 | -.01559 | -.01670 | -.00112 |
| 280.1 | 250.96 | 2379 | 2.100 | -.016 | .98766 | -.01604 | -.01406 | .00198 |
| | | 2303 | 2.100 | | | | | |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 282.1 | 253.26 | 2474 | 2.100 | .036 | .98640 | .03540 | .03501 | -.00039 |
| 284.1 | 255.74 | 2283 | 2.100 | -.040 | .98479 | -.03974 | -.03976 | -.00003 |
| 286.1 | 258.02 | 2229 | 2.100 | -.012 | .98466 | -.01164 | -.01432 | -.00268 |
| 288.1 | 260.25 | 2356 | 2.100 | .028 | .98390 | .02722 | .03091 | .00369 |
| 290.1 | 262.61 | 2238 | 2.100 | -.026 | .98326 | -.02520 | -.03088 | -.00568 |
| 292.1 | 264.84 | 2263 | 2.100 | .005 | .98323 | .00538 | .00851 | .00313 |
| 294.1 | 267.11 | 2160 | 2.100 | -.023 | .98270 | -.02280 | -.02346 | -.00066 |
| 296.1 | 269.27 | 2285 | 2.100 | .028 | .98193 | .02752 | .02068 | -.00685 |
| 298.1 | 271.55 | 2091 | 2.100 | -.044 | .98001 | -.04347 | -.03068 | .01279 |
| 300.1 | 273.64 | 2159 | 2.100 | .016 | .97975 | .01576 | .00201 | -.01375 |
| 302.1 | 275.80 | 2103 | 2.100 | -.013 | .97958 | -.01296 | -.00741 | .00555 |
| 304.1 | 277.91 | 2074 | 2.100 | -.007 | .97953 | -.00684 | -.00958 | -.00274 |
| 306.1 | 279.98 | 2150 | 2.100 | .018 | .97921 | .01766 | .02147 | .00381 |
| 308.1 | 282.13 | 2032 | 2.100 | -.028 | .97843 | -.02775 | -.03532 | -.00757 |
| 310.1 | 284.16 | 2092 | 2.100 | .015 | .97822 | .01444 | .01703 | .00259 |
| 312.1 | 286.25 | 2104 | 2.100 | .003 | .97821 | .00279 | .00943 | .00665 |
| 314.1 | 288.36 | 2166 | 2.100 | .014 | .97800 | .01415 | .00213 | -.01202 |
| 316.1 | 290.52 | 2149 | 2.100 | -.004 | .97799 | -.00387 | .00820 | .01206 |
| 318.1 | 292.67 | 2132 | 2.100 | -.004 | .97797 | -.00392 | -.00966 | -.00574 |
| 320.1 | 294.80 | 2146 | 2.100 | .003 | .97796 | .00315 | .00547 | .00231 |
| 322.1 | 296.95 | 2101 | 2.100 | -.010 | .97785 | -.01027 | -.00810 | .00216 |
| 324.1 | 299.05 | 2144 | 2.100 | .010 | .97775 | .00987 | .00759 | -.00228 |
| 326.1 | 301.20 | 2176 | 2.100 | .007 | .97770 | .00715 | .00996 | .00281 |
| 328.1 | 303.37 | 2129 | 2.100 | -.011 | .97759 | -.01056 | -.00998 | .00059 |
| 330.1 | 305.50 | | | .008 | .97752 | .00783 | .00948 | .00165 |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 332.1 | 307.66 | 2164 | 2.100 | -.014 | .97735 | -.01325 | -.01850 | -.00525 |
| 334.1 | 309.77 | 2106 | 2.100 | -.003 | .97734 | -.00286 | .00251 | .00537 |
| 336.1 | 311.86 | 2093 | 2.100 | .006 | .97730 | .00610 | .00837 | .00227 |
| 338.1 | 313.98 | 2120 | 2.100 | -.003 | .97729 | -.00265 | -.01003 | -.00737 |
| 340.1 | 316.09 | 2108 | 2.100 | -.005 | .97727 | -.00485 | .00283 | .00769 |
| 342.1 | 318.18 | 2087 | 2.100 | -.019 | .97692 | -.01847 | -.02180 | -.00333 |
| 344.1 | 320.19 | 2010 | 2.100 | .030 | .97606 | .02889 | .02645 | -.00244 |
| 346.1 | 322.32 | 2132 | 2.100 | .038 | .97465 | .03711 | .03986 | .00275 |
| 348.1 | 324.62 | 2301 | 2.100 | -.005 | .97463 | -.00448 | -.00350 | .00098 |
| 350.1 | 326.90 | 2280 | 2.100 | .061 | .97105 | .05913 | .05913 | 0 |
| 352.1 | 329.48 | 2574 | 2.100 | -.050 | .96864 | -.04834 | -.04643 | .00191 |
| 354.1 | 331.81 | 2330 | 2.100 | .016 | .96840 | .01519 | .01147 | -.00372 |
| 356.1 | 334.21 | 2404 | 2.100 | -.015 | .96818 | -.01455 | -.01111 | .00344 |
| 358.1 | 336.54 | 2333 | 2.100 | .042 | .96650 | .04036 | .03595 | -.00441 |
| 360.1 | 339.08 | 2536 | 2.100 | -.065 | .96239 | -.06301 | -.05377 | .00924 |
| 362.1 | 341.31 | 2226 | 2.100 | .014 | .96220 | .01354 | -.00064 | -.01418 |
| 364.1 | 343.59 | 2289 | 2.100 | .075 | .95681 | .07202 | .08099 | .00897 |
| 366.1 | 346.25 | 2660 | 2.100 | -.084 | .95008 | -.08024 | -.08249 | -.00225 |
| 368.1 | 348.50 | 2248 | 2.100 | .012 | .94995 | .01106 | .00721 | -.00385 |
| 370.1 | 350.80 | 2301 | 2.100 | -.030 | .94911 | -.02828 | -.02517 | .00310 |
| 372.1 | 352.97 | 2168 | 2.100 | .012 | .94898 | .01134 | .00286 | -.00848 |
| 374.1 | 355.19 | 2220 | 2.100 | .010 | .94889 | .00909 | .02709 | .01800 |
| 376.1 | 357.46 | 2263 | 2.100 | -.023 | .94840 | -.02146 | -.04238 | -.02092 |
| 378.1 | 359.62 | 2163 | 2.100 | -.003 | .94840 | -.00242 | .00257 | .00498 |
| | | 2152 | 2.100 | | | | | |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 380.1 | 361.77 | 2100 | 2.100 | -.012 | .94825 | -.01169 | -.00514 | .00656 |
| 382.1 | 363.87 | 2096 | 2.100 | -.001 | .94825 | -.00081 | -.01307 | -.01226 |
| 384.1 | 365.97 | 2152 | 2.100 | .013 | .94809 | .01245 | .01529 | .00284 |
| 386.1 | 368.12 | 2118 | 2.100 | -.008 | .94803 | -.00747 | -.00371 | .00376 |
| 388.1 | 370.24 | 2238 | 2.100 | .028 | .94731 | .02609 | .02103 | -.00507 |
| 390.1 | 372.48 | 2082 | 2.100 | -.036 | .94607 | -.03424 | -.03596 | -.00172 |
| 392.1 | 374.56 | 2134 | 2.100 | .012 | .94593 | .01171 | .01372 | .00201 |
| 394.1 | 376.69 | 2123 | 2.100 | -.003 | .94592 | -.00248 | -.00388 | -.00140 |
| 396.1 | 378.82 | 1999 | 2.100 | -.030 | .94507 | -.02839 | -.02851 | -.00012 |
| 398.1 | 380.82 | 2154 | 2.100 | .037 | .94376 | .03523 | .04265 | .00742 |
| 400.1 | 382.97 | 2371 | 2.100 | .048 | .94159 | .04525 | .03745 | -.00780 |
| 402.1 | 385.34 | 2494 | 2.100 | .025 | .94099 | .02370 | .03614 | .01243 |
| 404.1 | 387.84 | 2001 | 2.100 | -.110 | .92967 | -.10323 | -.09942 | .00381 |
| 406.1 | 389.84 | 2064 | 2.100 | .016 | .92944 | .01443 | -.00578 | -.02021 |
| 408.1 | 391.90 | 2123 | 2.100 | .014 | .92926 | .01312 | .02888 | .01576 |
| 410.1 | 394.02 | 2082 | 2.100 | -.010 | .92917 | -.00908 | -.00711 | .00197 |
| 412.1 | 396.10 | 2047 | 2.100 | -.008 | .92910 | -.00780 | -.00197 | .00583 |
| 414.1 | 398.15 | 2150 | 2.100 | .024 | .92855 | .02267 | -.00059 | -.02326 |
| 416.1 | 400.30 | 2238 | 2.100 | .020 | .92818 | .01862 | .04829 | .02968 |
| 418.1 | 402.54 | 2131 | 2.100 | -.024 | .92763 | -.02264 | -.03322 | -.01058 |
| 420.1 | 404.67 | 1943 | 2.100 | -.046 | .92565 | -.04276 | -.05159 | -.00884 |
| 422.1 | 406.61 | 2194 | 2.100 | .061 | .92225 | .05614 | .06672 | .01058 |
| 424.1 | 408.81 | 2533 | 2.100 | .072 | .91752 | .06606 | .06874 | .00268 |
| 426.1 | 411.34 | 2183 | 2.100 | -.074 | .91248 | -.06800 | -.06163 | .00636 |
| 428.1 | 413.52 | | | -.039 | .91109 | -.03560 | -.05898 | -.02339 |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 430.1 | 415.54 | 2019 | 2.100 | .008 | .91103 | .00735 | .01894 | .01160 |
| 432.1 | 417.59 | 2052 | 2.100 | .003 | .91102 | .00291 | -.01100 | -.01390 |
| 434.1 | 419.66 | 2065 | 2.100 | -.013 | .91088 | -.01152 | .00266 | .01418 |
| 436.1 | 421.67 | 2014 | 2.100 | .003 | .91087 | .00278 | -.00585 | -.00863 |
| 438.1 | 423.70 | 2026 | 2.100 | .007 | .91082 | .00670 | -.00571 | -.01242 |
| 440.1 | 425.75 | 2056 | 2.100 | .039 | .90944 | .03537 | .05750 | .02213 |
| 442.1 | 427.98 | 2222 | 2.100 | -.001 | .90944 | -.00126 | -.02038 | -.01911 |
| 444.1 | 430.19 | 2216 | 2.100 | .015 | .90925 | .01322 | .01461 | .00139 |
| 446.1 | 432.47 | 2281 | 2.100 | -.007 | .90921 | -.00597 | .01963 | .02561 |
| 448.1 | 434.73 | 2252 | 2.100 | -.006 | .90917 | -.00587 | -.02074 | -.01487 |
| 450.1 | 436.95 | 2223 | 2.100 | -.011 | .90905 | -.01045 | -.00927 | .00118 |
| 452.1 | 439.12 | 2172 | 2.100 | -.001 | .90905 | -.00131 | -.00496 | -.00365 |
| 454.1 | 441.29 | 2166 | 2.100 | .084 | .90266 | .07623 | .08747 | .01124 |
| 456.1 | 443.85 | 2562 | 2.100 | -.057 | .89977 | -.05102 | -.05250 | -.00148 |
| 458.1 | 446.14 | 2288 | 2.100 | .013 | .89962 | .01193 | -.00031 | -.01223 |
| 460.1 | 448.49 | 2350 | 2.100 | -.016 | .89940 | -.01400 | .00597 | .01997 |
| 462.1 | 450.76 | 2278 | 2.100 | -.014 | .89921 | -.01299 | -.03778 | -.02479 |
| 464.1 | 452.98 | 2213 | 2.100 | -.029 | .89843 | -.02649 | -.00790 | .01858 |
| 466.1 | 455.06 | 2086 | 2.100 | .014 | .89825 | .01284 | -.00817 | -.02102 |
| 468.1 | 457.21 | 2147 | 2.100 | -.004 | .89823 | -.00403 | .00071 | .00474 |
| 470.1 | 459.34 | 2128 | 2.100 | .045 | .89643 | .04024 | .05738 | .01714 |
| 472.1 | 461.67 | 2327 | 2.100 | -.035 | .89531 | -.03166 | -.04831 | -.01665 |
| 474.1 | 463.83 | 2168 | 2.100 | .028 | .89458 | .02550 | .02807 | .00257 |
| 476.1 | 466.13 | 2295 | 2.100 | .002 | .89458 | .00172 | .00881 | .00709 |
| | | 2304 | 2.100 | | | | | |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 478.1 | 468.43 | | | .008 | .89451 | .00759 | .00790 | .00031 |
| 480.1 | 470.78 | 2344 | 2.100 | -.031 | .89364 | -.02799 | -.03653 | -.00853 |
| 482.1 | 472.98 | 2202 | 2.100 | -.008 | .89357 | -.00756 | -.01157 | -.00401 |
| 484.1 | 475.14 | 2165 | 2.100 | .002 | .89357 | .00190 | .01381 | .01192 |
| 486.1 | 477.32 | 2174 | 2.100 | .015 | .89337 | .01325 | .00506 | -.00819 |
| 488.1 | 479.56 | 2239 | 2.100 | -.016 | .89315 | -.01410 | -.00426 | .00983 |
| 490.1 | 481.73 | 2170 | 2.100 | -.009 | .89308 | -.00816 | -.02283 | -.01467 |
| 492.1 | 483.86 | 2130 | 2.100 | -.007 | .89304 | -.00612 | .00769 | .01381 |
| 494.1 | 485.96 | 2101 | 2.100 | .024 | .89251 | .02156 | .02113 | -.00043 |
| 496.1 | 488.16 | 2205 | 2.100 | .037 | .89130 | .03295 | .01743 | -.01553 |
| 498.1 | 490.54 | 2374 | 2.100 | -.027 | .89066 | -.02378 | -.00158 | .02219 |
| 500.1 | 492.79 | 2251 | 2.100 | -.023 | .89020 | -.02028 | -.02623 | -.00595 |
| 502.1 | 494.94 | 2151 | 2.100 | .045 | .88837 | .04038 | .04749 | .00711 |
| 504.1 | 497.29 | 2355 | 2.100 | .007 | .88833 | .00588 | -.00738 | -.01326 |
| 506.1 | 499.68 | 2387 | 2.100 | -.018 | .88805 | -.01574 | -.01059 | .00514 |
| 508.1 | 501.98 | 2304 | 2.100 | -.020 | .88769 | -.01802 | .00225 | .02027 |
| 510.1 | 504.20 | 2212 | 2.100 | .025 | .88712 | .02234 | -.00023 | -.02257 |
| 512.1 | 506.52 | 2326 | 2.100 | .004 | .88711 | .00340 | .01567 | .01227 |
| 514.1 | 508.87 | 2344 | 2.100 | .012 | .88699 | .01024 | -.00380 | -.01403 |
| 516.1 | 511.27 | 2399 | 2.100 | .063 | .88348 | .05582 | .05903 | .00321 |
| 518.1 | 513.99 | 2721 | 2.100 | -.060 | .88032 | -.05286 | -.04092 | .01194 |
| 520.1 | 516.40 | 2414 | 2.100 | -.030 | .87955 | -.02601 | -.04115 | -.01514 |
| 522.1 | 518.68 | 2275 | 2.100 | -.001 | .87955 | -.00091 | .02541 | .02632 |
| 524.1 | 520.95 | 2271 | 2.100 | .053 | .87706 | .04680 | .02658 | -.02021 |
| 526.1 | 523.47 | 2526 | 2.100 | -.023 | .87660 | -.02011 | -.01098 | .00913 |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| | | 2412 | 2.100 | | | | | |
| 528.1 | 525.88 | 2847 | 2.100 | .083 | .87061 | .07247 | .06429 | -.00818 |
| 530.1 | 528.73 | 2655 | 2.100 | -.035 | .86954 | -.03045 | -.01966 | .01079 |
| 532.1 | 531.39 | 2221 | 2.100 | -.089 | .86264 | -.07745 | -.08324 | -.00579 |
| 534.1 | 533.61 | 2384 | 2.100 | .035 | .86156 | .03052 | .01426 | -.01626 |
| 536.1 | 535.99 | 2366 | 2.100 | -.004 | .86155 | -.00317 | .01660 | .01977 |
| 538.1 | 538.36 | 2199 | 2.100 | -.037 | .86040 | -.03150 | -.04709 | -.01559 |
| 540.1 | 540.56 | 2092 | 2.100 | -.025 | .85986 | -.02144 | -.02229 | -.00085 |
| 542.1 | 542.65 | 2179 | 2.100 | .020 | .85951 | .01751 | -.00625 | -.02377 |
| 544.1 | 544.83 | 2298 | 2.100 | .027 | .85890 | .02280 | .05115 | .02834 |
| 546.1 | 547.13 | 2479 | 2.100 | .038 | .85768 | .03247 | .04541 | .01294 |
| 548.1 | 549.60 | 2169 | 2.100 | -.067 | .85388 | -.05708 | -.08557 | -.02849 |
| 550.1 | 551.77 | 2605 | 2.100 | .091 | .84676 | .07796 | .09562 | .01766 |
| 552.1 | 554.38 | 2243 | 2.100 | -.075 | .84203 | -.06329 | -.03991 | .02338 |
| 554.1 | 556.62 | 2247 | 2.100 | .001 | .84203 | .00085 | -.04978 | -.05063 |
| 556.1 | 558.87 | 2168 | 2.100 | -.018 | .84176 | -.01513 | .00665 | .02179 |
| 558.1 | 561.04 | 2261 | 2.100 | .021 | .84138 | .01768 | .00072 | -.01695 |
| 560.1 | 563.30 | 2247 | 2.100 | -.003 | .84138 | -.00259 | .01994 | .02254 |
| 562.1 | 565.54 | 2287 | 2.100 | .009 | .84131 | .00740 | .01014 | .00273 |
| 564.1 | 567.83 | 2777 | 2.100 | .097 | .83344 | .08135 | .07157 | -.00978 |
| 566.1 | 570.61 | 2125 | 2.100 | -.133 | .81869 | -.11088 | -.11237 | -.00149 |
| 568.1 | 572.73 | 1914 | 2.100 | -.052 | .81646 | -.04271 | -.05432 | -.01160 |
| 570.1 | 574.65 | 1987 | 2.100 | .019 | .81618 | .01529 | .02498 | .00969 |
| 572.1 | 576.63 | 2116 | 2.100 | .031 | .81537 | .02563 | -.00986 | -.03550 |
| 574.1 | 578.75 | 2068 | 2.100 | -.011 | .81527 | -.00938 | .05560 | .06497 |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|------------------------|---------------------------|-----------------------|-----------------------|-----------------|-----------------------|---------------------------|---------------------|----------------|
| 576.1 | 580.82 | 1914 | 2.100 | -.039 | .81405 | -.03143 | -.06863 | -.03720 |
| 578.1 | 582.73 | 2090 | 2.124 | .050 | .81205 | .04038 | .02831 | -.01207 |
| 580.1 | 584.82 | 2421 | 2.171 | .084 | .80626 | .06856 | .09392 | .02535 |
| 582.1 | 587.24 | 1975 | 2.106 | -.117 | .79527 | -.09412 | -.07186 | .02226 |
| 584.1 | 589.22 | 2302 | 2.166 | .090 | .78879 | .07180 | .03446 | -.03735 |
| 586.1 | 591.52 | 2295 | 2.154 | -.004 | .78878 | -.00314 | .01855 | .02170 |
| 588.1 | 593.81 | 2306 | 2.279 | .030 | .78805 | .02396 | .03150 | .00754 |
| 590.1 | 596.12 | 2459 | 2.186 | .011 | .78795 | .00901 | .01529 | .00629 |
| 592.1 | 598.58 | 2164 | 2.163 | -.069 | .78417 | -.05456 | -.07927 | -.02471 |
| 594.1 | 600.74 | 2254 | 2.169 | .022 | .78379 | .01724 | .02112 | .00388 |
| 596.1 | 603.00 | 2254 | 2.190 | .005 | .78377 | .00364 | .03542 | .03178 |
| 598.1 | 605.25 | 2399 | 2.349 | .066 | .78033 | .05196 | .04300 | -.00895 |
| 600.1 | 607.65 | 2267 | 2.230 | -.054 | .77802 | -.04244 | -.05384 | -.01141 |
| 602.1 | 609.92 | 2278 | 2.267 | .011 | .77793 | .00832 | .00289 | -.00543 |
| 604.1 | 612.19 | 2126 | 2.095 | -.074 | .77370 | -.05742 | -.02293 | .03449 |
| 606.1 | 614.32 | 2126 | 2.095 | 0 | .77370 | -.00008 | -.05671 | -.05662 |
| 608.1 | 616.45 | 212 | 2.186 | .021 | .77334 | .01648 | .02627 | .00979 |
| 610.1 | 618.57 | 2126 | 2.153 | -.008 | .77330 | -.00595 | -.01149 | -.00554 |
| 612.1 | 620.70 | 2065 | 2.135 | -.019 | .77303 | -.01432 | .02657 | .04090 |
| 614.1 | 622.76 | 2090 | 2.118 | .002 | .77303 | .00159 | -.04694 | -.04853 |
| 616.1 | 624.85 | 1989 | 2.101 | -.029 | .77239 | -.02229 | -.02264 | -.00034 |
| 618.1 | 626.84 | 2007 | 2.085 | .001 | .77239 | .00043 | .02661 | .02618 |
| 620.1 | 628.85 | 2014 | 2.068 | -.002 | .77238 | -.00184 | -.02864 | -.02681 |
| 622.1 | 630.86 | 2020 | 2.001 | -.015 | .77221 | -.01153 | -.01564 | -.00411 |
| 624.1 | 632.88 | | | .004 | .77220 | .00308 | -.01222 | -.01531 |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 626.1 | 634.95 | 2063 | 1.976 | .022 | .77181 | .01734 | .05044 | .03311 |
| 628.1 | 636.99 | 2040 | 2.089 | -.013 | .77167 | -.01029 | -.04019 | -.02989 |
| 630.1 | 639.01 | 2020 | 2.054 | -.025 | .77119 | -.01926 | -.01170 | .00756 |
| 632.1 | 640.97 | 1964 | 2.010 | .052 | .76914 | .03979 | .04603 | .00624 |
| 634.1 | 643.06 | 2092 | 2.093 | -.001 | .76914 | -.00096 | -.00746 | -.00650 |
| 636.1 | 645.14 | 2077 | 2.102 | -.010 | .76906 | -.00790 | .00232 | .01021 |
| 638.1 | 647.19 | 2055 | 2.082 | .044 | .76759 | .03354 | .02375 | -.00979 |
| 640.1 | 649.39 | 2191 | 2.130 | .006 | .76757 | .00440 | .01694 | .01254 |
| 642.1 | 651.59 | 2209 | 2.137 | -.053 | .76543 | -.04051 | -.02680 | .01371 |
| 644.1 | 653.68 | 2085 | 2.038 | .005 | .76541 | .00409 | -.01209 | -.01618 |
| 646.1 | 655.71 | 2032 | 2.113 | -.003 | .76540 | -.00256 | -.00579 | -.00323 |
| 648.1 | 657.71 | 2004 | 2.128 | .017 | .76517 | .01334 | .02272 | .00938 |
| 650.1 | 659.80 | 2090 | 2.113 | .089 | .75907 | .06832 | .11116 | .04284 |
| 652.1 | 662.12 | 2317 | 2.280 | -.056 | .75667 | -.04265 | -.05481 | -.01216 |
| 654.1 | 664.31 | 2194 | 2.152 | -.009 | .75660 | -.00717 | -.01574 | -.00857 |
| 656.1 | 666.46 | 2147 | 2.157 | -.016 | .75640 | -.01236 | .01200 | .02436 |
| 658.1 | 668.58 | 2118 | 2.116 | .018 | .75616 | .01348 | -.01446 | -.02795 |
| 660.1 | 670.72 | 2136 | 2.175 | -.005 | .75614 | -.00374 | .00193 | .00566 |
| 662.1 | 672.85 | 2134 | 2.156 | .015 | .75598 | .01104 | .00172 | -.00932 |
| 664.1 | 674.92 | 2073 | 2.285 | .031 | .75525 | .02355 | .02986 | .00631 |
| 666.1 | 677.11 | 2186 | 2.306 | .045 | .75371 | .03405 | .05130 | .01725 |
| 668.1 | 679.38 | 2275 | 2.425 | -.131 | .74072 | -.09895 | -.12772 | -.02877 |
| 670.1 | 681.33 | 1950 | 2.173 | -.003 | .74071 | -.00231 | -.00384 | -.00153 |
| 672.1 | 683.32 | 1984 | 2.122 | .003 | .74071 | .00215 | .01510 | .01295 |
| | | 1994 | 2.123 | | | | | |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 674.1 | 685.31 | 1965 | 2.093 | -.015 | .74055 | -.01075 | -.00300 | .00775 |
| 676.1 | 687.28 | 1971 | 2.111 | .006 | .74053 | .00411 | -.05761 | -.06172 |
| 678.1 | 689.25 | 1991 | 2.089 | 0 | .74053 | .00008 | .00949 | .00941 |
| 680.1 | 691.24 | 2115 | 2.233 | .064 | .73754 | .04706 | .07194 | .02487 |
| 682.1 | 693.35 | 1961 | 2.179 | -.050 | .73568 | -.03703 | -.05636 | -.01933 |
| 684.1 | 695.31 | 1987 | 2.141 | -.002 | .73568 | -.00156 | .02573 | .02729 |
| 686.1 | 697.30 | 2104 | 2.201 | .042 | .73436 | .03105 | .01531 | -.01574 |
| 688.1 | 699.40 | 2029 | 2.188 | -.021 | .73404 | -.01550 | .01000 | .02550 |
| 690.1 | 701.43 | 1903 | 2.194 | -.031 | .73335 | -.02240 | -.02253 | -.00013 |
| 692.1 | 703.34 | 1901 | 2.148 | -.011 | .73326 | -.00822 | -.04102 | -.03280 |
| 694.1 | 705.24 | 1958 | 2.147 | .015 | .73311 | .01070 | -.00197 | -.01267 |
| 696.1 | 707.20 | 2001 | 2.102 | 0 | .73311 | .00018 | .00337 | .00319 |
| 698.1 | 709.20 | 1936 | 2.059 | -.027 | .73257 | -.01975 | .01282 | .03256 |
| 700.1 | 711.13 | 1981 | 2.142 | .031 | .73186 | .02279 | .00614 | -.01665 |
| 702.1 | 713.11 | 1966 | 2.120 | -.009 | .73181 | -.00637 | -.00341 | .00296 |
| 704.1 | 715.08 | 2068 | 2.178 | .039 | .73071 | .02834 | .02603 | -.00231 |
| 706.1 | 717.15 | 2294 | 2.534 | .127 | .71894 | .09274 | .07123 | -.02151 |
| 708.1 | 719.44 | 2061 | 2.453 | -.070 | .71545 | -.05011 | .02819 | .07830 |
| 710.1 | 721.50 | 2051 | 2.265 | -.042 | .71418 | -.03019 | -.04128 | -.01109 |
| 712.1 | 723.55 | 2058 | 2.242 | -.004 | .71417 | -.00257 | -.04635 | -.04378 |
| 714.1 | 725.61 | 2060 | 2.268 | .006 | .71414 | .00458 | .01046 | .00588 |
| 716.1 | 727.67 | 2464 | 2.284 | .093 | .70801 | .06616 | .05408 | -.01208 |
| 718.1 | 730.14 | 2475 | 2.239 | -.008 | .70797 | -.00533 | .06140 | .06673 |
| 720.1 | 732.61 | 2719 | 2.209 | .040 | .70682 | .02847 | -.03735 | -.06582 |
| 722.1 | 735.33 | | | .117 | .69720 | .08247 | .15311 | .07064 |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| | | 3187 | 2.383 | | | | | |
| 724.1 | 738.52 | 3280 | 2.299 | -.003 | .69719 | -.00241 | .03904 | .04145 |
| 726.1 | 741.80 | 3070 | 2.339 | -.025 | .69677 | -.01711 | -.04948 | -.03237 |
| 728.1 | 744.87 | 2996 | 2.312 | -.018 | .69655 | -.01248 | .00805 | .02053 |
| 730.1 | 747.86 | 2909 | 2.276 | -.023 | .69619 | -.01581 | -.04880 | -.03299 |
| 732.1 | 750.77 | 2912 | 2.255 | -.004 | .69618 | -.00289 | .03666 | .03956 |
| 734.1 | 753.68 | 3016 | 2.326 | .033 | .69541 | .02305 | .01519 | -.00786 |
| 736.1 | 756.70 | 2846 | 2.237 | -.049 | .69378 | -.03374 | -.06240 | -.02866 |
| 738.1 | 759.55 | 3007 | 2.327 | .047 | .69223 | .03273 | .04106 | .00833 |
| 740.1 | 762.55 | 2900 | 2.210 | -.044 | .69090 | -.03039 | -.04142 | -.01103 |
| 742.1 | 765.45 | 3039 | 2.305 | .045 | .68953 | .03076 | .00896 | -.02180 |
| 744.1 | 768.49 | 2978 | 2.163 | -.042 | .68832 | -.02891 | .00844 | .03735 |
| 746.1 | 771.47 | 3084 | 2.315 | .051 | .68651 | .03530 | .03885 | .00356 |
| 748.1 | 774.55 | 3070 | 2.360 | .007 | .68647 | .00514 | .00255 | -.00259 |
| 750.1 | 777.62 | 2350 | 2.175 | -.173 | .66596 | -.11865 | -.14672 | -.02808 |
| 752.1 | 779.97 | 2344 | 2.214 | .008 | .66592 | .00513 | .00910 | .00396 |
| 754.1 | 782.32 | 2522 | 2.183 | .030 | .66533 | .01977 | -.02129 | -.04106 |
| 756.1 | 784.84 | 2533 | 2.183 | .002 | .66533 | .00147 | -.01323 | -.01470 |
| 758.1 | 787.37 | 2535 | 2.157 | -.006 | .66531 | -.00377 | .03274 | .03652 |
| 760.1 | 789.91 | 2339 | 2.169 | -.037 | .66438 | -.02490 | -.00981 | .01509 |
| 762.1 | 792.25 | 2312 | 2.191 | -.001 | .66438 | -.00064 | -.03712 | -.03648 |
| 764.1 | 794.56 | 2253 | 2.121 | -.029 | .66381 | -.01936 | -.05268 | -.03332 |
| 766.1 | 796.81 | 2459 | 2.239 | .071 | .66049 | .04697 | .05146 | .00449 |
| 768.1 | 799.27 | 2275 | 2.132 | -.063 | .65784 | -.04186 | -.03147 | .01039 |
| 770.1 | 801.55 | 2438 | 2.178 | .045 | .65648 | .02991 | .06073 | .03081 |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 772.1 | 803.98 | 2580 | 2.202 | .034 | .65573 | .02210 | -.02333 | -.04543 |
| 774.1 | 806.56 | 2514 | 2.175 | -.019 | .65549 | -.01254 | .05155 | .06409 |
| 776.1 | 809.08 | 2442 | 2.183 | -.013 | .65538 | -.00838 | .00083 | .00921 |
| 778.1 | 811.52 | 2458 | 2.225 | .013 | .65528 | .00843 | -.02330 | -.03173 |
| 780.1 | 813.98 | 2415 | 2.202 | -.014 | .65515 | -.00906 | -.01435 | -.00528 |
| 782.1 | 816.39 | 2699 | 2.224 | .060 | .65277 | .03946 | .05391 | .01445 |
| 784.1 | 819.09 | 2712 | 2.192 | -.005 | .65276 | -.00310 | .04914 | .05225 |
| 786.1 | 821.80 | 2804 | 2.184 | .015 | .65262 | .00969 | -.01633 | -.02602 |
| 788.1 | 824.61 | 2656 | 2.182 | -.027 | .65212 | -.01790 | -.01889 | -.00098 |
| 790.1 | 827.26 | 2596 | 2.208 | -.006 | .65210 | -.00372 | .01369 | .01740 |
| 792.1 | 829.86 | 2557 | 2.227 | -.003 | .65210 | -.00205 | -.02569 | -.02364 |
| 794.1 | 832.42 | 2540 | 2.224 | -.004 | .65209 | -.00268 | .03660 | .03929 |
| 796.1 | 834.96 | 2450 | 2.264 | -.009 | .65203 | -.00590 | -.03285 | -.02695 |
| 798.1 | 837.41 | 2518 | 2.196 | -.002 | .65203 | -.00104 | -.02860 | -.02757 |
| 800.1 | 839.92 | 2525 | 2.245 | .013 | .65193 | .00818 | .03020 | .02202 |
| 802.1 | 842.45 | 2482 | 2.241 | -.010 | .65187 | -.00622 | -.05093 | -.04471 |
| 804.1 | 844.93 | 2381 | 2.120 | -.048 | .65035 | -.03151 | .02687 | .05838 |
| 806.1 | 847.31 | 2539 | 2.210 | .053 | .64854 | .03425 | -.00107 | -.03531 |
| 808.1 | 849.85 | 2572 | 2.232 | .011 | .64846 | .00741 | -.00911 | -.01652 |
| 810.1 | 852.42 | 2148 | 2.033 | -.136 | .63647 | -.08817 | -.06208 | .02609 |
| 812.1 | 854.57 | 2282 | 2.047 | .034 | .63574 | .02149 | -.00309 | -.02458 |
| 814.1 | 856.85 | 2537 | 2.230 | .095 | .62995 | .06067 | .08240 | .02173 |
| 816.1 | 859.39 | 2545 | 2.214 | -.002 | .62995 | -.00117 | -.03043 | -.02927 |
| 818.1 | 861.94 | 2415 | 2.151 | -.041 | .62890 | -.02579 | -.00510 | .02070 |
| 820.1 | 864.35 | | | .034 | .62816 | .02147 | .00558 | -.01589 |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 822.1 | 866.93 | 2580 | 2.155 | -.004 | .62815 | -.00265 | -.00400 | -.00135 |
| 824.1 | 869.50 | 2571 | 2.145 | -.032 | .62752 | -.01994 | .01645 | .03638 |
| 826.1 | 871.91 | 2407 | 2.150 | -.003 | .62751 | -.00170 | -.03089 | -.02919 |
| 828.1 | 874.30 | 2394 | 2.150 | 0 | 0 | 0 | -.00745 | -.00745 |
| 830.1 | | | | | | | .01878 | .01878 |
| 832.1 | | | | | | | -.00859 | -.00859 |
| 834.1 | | | | | | | -.03270 | -.03270 |
| 836.1 | | | | | | | .04902 | .04902 |
| 838.1 | | | | | | | .01018 | .01018 |
| 840.1 | | | | | | | -.05747 | -.05747 |
| 842.1 | | | | | | | -.02056 | -.02056 |
| 844.1 | | | | | | | .05628 | .05628 |
| 846.1 | | | | | | | .01492 | .01492 |
| 848.1 | | | | | | | -.06011 | -.06011 |
| 850.1 | | | | | | | .03671 | .03671 |
| 852.1 | | | | | | | .04076 | .04076 |
| 854.1 | | | | | | | -.04247 | -.04247 |
| 856.1 | | | | | | | -.02317 | -.02317 |
| 858.1 | | | | | | | .00477 | .00477 |
| 860.1 | | | | | | | .03451 | .03451 |
| 862.1 | | | | | | | -.00134 | -.00134 |
| 864.1 | | | | | | | -.03955 | -.03955 |
| 866.1 | | | | | | | .05704 | .05704 |
| 868.1 | | | | | | | .00442 | .00442 |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 870.1 | | | | | | | -.03565 | -.03565 |
| 872.1 | | | | | | | -.00033 | -.00033 |
| 874.1 | | | | | | | -.01432 | -.01432 |
| 876.1 | | | | | | | -.00275 | -.00275 |
| 878.1 | | | | | | | .02528 | .02528 |
| 880.1 | | | | | | | .03419 | .03419 |
| 882.1 | | | | | | | -.01412 | -.01412 |
| 884.1 | | | | | | | .01063 | .01063 |
| 886.1 | | | | | | | .00968 | .00968 |
| 888.1 | | | | | | | -.06429 | -.06429 |
| 890.1 | | | | | | | .04910 | .04910 |
| 892.1 | | | | | | | -.04214 | -.04214 |
| 894.1 | | | | | | | .02888 | .02888 |
| 896.1 | | | | | | | .02165 | .02165 |
| 898.1 | | | | | | | -.02809 | -.02809 |
| 900.1 | | | | | | | .00627 | .00627 |
| 902.1 | | | | | | | -.02353 | -.02353 |
| 904.1 | | | | | | | .01549 | .01549 |
| 906.1 | | | | | | | .01620 | .01620 |
| 908.1 | | | | | | | -.04931 | -.04931 |
| 910.1 | | | | | | | .03087 | .03087 |
| 912.1 | | | | | | | -.00657 | -.00657 |
| 914.1 | | | | | | | -.02344 | -.02344 |
| 916.1 | | | | | | | .01089 | .01089 |
| 918.1 | | | | | | | .02920 | .02920 |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 920.1 | | | | | | | .02566 | .02566 |
| 922.1 | | | | | | | -.03997 | -.03997 |
| 924.1 | | | | | | | .03114 | .03114 |
| 926.1 | | | | | | | -.03649 | -.03649 |
| 928.1 | | | | | | | -.01787 | -.01787 |
| 930.1 | | | | | | | -.00698 | -.00698 |
| 932.1 | | | | | | | .03123 | .03123 |
| 934.1 | | | | | | | .00692 | .00692 |
| 936.1 | | | | | | | -.03178 | -.03178 |
| 938.1 | | | | | | | .02049 | .02049 |
| 940.1 | | | | | | | -.00152 | -.00152 |
| 942.1 | | | | | | | .01518 | .01518 |
| 944.1 | | | | | | | -.05803 | -.05803 |
| 946.1 | | | | | | | .02598 | .02598 |
| 948.1 | | | | | | | .01669 | .01669 |
| 950.1 | | | | | | | -.04879 | -.04879 |
| 952.1 | | | | | | | .06494 | .06494 |
| 954.1 | | | | | | | .00152 | .00152 |
| 956.1 | | | | | | | -.03444 | -.03444 |
| 958.1 | | | | | | | .02425 | .02425 |
| 960.1 | | | | | | | .00039 | .00039 |
| 962.1 | | | | | | | -.00978 | -.00978 |
| 964.1 | | | | | | | -.00345 | -.00345 |
| 966.1 | | | | | | | .02831 | .02831 |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 968.1 | | | | | | | -.04262 | -.04262 |
| 970.1 | | | | | | | .02399 | .02399 |
| 972.1 | | | | | | | .04924 | .04924 |
| 974.1 | | | | | | | -.01998 | -.01998 |
| 976.1 | | | | | | | -.01827 | -.01827 |
| 978.1 | | | | | | | -.01014 | -.01014 |
| 980.1 | | | | | | | -.00285 | -.00285 |
| 982.1 | | | | | | | -.00191 | -.00191 |
| 984.1 | | | | | | | -.01455 | -.01455 |
| 986.1 | | | | | | | .02918 | .02918 |
| 988.1 | | | | | | | -.00063 | -.00063 |
| 990.1 | | | | | | | -.01328 | -.01328 |
| 992.1 | | | | | | | -.04067 | -.04067 |
| 994.1 | | | | | | | .05431 | .05431 |
| 996.1 | | | | | | | -.03137 | -.03137 |
| 998.1 | | | | | | | -.06311 | -.06311 |
| 1000.1 | | | | | | | .08502 | .08502 |
| 1002.1 | | | | | | | -.02402 | -.02402 |
| 1004.1 | | | | | | | -.03250 | -.03250 |
| 1006.1 | | | | | | | .01707 | .01707 |
| 1008.1 | | | | | | | -.00771 | -.00771 |
| 1010.1 | | | | | | | .02963 | .02963 |
| 1012.1 | | | | | | | -.03709 | -.03709 |
| 1014.1 | | | | | | | .01589 | .01589 |
| 1016.1 | | | | | | | .01062 | .01062 |

| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 1018.1 | | | | | | | -.01313 | -.01313 |
| 1020.1 | | | | | | | -.00018 | -.00018 |
| 1022.1 | | | | | | | .04120 | .04120 |
| 1024.1 | | | | | | | .04582 | .04582 |
| 1026.1 | | | | | | | -.03227 | -.03227 |
| 1028.1 | | | | | | | -.04004 | -.04004 |
| 1030.1 | | | | | | | .02503 | .02503 |
| 1032.1 | | | | | | | .04337 | .04337 |
| 1034.1 | | | | | | | .00020 | .00020 |
| 1036.1 | | | | | | | -.08766 | -.08766 |
| 1038.1 | | | | | | | .04145 | .04145 |
| 1040.1 | | | | | | | .03313 | .03313 |
| 1042.1 | | | | | | | -.01200 | -.01200 |
| 1044.1 | | | | | | | .00749 | .00749 |
| 1046.1 | | | | | | | -.00156 | -.00156 |
| 1048.1 | | | | | | | .02217 | .02217 |
| 1050.1 | | | | | | | -.05086 | -.05086 |
| 1052.1 | | | | | | | -.00097 | -.00097 |
| 1054.1 | | | | | | | .01081 | .01081 |
| 1056.1 | | | | | | | -.00752 | -.00752 |
| 1058.1 | | | | | | | .00480 | .00480 |
| 1060.1 | | | | | | | .00426 | .00426 |
| 1062.1 | | | | | | | .01158 | .01158 |
| 1064.1 | | | | | | | -.02978 | -.02978 |

COMPANY : LASMO ENERGY

WELL : PATRICIA - 1

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| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 1066.1 | | | | | | | -.01226 | -.01226 |
| 1068.1 | | | | | | | .04191 | .04191 |
| 1070.1 | | | | | | | -.05668 | -.05668 |
| 1072.1 | | | | | | | .00428 | .00428 |
| 1074.1 | | | | | | | .00994 | .00994 |
| 1076.1 | | | | | | | .01444 | .01444 |
| 1078.1 | | | | | | | -.00447 | -.00447 |
| 1080.1 | | | | | | | -.01692 | -.01692 |
| 1082.1 | | | | | | | .05938 | .05938 |
| 1084.1 | | | | | | | -.05220 | -.05220 |
| 1086.1 | | | | | | | -.00828 | -.00828 |
| 1088.1 | | | | | | | -.00366 | -.00366 |
| 1090.1 | | | | | | | .01690 | .01690 |
| 1092.1 | | | | | | | .03812 | .03812 |
| 1094.1 | | | | | | | .00590 | .00590 |
| 1096.1 | | | | | | | -.01092 | -.01092 |
| 1098.1 | | | | | | | -.01566 | -.01566 |
| 1100.1 | | | | | | | .00609 | .00609 |
| 1102.1 | | | | | | | .00714 | .00714 |
| 1104.1 | | | | | | | .00140 | .00140 |
| 1106.1 | | | | | | | .03070 | .03070 |
| 1108.1 | | | | | | | -.00649 | -.00649 |
| 1110.1 | | | | | | | .00833 | .00833 |
| 1112.1 | | | | | | | -.01997 | -.01997 |
| 1114.1 | | | | | | | -.00958 | -.00958 |

COMPANY : LASMO ENERGY

WELL : PATRICIA - 1

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| TWO WAY TRAVEL TIME MS | DEPTH FROM SRD (OR TOP) M | INTERVAL VELOCITY M/S | INTERVAL DENSITY G/C3 | REFLECT. COEFF. | TWO WAY ATTEN. COEFF. | SYNTHETIC SEISMO. PRIMARY | PRIMARY + MULTIPLES | MULTIPLES ONLY |
|---------------------------------|------------------------------------|-----------------------------|-----------------------------|--------------------|-----------------------------|---------------------------------|---------------------------|-------------------|
| 1116.1 | | | | | | | .03246 | .03246 |
| 1118.1 | | | | | | | -.01190 | -.01190 |
| 1120.1 | | | | | | | .02906 | .02906 |
| 1122.1 | | | | | | | -.04700 | -.04700 |
| 1124.1 | | | | | | | -.01467 | -.01467 |
| 1126.1 | | | | | | | .01821 | .01821 |

PE906989

This is an enclosure indicator page.
The enclosure PE906989 is enclosed within the
container PE906975 at this location in this
document.

The enclosure PE906989 has the following characteristics:

- ITEM_BARCODE = PE906989
- CONTAINER_BARCODE = PE906975
 - NAME = Geogram/Synthetic Seismogram
 - BASIN = GIPPSLAND
 - PERMIT = VIC/P11
 - TYPE = WELL
 - SUBTYPE = SYNTH_SEISMOGRAM
 - DESCRIPTION = Geogram/Synthetic Seismogram, 60Hz,
(enclosure from attachment to WCR) for
Patricia-1
- REMARKS =
- DATE_CREATED = 6/07/87
- DATE_RECEIVED = 17/08/87
 - W_NO = W963
 - WELL_NAME = PATRICIA-1
 - CONTRACTOR = SCHLUMBERGER
 - CLIENT_OP_CO = LASMO ENERGY AUSTRALIA LIMITED

(Inserted by DNRE - Vic Govt Mines Dept)

PE906990

This is an enclosure indicator page.
The enclosure PE906990 is enclosed within the
container PE906975 at this location in this
document.

The enclosure PE906990 has the following characteristics:

- ITEM_BARCODE = PE906990
- CONTAINER_BARCODE = PE906975
 - NAME = Geogram/Synthetic Seismogram
 - BASIN = GIPPSLAND
 - PERMIT = VIC/P11
 - TYPE = WELL
 - SUBTYPE = SYNTH_SEISMOGRAM
 - DESCRIPTION = Geogram/Synthetic Seismogram, 40Hz,
(enclosure from attachment to WCR) for
Patricia-1
- REMARKS =
- DATE_CREATED = 6/07/87
- DATE_RECEIVED = 17/08/87
 - W_NO = W963
 - WELL_NAME = PATRICIA-1
 - CONTRACTOR = SCHLUMBERGER
 - CLIENT_OP_CO = LASMO ENERGY AUSTRALIA LIMITED

(Inserted by DNRE - Vic Govt Mines Dept)

PE906991

This is an enclosure indicator page.
The enclosure PE906991 is enclosed within the
container PE906975 at this location in this
document.

The enclosure PE906991 has the following characteristics:

- ITEM_BARCODE = PE906991
- CONTAINER_BARCODE = PE906975
- NAME = Geogram/Synthetic Seismogram
- BASIN = GIPPSLAND
- PERMIT = VIC/P11
- TYPE = WELL
- SUBTYPE = SYNTH_SEISMOGRAM
- DESCRIPTION = Geogram/Synthetic Seismogram, 50Hz,
(enclosure from attachment to WCR) for
Patricia-1
- REMARKS =
- DATE_CREATED = 6/07/87
- DATE_RECEIVED = 17/08/87
- W_NO = W963
- WELL_NAME = PATRICIA-1
- CONTRACTOR = SCHLUMBERGER
- CLIENT_OP_CO = LASMO ENERGY AUSTRALIA LIMITED

(Inserted by DNRE - Vic Govt Mines Dept)

PE906992

This is an enclosure indicator page.
The enclosure PE906992 is enclosed within the
container PE906975 at this location in this
document.

The enclosure PE906992 has the following characteristics:

- ITEM_BARCODE = PE906992
- CONTAINER_BARCODE = PE906975
- NAME = Seismic Calibration Log
- BASIN = GIPPSLAND
- PERMIT = VIC/P11
- TYPE = WELL
- SUBTYPE = VELOCITY_CHART
- DESCRIPTION = Seismic Calibration Log, Adjusted
Continuous Velocity Log, (enclosure
from attachment to WCR) for Patricia-1
- REMARKS =
- DATE_CREATED = 6/07/87
- DATE_RECEIVED = 17/08/87
- W_NO = W963
- WELL_NAME = PATRICIA-1
- CONTRACTOR = SCHLUMBERGER
- CLIENT_OP_CO = LASMO ENERGY AUSTRALIA LIMITED

(Inserted by DNRE - Vic Govt Mines Dept)

PE906993

This is an enclosure indicator page.
The enclosure PE906993 is enclosed within the
container PE906975 at this location in this
document.

The enclosure PE906993 has the following characteristics:

- ITEM_BARCODE = PE906993
- CONTAINER_BARCODE = PE906975
 - NAME = Seismic Calibration Log
 - BASIN = GIPPSLAND
 - PERMIT = VIC/P11
 - TYPE = WELL
 - SUBTYPE = VELOCITY_CHART
 - DESCRIPTION = Seismic Calibration Log (enclosure from
attachment to WCR) for Patricia-1
- REMARKS =
- DATE_CREATED = 6/07/87
- DATE_RECEIVED = 17/08/87
 - W_NO = W963
 - WELL_NAME = PATRICIA-1
 - CONTRACTOR = SCHLUMBERGER
 - CLIENT_OP_CO = LASMO ENERGY AUSTRALIA LIMITED

(Inserted by DNRE - Vic Govt Mines Dept)